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**DOCUMENT 360-82** 

KWAJALEIN MISSILE RANGE KWAJALEIN, MARSHALL ISLANDS

RANGE REFERENCE ATMOSPHERE
0-70 KM ALTITUDE



WHITE SANDS MISSILE RANGE KWAJALEIN MISSILE RANGE YUMA PROVING GROUND

PACIFIC MISSILE TEST CENTER
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#### DOCUMENT 360-82

# KWAJALEIN MISSILE RANGE KWAJALEIN, MARSHALL ISLANDS RANGE REFERENCE ATMOSPHERE 0-70 km ALTITUDE

Prepared by

Range Reference Atmosphere Committee

Meteorology Group

Range Commanders Council

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White Sands Missile Range, New Mexico 88002

## TABLE OF CONTENTS

		Page
CHAPTER I.	INTRODUCTION	1
	A. Definition and Purpose of the Range	
	Reference Atmosphere	1
	and Arrangement of Tables	$\begin{array}{c} 1 \\ 2 \end{array}$
	D. Organization of the Chapters	3
CHAPTER II.	WIND STATISTICS AND MODELS	5
	A. General Considerations  B. Coordinate System and Computation of	5
	Statistical Parameters	8 10
	D. Statistical Parameters With Respect to Any	10
	Orthogonal Axes	25
CHAPTER III.	STATISTICS OF THERMODYNAMIC QUANTITIES	27
	AND MODELS	21
	A. General Considerations  B. Establishing Data Samples at the Required	27
	Altitude Levels	30
	Tables II and III	35
	D. Derived Monthly Mean and Annual Mean Model Atmospheres	38
	E. Thermodynamic Quantities Derivable from the Basic Tables	38
CHADTED IV	CONCLUSIONS AND RECOMMENDATIONS	45
REFERENCES .		46
CONVERSION U	A A A A A A A A A A A A A A A A A A A	49
APPENDIX A		105
APPENDIX B	Wommounced Februariou	158
	Distribution/	
	Availability Codes	
	l emenial	
	Dise	



#### LIST OF ORGANIZATION ACRONYMS

AD Armament Division

AFFTC Air Force Flight Test Center

AFSC Air Force Systems Command

AFSC/AFGL AFSC/Air Force Geophysics Laboratory

AFSCF Air Force Satellite Control Facility

AFTFWC Air Force Tactical Fighter Weapons Center

AWS Air Weather Service

BMD Ballist's Missile Division

DOD Department of Defense

DOE Department of Energy

DOE/NTS DOE/Nevada Test Site

DPG Dugway Proving Ground

ESMC Eastern Space and Missile Center

ETR Eastern Test Range

KMR Kwajalein Missile Range

NASA National Aeronautics and Space Administration

NASA/MSFC NASA/Marshall Space Flight Center

NASA/WFC NASA/Wallops Flight Center

NOAA -- National Oceanic and Atmospheric Administration

NWC Maral Weapons Center

PMTC Pecific Missile Test Center

SAMTO Space and Missile Test Organization

USA/DTA U.S. Army/Deseret Test Center

USAECOM USAECOM Electronics Command

USAFETAC United States Air Force Environmental Technical Applications Center

UTTR Utah Test and Training Range

WSMC Western Space and Missile Center

WSMR White Sands Missile Range

WTR Western Test Range

YPG Yuma Proving Ground

6585TG 6585th Test Group

TSCF Targeting Systems Characterization Facility

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#### **FOREWORD**

Atmospheric parameters are essential to the research and development of missiles and aerospace vehicles. The need for realistic atmospheric models derived in a consistent manner for each of the several major test ranges was recognized in the early 1960's. An atmospheric model which is derived from statistical data for a particular geographical location is referred to as a reference atmosphere.

Following the first Range Reference Atmosphere (RRA) by the Inter-Range Instrumentation Group (IRIG) for Cape Kennedy, Florida, issued in 1963 and additional publications for several ranges up to 1974, improved upper-air data bases have become available from which to develop the RRA. This is the result of the extended period of records and improvement in the upper-air measuring program by rocketsondes for altitudes above the rawinsonde ceiling of 30 km altitude. Revised and improved RRAs are justified because:

- 1) Needs for more definitive statistical atmospheric models have arisen due to changes and advances in aerospace technology. The Space Transportation System (Space Shuttle) is one example.
- 2) There is now an extended and improved upper-air data base for most ranges from which to develop a more definitive RRA.
- 3) There are requirements for RRAs for new ranges and range sites.
- 4) There have been scientific advances in understanding the upper atmospheric structure and physical relationships.
- 5) Advances in statistical modeling techniques have been made due to the general availability of high-speed electronic computers. This has led to the adoption of advanced concepts in atmospheric modeling. For these reasons the Range Reference Atmosphere Committee (RRAC) was tasked by the Range Commander's Council/Meteorology Group (RCC/MG) to establish new and improved RRAs. The purpose, scope, and objectives of this task are:

Purpose: This committee, Task MG-1, establishes RRAs for the several ranges as provided by the RCC. An RRA is a model of the Earth's atmosphere over a geographical location of interest for use by DOD and other U.S. Government range users. The RRA is used to provide planning data for evaluating environmental constraints for the particular configurations of environment-sensitive systems and components being developed or undergoing tests.

Scope: Using the best available upper atmosphere data base to include rawinsonde, rocketsonde and possibly other high-altitude data sources for the range location, the task is to establish a model of certain statistics for wind and thermodynamic quantities derived in a uniform manner and published in a standardized format.

Parice

Objectives: The wind statistics shall be, insofar as practical, modeled to be consistent with rigorous mathematical probability properties of the multivariate normal probability theory. The thermodynamic quantities statistics shall be, insofar as practical, modeled to be consistent with the hydrostatic equation, the equation of state, and the probability principles which are related through these physical equations. The document shall serve as an authoritative source of information and as an atmospheric model for a particular range. The first in the series of revised RRAs to be published is for Kwajalein Missile Range (KMR) (publication date December 1982). The altitude range required for KMR is 0 to 70 km. The order of priority for the subsequent publications is:

Range		Altitude Range Required		
1.	AFFTC/Edwards AFB. CA	0 - 70 km <sup>a</sup>		
2.	ESMC/Cape Canaveral AFS, FL	0 - 70 km		
3.	WSMC/Vandenberg, AFB, CA	0 - 70 km <sup>a</sup>		
4.	WSMR/White Sands, NM	.0 - 70 km		
5.	PMTC/Point Mugu, CA	0 - 70 km		
6.	UTTR/Dugway (Michales AAF), UT	$0 - 30 \text{ km}^b$		
7.	AD/Eglin AFB, FL	0 - 30 km		
8.	ESMC/Ascension Island	0 - 70 km (Terminates at 66 km because of insufficient data)		
9.	NASA/Wallops Flight Center, VA	0 - 70 km		
10.	Taquac (Guam)	0 - 30 km		
11.	PMTC/Barking Sands, HI	0 - 70 km		

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In keeping with the RCC's objective of standardization, the modeling techniques, basic text, and tabulation format are to be the same for all RRAs. These new and revised RRAs present not only the mean values of the thermodynamic quantities (pressure, temperature, virtual temperature, and density) but also include a statistical measure for the dispersion, i.e , standard deviations and skewness coefficients. New quantities presented are water vapor pressure and dewpoint temperature. The statistical modeling for the wind is entirely new. The new approach uses the properties of the bivariate normal probability distribution function.

a. Use rocketsonde data from PMTC/Point Mugu for altitudes above 30 km.

b. Consider augmenting data base from Ely or Salt Lake City.

All final computations were performed by the United States Air Force Environmental Technical Applications Center (USAFETAC) in response to a task from Eastern Space and Missile Center (ESMC).

The test was prepared jointly between USAFETAC and the NASA/George C. Marshall Space Flight Center's Space Sciences Laboratory. Atmospheric Sciences Division. The editing and preparation of the manuscript master was performed by the NASA/MSFC organization.

The co-chairmen express their gratitude to all RRAC members and their respective colleagues who have made significant technical contributions to the establishment of these RRAs.

Special thanks are tendered to Lt. B. Novogard for his diligence in performing the many computations and the development of the primary Tables, I through IV. Special thanks goes to Lt. F. Wirsing for editing and formulating the equations for the derivable thermodynamic equations. These gentlemen performed this outstanding work under the direction of Major B. Lilius, USAFETAC.

Grateful acknowledgment goes to Mrs. Annette Tingle, NASA/MSFC, for editing the manuscript.

The RCC/MG Range Reference Atmosphere Committee consists of representatives from the U.S. Air Force, U.S. Army, National Aeronautics and Space Administration, U.S. Navy, and National Oceanographic and Atmospheric Administration. The committee members for the RRA for the first publication are:

- G. G. Boire, WSMC
- O. H. Daniel, ESMC
- R. de Violini, PMTC
- F. G. Finger, NOAA/NWS
- E. E. Fisher, HQ AFSC
- B. R. Hixon, PMTC
- J. M. Hobbie, KMR
- E. J. Keppel, AD
- S. F. Kubinski, WSMR
- F. J. Schmidlin, NASA/WFC
- O. E. Smith Co-Chairman, NASA/MSFC

Maj. B. W. Galusha Co-Chairman, USAF/ETAC The second of the second second

#### CHAPTER I. INTRODUCTION

#### A. Definition and Purpose of the Range Reference Atmosphere

#### A.1 Definition

A reference atmosphere is a statistical model of the Earth's atmosphere derived from upper-air measurements over a particular geographical location. Hence, the atmospheric models developed by the Range Reference Atmosphere Committee (RRAC) in response to a task by the Range Commander's Council/Meteorology Group (RCC/MG) and published by the Secretariat, Range Commander's Council (RCC) are called Range Reference Atmospheres (RRAs). This organization group, formerly called the Inter-Range Instrumentation Group/Meteorology Working Group (IRIG/MWG), published a series of RRAs during the period 1963 through 1974.

#### A.2 Purpose

A series of revised and expanded RRAs are to be published for locations of interest to the RCC. These publications are to serve as an authoritative reference source on certain upper air statistics and as atmospheric models for a particular range site (location). The technical usefulness of these documents for the ranges, range users, U.S. aerospace industries, and the scientific community is recognized because of the standardization of the development techniques and the presentation of the tabulations.

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#### B. Scope of the Range Reference Atmosphere and Arrangement of Tables

#### B.1 Scope

The RRA contains tabulations for monthly and annual means, standard deviations, skewness coefficients for wind speed, pressure temperature, density, water vapor pressure, virtual temperature, dew-point temperature, and the means and standard deviations for the zonal and meridional wind components and the linear (product moment) correlation coefficient between the wind components. These statistical parameters are tabulated at the station elevation and at 1 km intervals from sea level to 30 km and at 2 km intervals from 30 to 90 km altitude. The wind statistics are given at approximately 10 m above the station elevations and at altitudes with respect to mean sea level thereafter. For those range sites without rocketsonde measurements, the RRAs terminate at 30 km altitude or they are extended, if required, when rocketsonde data from a nearby launch site are available. There are four sets of tables for each of the 12 monthly reference periods and the annual reference period.

#### B.2 Arrangement of Tables

The statistical parameters for the RRA models are presented in four tables.

Table I contains all the wind statistical parameters. This table gives the monthly and annual means and standard deviations of the zonal and meridional wind components and the linear (product moment) correlation coefficient between these two components; the mean, standard deviation and skewness coefficient of the wind speed; and the number of wind observations (sample size).

Table II contains the monthly and annual means, standard deviations, and skewness values of pressure, temperature, and density, and the number of observations used for each of these thermodynamic quantities.

Table III contains the monthly and annual means, standard deviations and skewness values of the water vapor pressure, virtual temperature and dew point, and the number of observations for each of these moisture-related quantities. The statistical parameters for water vapor pressure and dew point terminate at 15 km altitude. Above 15 km the statistical parameters for virtual temperature are considered to be the same as those for temperature.

Table IV contains the monthly and annual mean atmospheric models for the thermodynamic variables: pressure, virtual temperature, and density. This table is derived from the monthly and annual mean virtual temperature versus altitude (geometric) using the hydrostatic equation and the equation of state. Also presented is the geopotential height corresponding to the tabulated geometric altitudes.

The physical unit for all wind parameters is m/s. The physical unit for pressure is mb; for temperature and virtual temperature, K; for density, gm/m³; and for water vapor pressure, mb. In all cases the skewness coefficient and the correlation coefficient between wind components are unitless. All reference to altitude is geometric altitude and has the unit km. All reference to height is geopotential height and has the unit geopotential m or km. All geometric altitudes and geopotential heights are with respect to mean sea level.

#### C. Data Quality Control Procedures

A small proportion (less than 10 percent) of the soundings in the data base used to calculate the RRA tables contained erroneous data values. The soundings which contained these erroneous values were eliminated from the data base using the following procedures:

- 1) Soundings containing gaps in their height data greater than 200 mb were rejected. This step was taken because some soundings only contained height values at their "mandatory" pressure levels, which were occasionally missing, resulting in soundings with no height information at all.
- 2) An initial set of RRA statistics was computed using all the remaining soundings. This initial set of statistics was used to determine data limits for the temperature, pressure. U and V components of the wind, and the dew point (for the 0-30 km portion of the RRA) or the density (for the

30-90 km portion of the RRA). The lower (upper) data limits were set at the mean value for a specific parameter, minus (plus) six standard deviations of that quantity. One pair of data limits was computed for each of these parameters, month of the year and data level.

- 3) This initial set of data limits was then used to screen the data base. All the soundings which contained values outside these data limits were rejected. A new RRA was then computed using the screened data base. This second RRA was used to generate a second set of data limits.
- 4) The second set of data limits was then used to screen the data base further. A new RRA was again generated. The skewness values in this RRA were then evaluated according to empirical criteria specified in Section II.A.3 of this document for the winds and according to criteria in Section III.A.3 for the thermodynamic quantities. If these criteria were satisfied, the new RRA was then used to generate a final set of data limits, which were used to quality control the data base for the final version of the RRA.
- 5) Occasionally, the third RRA which was generated did not satisfy all of the skewness criteria. This indicated that some incorrect values were still present in the data base. To complete quality control, the data limits-to-RRA-to-data-limits cycle was continued for additional iterations (usually one or two) until the resulting RRA satisfied the skewness criteria. At that point, a final set of data limits was generated. This final set of data limits was then used to quality control the data base and generate the final RRA.

#### D. Organization of the Chapters

Because there are plans to publish a series of RRAs, comments on the special organization of the document are in order. The RRA cocument is arranged in four chapters. Chapter I is the Introduction. Chapter II. Wind Statistics and Models, contains the techniques used to arrive at the wind statistical parameters, Table I, and the probability functions which are to be used as wind models to derive several wind statistics. Chapter III, Statistics of Thermodynamic Quantities and Models, contains the techniques used to arrive at the thermodynamic and moisture-related statistical parameters given in Tables II and III and the atmospheric thermodynamic model presented in Table IV. This chapter also contains sets of equations to calculate several atmospheric properties. Chapter IV contains the general conclusions and recommendations. These four chapters are reprinted without change for each documented RRA to assure consistency and for expediency in preparing the documentation. To account for variations particular to a specific RRA, two appendixes have been included. Appendix A, Examples of Wind Statistics, is designed to give a few illustrative examples of wind statistics for the specific RRA and cursory observations, comparisons, or comments on wind statistics. Appendix B, Range Specific Information, is designed to present specific information particular to the range, such as geographical location, data base, etc., and any cursory observations or comments on the thermodynamic quantities.

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Read these appendixes! They are located as the last two units in the document because they may vary in length depending on the circumstances. Appendixes A and B and the principal Tables I, II, III, and IV are the only changes to be made to each RRA document published in this new RRA series.

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#### CHAPTER II. WIND STATISTICS AND MODELS

#### A. General Considerations

#### A.1. Objectives

An objective of the RRA is to furnish minimum tabulation for the wind statistics. To meet this objective, the bivariate normal probability distribution was adopted as a statistical model for the wind treated as a vector quantity at the RRA data levels. Only five statistical parameters are required to completely describe this probability function. In Cartesian coordinates these parameters are the means and standard deviations of the two orthogonal components and the correlation coefficient between the two components. These five statistical parameters for the zonal and meridional (meteorological coordinates) components are given in Table I. The statistical properties of the bivariate normal probability distribution are used to derive many wind statistics that are of interest to the ranges and range users. This procedure produces consistent wind statistics that are connected through rigorous mathematical probability functions. By using these functions, extensive tabulations of wind statistics are avoided.

The statistical properties of the bivariate normal probability distribution presented for the vector wind statistical model are:

- 1) The wind components are univariate normally distributed.
- 2) The conditional distribution of one component given a value of the other component is univariate normally distributed.
- 3) The wind speed is of the form of a generalized Rayleigh distribution.
  - 4) The frequency distribution of wind direction can be derived.
- 5) The conditional distribution of wind speed given a value of wind direction (wind rose) can be derived.
- 6) The five tabulated wind statistical parameters which are with respect to the meteorological zonal and meridional coordinate system can be derived for any arbitrary rotation of the orthogonal axes.

The probability distribution functions and sets of equations to derive wind statistics for the previously stated properties of the vector wind model are presented. Illustrative examples are presented in Appendix A. No attempt is made to give the derivation of the probability functions. The reader is referred to Smith (1976) for some derivations and several applications of the probability distribution properties for wind statistics.

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#### TABLE A. LIST OF SYMBOLS USED IN CHAPTER II

- N The number of wind measurements in Table I
- r A general variable for the bivariate normal probability distribution in polar coordinates
- R A generalized Rayleigh variable used for derived wind speed probability distribution
- R (U, V) The linear (product moment) correlation coefficient between the zonal and meridional wind components in Table I
- SK (W) Skewness parameter for wind speed in Table I
- S (U) The standard deviation of the zonal wind component in Table I
- S (V) The standard deviation of the meridional wind component in Table I
- S (W) The standard deviation of wind speed in Table I
- t A standardized normal variate used in text Table A
- U The zonal wind component
- UBAR The mean value of the zonal wind component in Table I
- V The meridional wind component
- $VBAR\mbox{ -}$  The mean value of the meridional wind component in Table I
- W Wind speed or modulus of wind vector, a scalar quantity
- WBAR The mean value of wind speed in Table I
- X A general component variable or coordinate axes
- Y A general component variable or coordinate axes
- $\overline{X}$  A general component mean value in the [x,y] coordinate system
- $\overline{Y}$  A general component mean value in the [x,y] coordinate system
- α (alpha) Rotation angle for the [x,y] coordinate system

#### TABLE A. (Concluded)

- $\theta$  (theta) Wind direction in the polar coordinate system
- $\lambda_{\mbox{\scriptsize ()}}$  (Lambda) A parameter in the bivariate normal probability distribution in text Table B
- $\xi$  (Xi) The mean value in the standardized normal probability distribution used in text Table A
- $\pi$  (Pi) Constant = 3.14159 ...
- ρ (Rho) The general linear correlation coefficient between the two component variables in the [x,y] coordinate system
- $\sigma_x, \sigma_y$  The general standard deviations of the x and y component variables in the [x,y] coordinate system.

#### A.2. Data Quality Control

The U and V components of the wind were used to generate data limits which were set at plus and minus six standard deviations from the mean for each of the quantities. These data limits were used to screen the wind data base, as described in Section I.C. The data base was considered to be free from errors if:

- 1) The skewness of the wind speed was below 4.0 at data levels where the mean wind speed was less than 15 m/s, and
- 2) The skewness of the wind speed was below 2.5 at data levels where the mean wind speed was greater than 15 m/s.

#### A.3. Limitations

For the wind statistics, the correlation coefficients for like wind components and unlike wind components between altitude levels were not computed. Therefore, wind statistics with respect to altitude (profile) cannot be derived from the RRA statistics. For wind profile modeling techniques the user is referred to Smith (1976). However, the wind statistics at discrete altitudes are valid; all of the probability distribution functions given in Chapter II can be derived from the five wind component statistical parameters contained in Table I, and the derived distributions can be considered as wind models at discrete altitudes.

By convention, in the statistical literature Greek letters are used for population or theoretically known parameters, and sample estimates are denoted by English alphabetical letters or with a "hat" (,) over the Greek letters. In Chapter II Greek letters are used for the variances and the linear correlation coefficient, and the means are denoted by  $\overline{X}$  and  $\overline{Y}$  when dealing with the bivariate normal distribution. It will always be understood that Table I contains sample estimates of the statistical parameters and they are with respect to the meteorological zonal (U) and meridional (V) coordinate system.

#### B. Coordinate System and Computation of Statistical Parameters

#### B.1. Coordinate System

Wind measurements are recorded in terms of magnitude and direction. The wind direction is measured in degrees clockwise from true north and is the direction from which the wind is blowing. The wind magnitude (the modulus of the vector) is the scalar quantity and is referred to as wind speed or scalar wind. A statistical description that accounts for the wind as a vector quantity is appropriate and requires a coordinate system.

For the RRA the standard meteorological coordinate system has been chosen for the wind statistics, all tables of statistical parameters, and related discussions because the coordinate system used in aerospace and related applied fields has not always been consistent.

Using Figure 1, the polar and Cartesian forms for the meteorological coordinate system are defined:

- W = wind speed, scalar wind, or magnitude of the wind vector in m/s.
- $\theta$  = wind direction.  $\theta$  is measured in degrees clockwise from true north and is the direction from which the wind is blowing.

- U = zonal wind component, positive west to east in m/s.
- V = meridional wind component, positive south to north in m/s.

The components  $\boldsymbol{\theta}$  and W define the polar form, and the U-V components define the Cartesian forms:

$$U = -W \sin\theta \quad , \quad 0 < \theta < 360^{\circ}$$
 (1)

$$V = -W \cos\theta \qquad . \tag{2}$$

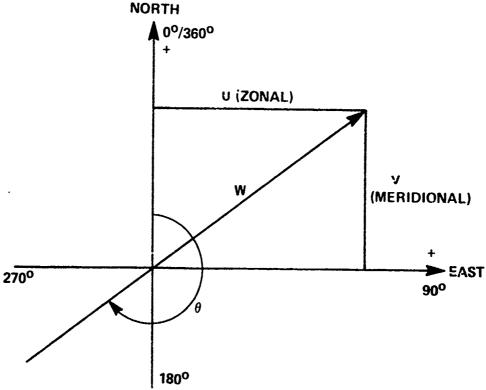


Figure 1. The meteorological coordinate system.

It is helpful to note the difference between the mathematical convention for a vector direction and the meteorological convention for wind direction, viz.:

$$\theta \text{ met} = 270 - \theta \text{ math} \tag{3}$$

when  $0 \le \theta \le 270$  degrees

$$\theta$$
 met = 360 + (270 -  $\theta$  math)

when  $270 \le \theta < 360$  degrees.

#### B.2. Computation of Statistical Parameters

The wind statistical parameters in Table I for the means and standard deviations of the zonal and meridional wind components and wind speed and the skewness parameter of wind speed were computed using the sums technique presented in Chapter III.C.3. In addition, the linear (product moment) correlation coefficient between the zonal and meridional wind components, r (u,v) in Table I, was computed. This correlation coefficient is defined as

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$$r (u,v) = \frac{\sum_{i=1}^{n} (U_i - \overline{U}) (V_i - \overline{V})}{N s(u) \cdot s(v)} . \tag{4}$$

These statistical parameters are with respect to the Standard Meteorological Coordinate System.

#### C. Statistical Wind Models

#### C.1. Wind Componer Statistics

The univarimormal (Gaussial) probability distribution function is used to obtain wind component statistics. In generalized notations, this probability density function (pdf) is

$$f(t) = \frac{\frac{t^2}{2}}{\sqrt{2\pi}}, \qquad (5)$$

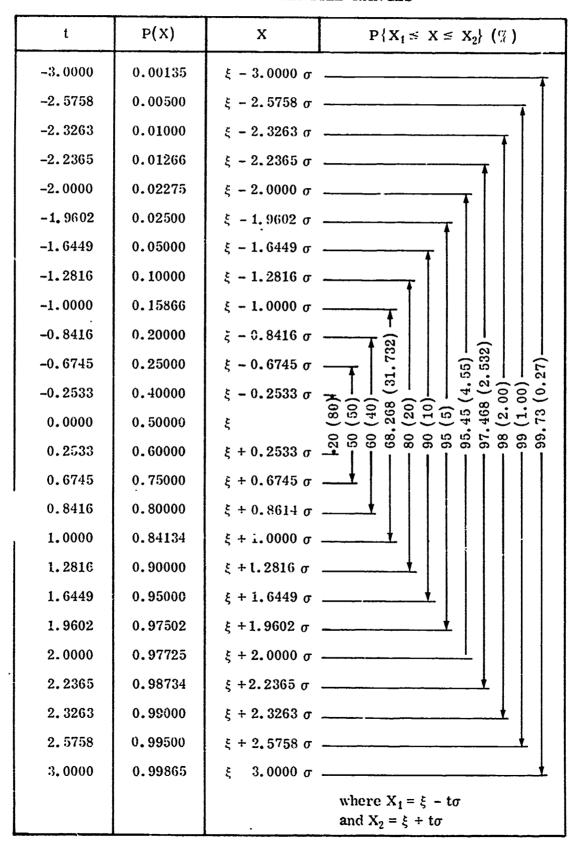
where  $t = X - \xi/\sigma_X$  is the standardized variate with  $\xi$  defining the mean and  $\sigma_X$  the standard deviation. The probability distribution function (PDF) is

$$F(t) = \int_{-\infty}^{t} f(t) dt . \qquad (6)$$

Because this integral cannot be obtained in closed form, it is widely tabulated for zero mean and unit standard deviation. For a convenient reference for the RRA, selected values of F(t) are given in Table B. To emphasize the connotation of probability, F(t) is shown in Table B as  $P\{X\}$ . The t values in Table B are used as multiplier factors to the standard deviation to express the probability that a normally distributed variable, X, is less than or equal to a given value as

$$P\{X \leq \text{mean} + t \sigma_X\} = \text{probability, p}$$
 (7)

TABLE B. VALUES OF t FOR STANDARDIZED NORMAL (UNIVARIATE) DISTRIBUTION FOR PERCENTILES AND INTERPERCENTILE RANGES



For example, when t=1.6449, the probability that X is less than or equal to the mean plus 1.6449 standard deviations is 0.95. That value of X which is less than or equal to the mean plus 1.6449 standard deviations is called the 95th percentile value of X. Also given in Table 2 are the numerical values to express the probability that X falls in the interval  $X_1$  and  $X_2$ ; i.e.,

$$P\left\{X_{1} \leq X \leq X_{2}\right\} = \text{Interpercentile Range}$$
 where 
$$X_{1} = \overline{X} - t \sigma_{X}$$
 
$$X_{2} = \overline{X} + t \sigma_{X}$$
 (8)

For t = 1.9602 the probability that X lies in the interval  $X_1$  and  $X_2$  is 0.95. The values of  $X_1$  and  $X_2$  in this example comprise the 95th interpercentile range.

For a normally distributed variable, the mode (most frequent value) and the median (50th percentile value) are the same as the mean value. The means and standard deviations of the zonal and meridional wind components from Table I are used in equations (7) and (8) to compute the percentile values and interpercentile ranges of the zonal and meridional wind components. When equation (7) is illustrated on a normal probability graph, a straight line is formed.

#### C.2. The Vector Wind Model

Because wind is a vector quantity having direction and magnitude which can be expressed as two components in an orthogonal coordinate system, a probability model which describes the joint relationship is the bivariate normal probability distribution. In general component notation, the bivariate normal probability density function (BNpdf) is

$$f(X,Y) = \frac{1}{2\pi\sigma_{X}\sigma_{y}} \sqrt{1-\rho^{2}} \left[ \exp \frac{-1}{2(1-\rho^{2})} \left\{ \frac{(X-\overline{X})^{2}}{\sigma_{X}^{2}} - \frac{2\rho(X-\overline{X})(Y-\overline{Y})}{\sigma_{X}\sigma_{y}} + \frac{(Y-\overline{Y})^{2}}{\sigma_{y}^{2}} \right\} \right] - \infty \leq X \leq \infty \text{ and}$$

$$-\infty \leq Y \leq \infty . \tag{9}$$

where the five parameters are  $\bar{x}, \bar{y}$ , the component means,  $\sigma_{x}, \sigma_{y}$ , the component standard deviations, and  $\rho$ , the correlation coefficient between the two component variables. X and Y.

For many applications the interest is in determining the probability that a point  $\{X,Y\}$  will fall within a contour of equal probability density. The exponential terms of equation (9), when set equal to a constant,  $\lambda^2$ , give a family of ellipses depending on the value of the constant. The ellipses have a common center at the point  $\{\overline{X},\overline{Y}\}$ . Integration of equation (9) over the region bounded by the contours of equal probability density gives

$$P(\lambda) = 1 - e^{\frac{-\lambda^2}{2(1 - \rho^2)}} . (10)$$

Solving for  $\lambda^2$  and replacing  $P(\lambda)$  by p gives

$$\lambda^2 = -2 (1 - \rho^2) \ln (1 - p) . \tag{11}$$

Now define

$$\lambda_{p} = \sqrt{2} \sqrt{-\ln (1-p)} \quad . \tag{12}$$

For ready reference and comparisons,  $\boldsymbol{\lambda}_{e}$  is shown in Table C for selected values of p.

The probability ellipse that contains p-percent of the wind vectors expressed in the most general form is the conic defined by

$$AX^2 + BXY + CY^2 + DX + EY + F = 0$$
, (13)

where

$$A = \sigma_{v}^{2}$$

$$B = -2\rho\sigma_{\mathbf{x}}\sigma_{\mathbf{y}}$$

TABLE C. VALUES OF  $\lambda$  FOR BIVARIATE NORMAL DISTRIBUTION ELLIPSES AND CIRCLES

	λ <sub>c</sub>	λ <sub>c</sub>		λ	λ <sub>c</sub>
P(°; )	(ellipse)	(circle)	P("; )	(ellispe)	(circle)
0.000	0.0000	0.0000	65.000	1.4490	1.0246
5.000	0.3203	0.2265	68.268	1.5151	1.0713
10.000	0.4590	0.3246	70.000	1.5518	1.0973
15.000	0.5701	0.4031	75,000	1.6651	1.1774
20,000	0.6680	0.4723	80.000	1.7941	1.2686
25.000	0.7585	0.5363	85.000	1.9479	1.3774
30.000	0.8446	0.5972	86.466	2.0000	1.4142
35.000	0.9282	0.6563	90.000	2.1460	1.5175
39.347	1.0000	0.7071	95.000	2.4477	1.7308
40.000	1.0108	0.7147	95, 450	2.4860	1.7579
45.000	1.0935	0.7732	98.000	2.7971	1.9778
50.000	1.1774	0.8325	98.168	2.8284	2.0000
54.406	1.2533	0.8862	98.889	3.0000	2.1213
55.000	1.2637	0.8936	99.000	3.0348	2. 1460
60.000	1.3537	0.9572	99.730	3, 4393	2.4320
63, 212	1.4142	1.0000	99.9877	4.2426	3,0000

$$\lambda_{e} = \sqrt{2} \sqrt{-\ln (1 - P)}$$

$$\lambda_{c} = \sqrt{-\ln(1-P)}$$

$$C = \sigma_{x}^{2}$$

$$D = 2\sigma_{\mathbf{X}}\sigma_{\mathbf{y}} \circ \overline{\mathbf{Y}} - 2\sigma_{\mathbf{y}}^{2}\overline{\mathbf{X}} = -(B\overline{\mathbf{Y}} + 2A\overline{\mathbf{X}})$$

$$\mathbf{E} = 2\sigma_{\mathbf{X}}\sigma_{\mathbf{V}} \circ \overline{\mathbf{X}} - 2\sigma_{\mathbf{X}}^{2}\overline{\mathbf{Y}} = -(\mathbf{B}\overline{\mathbf{X}} + 2\mathbf{C}\overline{\mathbf{Y}})$$

$$F = A\overline{X}^2 + C\overline{Y}^2 + B\overline{X}\overline{Y} - AC (1 - \rho^2) \lambda_e^2$$

and

$$\lambda_{\rho} = \sqrt{2} \sqrt{-\ln (1 - \rho)} \quad .$$

For graphical presentations the range of the variable is important in order to arrange the scale. The largest and smallest values of X and Y for a given probability ellipse, p, are given by

$$X_{L,S} = \overline{X} \pm \sigma_{X} \lambda_{e}$$
 (14)

$$Y_{L,S} = \overline{Y} \pm \sigma_{y}^{\lambda} \lambda_{e} , \qquad (15)$$

where, as before,  $\lambda_e = \sqrt{2} \sqrt{-\ln (1-p)}$ 

Although there are several approaches to graphing the probability ellipses, the following procedure is advantageous for electronic computer plotting. In establishing the computer plotting program, the sample estimates for  $\overline{X}, \overline{Y}, \sigma_X, \sigma_y$ , and  $\rho$  are constants in equation (13). The user makes the choice of probability ellipses desired. Thus, p in equation (12) is programmed as a parameter. The largest and smallest values for X and Y are computed by equations (14) and (15) for the largest probability ellipse selected. This sets the graphical scale. Values of X within the range of X smallest to X largest are obtained by incrementing X between these limits. Using the quadratic equation, a solution of equation (13) is made for Y for each value of X and plotted. The centroid  $(\overline{X}, \overline{Y})$  for the family of probability ellipses is plotted as a point. Labeling and other identification completes the plotting program.

For a given probability, equation (13) defines an ellipse which contains p-percent of the points X,Y. Since the entire area under the bivariate normal density function [equation (9)] is unity, upon integration for a given probability ellipse, that given ellipse contains p-percent of the total area. In the wind statistics p-percent of the wind vectors fall within the specified probability ellipse. From this point of view, a specified probability ellipse gives the joint probability that p-percent of the U-V components lie within the given ellipse.

When  $\sigma_{X}^{2} = \sigma_{y}^{2} = \sigma^{2}$  and  $\rho = 0$  in the bivariate normal distribution, the probability ellipses of equation (13) reduce to circles whose centers are at the means  $\overline{X}, \overline{Y}$ . The radii of the probability circles are  $\sigma_{V1}^{\lambda}$  where

$$c_{\text{V1}} = \sqrt{2\sigma^2} \tag{16}$$

and

$$\lambda_{\mathbf{c}} = \sqrt{-\ln (1 - \mathbf{p})} \quad . \tag{17}$$

Values for  $\ _{\mathbf{c}}$  for selected probabilities, p, are given in Table 3.

Because this function is simple, it can be easily graphed manually. However, the generalized plotting technique for electronic computer plotters as represented by equation (13) can be advantageously used.

#### C.3. Derived Distributions for Wind Statistics

In this subsection the probability distribution functions and sets of equations are presented to derive certain probability distribution functions for wind statistics. These derived probability distributions are:

- 1) The conditional distribution of wind components
- 2) The generalized Rayleigh distribution for wind speed
- 3) The distribution for wind direction
- 4) The conditional distribution of wind speed given a wind direction (wind rose).

The required five statistical parameters for these derived distributions for wind statistics are given in Table I.

### C.3.1. The Conditional Distribution of Wind Components

Given that two random variables X and Y are bivariate normally distributed, the conditional distribution f(Y|X) is read as f(Y) given X, and likewise f(X|Y) is read as f(X) given Y. The conditional probability distribution function F(Y|X) has the mean E(Y|X) and variance  $\sigma^2(x|y)$ , where

$$E(Y | X^*) = \overline{Y} + \rho \left( \frac{\sigma_y}{\sigma_x} \right) (X^* - \overline{X})$$
 (18)

and

$$\sigma^2_{(y|x^*)} = \sigma_y^2 (1 - \rho^2)$$
 (19)

The conditional standard deviation is

$$\sigma_{(\mathbf{y}\,|\,\mathbf{x}^*)} = \sigma_{\mathbf{y}} \sqrt{1 - \rho^2} \quad . \tag{20}$$

By interchanging the variables and parameters, the conditional distribution function for  $F(X|Y^*)$  has the conditional mean

$$E(X | Y^*) = \overline{X} + \rho \left( \frac{\sigma_x}{\sigma_y} \right) (Y^* - \overline{Y}) , \qquad (21)$$

conditional variance

$$\sigma^{2}(x|y^{*}) = \sigma_{x}^{2} (1 - \rho^{2}) , \qquad (22)$$

and conditional standard deviation

$$\sigma_{(\mathbf{x}\,|\,\mathbf{y}^*)} = \sigma_{\mathbf{x}} \sqrt{1-\rho^2} \quad . \tag{23}$$

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The preceding conditional probability distribution functions are univariate normal distributions for a (fixed) given value for one of the bivariate normal variables. Thus the t-values given in Table 2 are applicable for conditional probabilities statements. For example,

$$F(Y|X^*) = E(Y|X^*) + t\sigma_{(Y|X^*)}$$
 (24)

For t = 1.6449 there is a 95 percent chance that Y is less than or equal to  $\overline{Y}$  + 1.6449  $\sigma_{(y|x^*)}$  given that X = X\*. In symbols this statement reads

$$P\left\{Y \leq E(Y|X^*) + 1.6449 \ \sigma_{(y|X^*)} \ | X = X^*\right\} = 0.9500 \ . \tag{25}$$

Interval probability statements can also be made; namely,

$$P \left\{ Y_1 = E(Y | X^*) - t\sigma_{(y | X^*)} \le Y \le Y_2 = E(Y | X^*) + t\sigma_{y} | X = X^* \right\}$$

where X\* can take on any fixed value of X, but a convenient arrangement is to let X\* =  $\overline{X} \pm t\sigma_{X}$ .

The close connection of the regression function of Y on X to the conditional mean for the bivariate normal distribution is noted; namely,

$$Y = \overline{Y} + \rho \left( \frac{\sigma_{y}}{\sigma_{x}} \right) (X - \overline{X}) . \qquad (26)$$

Similarly, the regression function of X on Y is

$$X = \overline{X} + \rho \left(\frac{\sigma_{\mathbf{y}}}{\sigma_{\mathbf{x}}}\right) (Y - \overline{Y}) \qquad . \tag{27}$$

These are linear functions and express the same results as would be obtained from a least-squares regression line.

#### C.3.2. The Generalized Rayleigh Distribution for Wind Speed

If two random variables, X and Y, are bivariate normally distributed, then the probability distribution for the modulus, R, can be derived in terms of the five parameters which define the bivariate normal distribution.

$$R = \sqrt{X^2 + Y^2} \tag{28}$$

The distribution of R so derived is called a generalized Rayleigh distribution because there are no restrictions on the parameters. For applications to the RRA, the variable R is recognized as wind speed or the modulus of the wina vector.

The probability density function for R is expressed as

$$f(R) = a_0^R e^{-a_1^R^2} \left[ I_0(a_2^R^2) I_0(a_3^R) + 2 \sum_{k=1}^{\infty} I_k(a_2^R^2) I_{2k}(a_3^R) \cos 2k\psi \right] R \ge 0 .$$
 (29)

The functions,  $I_0(\cdot)$ ,  $l_k(\cdot)$ , and  $I_{2k}(\cdot)$  are the modified Bessel function of the first kind for zero order, kth order, and 2kth order. The coefficients are:

$$\mathbf{a_0} = \exp \left[ -\frac{1}{2} \left\{ \frac{\overline{\mathbf{X}}^2}{\sigma_{\mathbf{a}}^2} + \frac{\overline{\mathbf{Y}}^2}{\sigma_{\mathbf{b}}^2} \right\} \right] / \sigma_{\mathbf{a}} \sigma_{\mathbf{b}} \quad ,$$

where  $\sigma_a^2$  and  $\sigma_b^2$  are the rotated variances to produce zero correlation between X and Y.  $\sigma_a$  and  $\sigma_b$  are the positive and negative roots of the expression

$$\sigma^{2}_{(+,-)} = \frac{1}{2} \left\{ \sigma_{x}^{2} + \sigma_{y}^{2} \pm \left[ (\sigma_{x}^{2} + \sigma_{y}^{2})^{2} - 4\sigma_{x}^{2} \sigma_{y}^{2} (1 - \rho^{2}) \right]^{1/2} \right\}$$

$$a_1 = (\sigma_x^2 + \sigma_y^2)/4(1 - \rho^2) \sigma_x^2 \sigma_y^2$$
,

<sup>1.</sup> See footnote on next page.

$$a_{2} = \frac{\left[\left(\sigma_{x}^{2} - \sigma_{y}^{2}\right)^{2} + 4\rho^{2}\sigma_{x}^{2}\sigma_{y}^{2}\right]^{1/2}}{4(1 - \rho^{2}) \sigma_{x}^{2}\sigma_{y}^{2}}$$

$$a_3 = \left[ \left( \frac{\overline{X}}{\sigma_a^2} \right)^2 + \left( \frac{\overline{Y}}{\sigma_b^2} \right)^2 \right]^{1/2} ,$$

and

$$\tan \psi = \frac{\overline{Y}}{\overline{X}} \frac{\sigma_a^2}{\sigma_b^2} \quad .$$

Since this density function cannot be integrated in closed form from zero to R, numerical integration is used to obtain practical results for the probability distribution function; i.e.,

$$F(R) = \int_{0}^{R*} f(R) dR \qquad . \tag{30}$$

A number of special cases can be obtained from the general Rayleigh distribution [equation (29)], the most simple of which is to let  $\sigma_{X} = \sigma_{y} = \sigma_{y}$  and  $\overline{X} = \overline{Y} = 0$  with independent variables X and Y. This gives

# 1. This computational form is obtained from the determinant

$$\begin{bmatrix} \sigma_{\mathbf{x}}^2 - K & \sigma_{\mathbf{x}}^2 \sigma_{\mathbf{y}} \rho \\ \\ \sigma_{\mathbf{x}}^2 \sigma_{\mathbf{y}} \rho & \sigma_{\mathbf{y}}^2 - K \end{bmatrix},$$

where K is  $\sigma^2_{(+,-)}$ , and  $\sigma_a$  and  $\sigma_b$  are analogous to the standard deviation of the major and minor axes of the bivariate nermal probability ellipse.

$$f(R) = \frac{R}{\sigma^2} e^{-R^2/2\sigma^2} , \qquad (31)$$

which is recognized as the classical Rayleigh probability density function. The density function, equation (31), can be integrated in closed form over any range of the variable R. Hence, the probability distribution function, F(R), for equation (31) is

$$F(R) = 1 - \exp\left\{\frac{-R^2}{2\sigma^2}\right\} . \tag{32}$$

#### C.3.3. The Derived Distribution of Wind Direction

Considering the wind as a vector quantity and bivariate normally distributed, the wind direction can be derived. This is done by first writing the bivariate normal probability density function in polar coordinates whose variables are

$$g(r,\theta) = rd_1 e^{-\frac{1}{2}(a^2r^2 - 2br + c^2)}$$
, (see footnote 2) (33)

where

$$a^{2} = \frac{1}{(1 - \rho^{2})} \left[ \frac{\sin^{2} \theta}{\sigma_{\mathbf{x}}^{2}} - \frac{2\rho \cos \theta \sin \theta}{\sigma_{\mathbf{x}}^{2} \sigma_{\mathbf{y}}} + \frac{\cos^{2} \theta}{\sigma_{\mathbf{y}}^{2}} \right]$$

$$b = \frac{-1}{(1 - \rho^2)} \left[ \frac{\overline{x} \sin \theta}{\sigma_x^2} - \frac{\rho(\overline{x} \cos \theta + \overline{y} \sin \theta)}{\sigma_x^2 \sigma_y} + \frac{\overline{y} \cos \theta}{\sigma_y^2} \right]$$

$$c^{2} = \frac{1}{(1 - \rho^{2})} \left[ \frac{\overline{x}^{2}}{\sigma_{x}^{2}} - \frac{2\rho \overline{x} \overline{y}}{\sigma_{x}^{2} \sigma_{y}} + \frac{\overline{y}^{2}}{\sigma_{y}^{2}} \right]$$

<sup>2.</sup> This expression, equation (33), in Smith (1976) is given with respect to the mathematical convention for a vector direction.

$$d_1 = \frac{1}{2\pi\sigma_{\mathbf{X}}\sigma_{\mathbf{V}}\sqrt{1-\rho^2}}$$

and  $r = \sqrt{x^2 + y^2}$  is the modulus of the vector or speed and  $\theta$  is the direction of the vector. After integrating  $g(r,\theta)$  over r = 0 to  $\infty$ , the probability density function of  $\theta$  is

$$g(\theta) = \frac{d_1}{a^2} e^{-\frac{1}{2}c^2} \left[ 1 + \sqrt{2\pi} \left( \frac{b}{a} \right) e^{\frac{1}{2} \left( \frac{b}{a} \right)^2} \phi \left( \frac{b}{a} \right) \right] , \quad (34)$$

where  $a^2$ , b,  $c^2$ , and  $d_1$  are as previously defined in equation (33) and

$$\Phi\left(\frac{b}{a}\right) = \Phi\left(\mathbf{x}\right) = \frac{1}{\sqrt{2\pi}} \cdot \int_{-\infty}^{x} e^{-\frac{1}{2}t^2} dt$$

is taken from tables of normal distribution functions or made available through a computer subroutine.

If desired, equation (34) can be integrated numerically over a chosen range of  $\theta$  to obtain the probability that the vector direction will lie within the chosen range; i.e.,

$$F(\theta) = \int_{\theta_2}^{\theta_1} g(\theta) d\theta . \qquad (35)$$

One application may be to obtain the probability that the wind will flow from a given quadrant or sector as, for example, onshore.

C.3.4. The Derived Conditional Distribution of Wind Speed Given the Wind Direction (Wind Rose)

Continuing with the considerations in Section C.3.3. of this chapter, the conditional probability density function (pdf) for wind speed, r, given a specified value for the wind direction,  $\theta$ , can be expressed as

$$f(\mathbf{r}|\theta) = \frac{a^2 \mathbf{r} e^{-\frac{1}{2} (a^2 \mathbf{r}^2 - b\mathbf{r})}}{1 + \sqrt{2\pi} \left(\frac{b}{a}\right) e^{\frac{1}{2} \left(\frac{b}{a}\right)^2} \Phi\left\{\frac{b}{a}\right\}},$$
(36)

where the coefficients, <u>a</u> and <u>b</u> and the function  $\Phi\left\{\frac{b}{a}\right\}$  are as previously defined in equation (33) and in equation (34).

From equation (36) the mode (most frequent value) of the conditional wind speed given a specified value of the wind direction is the positive solution of the quadratic equation,

$$a^2 r^2 - br - 1 = 0$$
 , (37)

which is

$$(\tilde{\mathbf{r}}\mid\theta) = \frac{1}{2a}\left[\left(\frac{\mathbf{b}}{\mathbf{a}}\right) + \sqrt{4 + \left(\frac{\mathbf{b}}{\mathbf{a}}\right)^2}\right] \qquad . \tag{38}$$

The locus of the conditional modal values of wind speed when plotted in polar form versus the given wind directions orms an ellipse.

The noncentral moment for equation (36) is expressed as

$$\mu_n' = \int_0^\infty \mathbf{r}^n \mathbf{f}(\mathbf{r}|\theta) d\mathbf{r} . \qquad (39)$$

Now the first noncentral moment is identical to the first central moment or the expected value, E  $(r \mid \theta)$ . The integration of equation (39) for the first moment is sufficiently simple to yield practical computations and can be expressed as

$$E(\mathbf{r}|0) = \frac{\left(\frac{\mathbf{b}}{\mathbf{a}}\right) + \left[1 + \left(\frac{\mathbf{b}}{\mathbf{a}}\right)^{2}\right] \sqrt{2\pi} e^{\frac{1}{2}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)^{2}} + \left\{\frac{\mathbf{b}}{\mathbf{a}}\right\}}{a\left[1 + \left(\frac{\mathbf{b}}{\mathbf{a}}\right) \sqrt{2\pi} e^{\frac{1}{2}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)^{2}} + \left\{\frac{\mathbf{b}}{\mathbf{a}}\right\}\right]} \qquad (40)$$

Hence, equation (40) gives the conditional mean value of the wind speed given a specified value for the wind direction.

The integration of equation (36) for the limits r=0 to  $r=r^*$  gives the probability that the conditional wind speed is  $\leq r^*$  given a value for the wind direction,  $\theta$ . This conditional probability distribution (PDF) can be written as

$$\Pr\left\{\mathbf{r} \leq \mathbf{r}^* \mid \theta = \theta_0\right\} = 1 - \left[\frac{e^{-\frac{1}{2}\mathbf{r}_S^2 + \sqrt{2\pi}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)\left\{1 - \Phi\left(\mathbf{r}_S\right)\right\}}}{e^{-\frac{1}{2}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)^2 + \sqrt{2\pi}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)\Phi\left(\frac{\mathbf{b}}{\mathbf{a}}\right)}}\right], \quad (41)$$

where 
$$r_s = \left[ a r^* - \left( \frac{b}{a} \right) \right]$$

By definition equation (41) is an expression for a "wind rose". Empirical wind rose statistics are often tabulated or graphically illustrated giving the frequency that the wind speed is not exceeded for those wind speed values which lie within assigned class intervals of the wind direction. After evaluation of equation (41) for various values of wind speed,  $r^*$ , and the given wind directions,  $\theta$ , interpolations can be performed to obtain various percentile values of the conditional wind speed.

For the special case when b in equation (33) (i.e., for  $\bar{x} = \bar{y} = 0$ ), the conditional modal values of wind speeds [equation (38)], the conditional mean values of wind speeds [equation (40)], and the fixed conditional percentile values of wind speeds [interpolated from evaluations of equation (41)], when plotted in polar form versus the given wind directions produce a family of ellipses.

For the special case when  $\bar{x} = \bar{y} = 0$ , equation (36) reduces to the following simple case:

$$\Pr\left\{\mathbf{r} \leq \mathbf{r}^* \mid \theta = \theta_0\right\} = 1 - e^{-\frac{\mathbf{a}^2 \mathbf{r}^2}{2}}$$
 (42)

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There is a special significance of equation (42) when related to the bivariate normal probability distribution. If  $r^*$  and  $\theta$  are measured from the centroid of the probability ellipse, then the probability that  $r < r^*$  is the same as the given probability ellipse. Further, solving equation (42) for  $r^*$ , gives

$$r^* = \frac{1}{a} \sqrt{-2 \ln (1 - P)}$$
 (43)

If a probability ellipse P is chosen, equation (42) gives the distance of r along any  $\theta$  from the centroid of the ellipse to the intercept of the specified probability ellipse. If there is an interest in conditional probability of winds for a given  $\theta$  relative to the monthly means, equation (43) is applicable. If it is desired to find the magnitude of the wind along any  $\theta$  relative to the monthly mean to the intercept of a given probability ellipse, equation (43) is applicable.

#### D. Statistical Parameters With Respect To Any Orthogonal Axes

The five wind statistical parameters presented in Table I are given with respect to the standard meteorological coordinate system; i.e., these parameters are for the zonal and meridional components. For many aerospace vehicles and range applications there is a need for wind statistics with respect to orthogonal axes other than west to east and south to north. For example, it may be required to present wind statistics with respect to a flight azimuth of an aerospace vehicle whose flight azimuth is  $\alpha$  degrees from true north measured in a clockwise direction. The following sets of equations are presented to compute the five parameters for the new coordinate axes rotated  $\alpha$  degrees clockwise from true north.

a. Rotation of the means through  $\alpha$  degrees:

$$\overline{X}_{\alpha} = \overline{X} \cos (90 - \alpha) + \overline{Y} \sin (90 - \alpha)$$
 (44)

$$\overline{Y}_{\alpha} = \overline{Y} \cos (90 - \alpha) - \overline{X} \sin (90 - \alpha)$$
 (45)

b. Rotation of the variances through  $\alpha$  degrees:

$$\sigma_{\mathbf{x}_{\alpha}}^{2} = \sigma_{\mathbf{x}}^{2} \cos^{2} (90 - \alpha) + \sigma_{\mathbf{y}}^{2} \sin^{2} (90 - \alpha)$$

$$+ 2\rho\sigma_{\mathbf{x}}\sigma_{\mathbf{y}}\cos(90 - \alpha)\sin(90 - \alpha) \tag{46}$$

$$\sigma_{\mathbf{y}_{\alpha}}^{2} = \sigma_{\mathbf{y}}^{2} \cos^{2} (90 - \alpha) + \sigma_{\mathbf{x}}^{2} \sin^{2} (90 - \alpha)$$

$$-2\rho\sigma_{x}\sigma_{y}\cos(90-\alpha)\sin(90-\alpha)$$
 . (47)

c. Rotation of the linear correlation coefficient through  $\alpha$  degrees:

$$\rho_{\alpha} = \frac{\operatorname{cov} (X,Y)_{\alpha}}{\sigma_{X_{\alpha}} \sigma_{Y_{\alpha}}} , \qquad (48)$$

where cov (X,Y) $_{\alpha}$  is the rotated covariance,

$$cov (X,Y)_{\alpha} = cov (X,Y) [cos^{2} (90 - \alpha) - sin^{2} (90 - \alpha)]$$
  
  $+ cos (90 - \alpha) sin (90 - \alpha) (\sigma_{x}^{2} - \sigma_{x}^{2})$ 

and ·

$$cov (X,Y) = \rho \sigma_{X} \sigma_{V}$$

By using these rotational equations, the bivariate normal distribution with respect to any desired rotated coordinates can be obtained from sample estimates that have been computed with respect to a specific axis. The marginal distributions after rotation are also normally (univariate) distributed. By using the rotational equations, computational efforts are greatly reduced for applications requiring statistics with respect to several coordinate axes.

Appendix A presents some illustrative examples for the wind statistics of the specific RRA.

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# CHAPTER III. STATISTICS OF THERMODYNAMICS QUANTITIES AND MODELS

#### A. General Considerations

#### A.1. Objectives

The objectives inherent in developing the thermodynamic section of the RRA were to describe the thermodynamic characteristics of the atmosphere using a minimum of data tabulations. A set of parameters was selected which, together, thermodynamically describe the climatological state of the atmosphere. These parameters are the pressure, temperature, density, dew point, virtual temperature, and water vapor pressure. Used together, these parameters permit the calculation of a large number of derived quantities. Some of these quantities, such as the speed of sound, are dealt with in Section III.E.

The probability distribution of each of the six thermodynamic RRA parameters is described by its mean value, its standard deviation, and its skewness. Several of these parameters (temperature, pressure, dew point and density) have probability distributions which are close to a univariate normal distribution; the others do not. The skewness parameter gives an estimate of the asymmetrical departures of a probability distribution.

Hydrostatically modeled mean values of pressure and density were calculated (Table IV), so that users may determine the departure of the actual climatological values of these parameters from hydrostatic conditions. This was done by hydrostatically integrating the pressure from the lowest RRA data level to the termination altitude of the particular RRA.

TABLE D. LIST OF SYMBOLS USED IN CHAPTER III

C<sub>s</sub> - Speed of sound
 C<sub>d</sub> - Collision diameter
 E - Vapor pressure
 g<sub>φ</sub> - Gravity at latitude φ
 H - Geopotential height
 H<sub>m</sub> - Geopotential height at a mandatory radiosonde data level
 H<sub>s</sub> - Geopotential height at a significant radiosonde data level

TABLE D. (Continued)

K<sub>t</sub> - Coefficient of thermal conductivity

L - Mean free path length

M - Mean molecular weight of air at sea level

M3q - Annual third moment of quantity Q

M3q - Monthly third moment of quantity Q

n - Refractive modulus

N - Refractive index

NA - Avogadro's constant

Nq - Number of values of quantity Q

P - Pressure

P<sub>m</sub> - Pressure at a mandatory radiosonde data level

P<sub>e</sub> - Pressure at a significant radiosonde data level

 $\mathbf{P}_{\mathbf{h}}$  - Hydrostatically integrated mean monthly or annual pressure

Q - Any tabulated RRA quantity

R\* - Universal gas constant

R' - Specific gas constant of dry air

r', r\* - Parameters used in converting z to h and vice versa

S - Sutherland's constant, used in the calculation of dynamic viscosity

T - Temperature

T<sub>A</sub> - Dew point

T, - Virtual temperature

T.... - Virtual temperature at a mandatory radiosonde data level

 $T_{we}$  · Virtual temperature at a significant radiosonde data level

V - Mean air particle speed

#### TABLE D. (Concluded)

v<sub>c</sub> - Mean collision frequency - Parameter used in the hydrostatic interpolation of pressure W and density - Geometric altitude λ - Wavelength  $^{\alpha}\mathbf{Q}$ - Skewness of quantity Q - Constant used in the equation for viscosity ß - Ratio of specific heat at constant pressure to specific heat at constant volume - Kinematic coefficient of viscosity

- Dynamic coefficient of viscosity

- Density

- Mean monthly or annual density derived from Ph oh

- Standard deviation of the quantity Q

## A.2. Data Quality Control

Data limits derived from the following parameters were used to screen the thermodynamic portion of the RRA data base: temperature, pressure, dew point (for the 0-30 km portion only), and density (for the 30-70 km portion only). These limits were set to plus and minus six standard deviations from the mean values of each of these quantities. These limits were used to screen the thermodynamic portion of the RRA data base, according to the procedures described in Section I.C. The data base used to generate the thermodynamic portion of the RRA (Tables I, II, and IV) was considered to be free from errors if:

- a) The skewness values of the pressure and temperature were between -2.5 and 2.5 at all data levels.
- b) The skewness values of the density were between -3.5 and 3.5 at data levels between 0 and 30 km.
- c) The skewness values of the density were between -3.0 and 3.0 at data levels between 30 and 70 km.
- d) The skewness values of the dew point were between -2.5 and 2.5 at all data levels with more than 10 data values.

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#### A.3. Limitation of Thermodynamic Statistics

The correlation coefficients between the thermodynamic quantities and the moisture-related quantities were not calculated at discrete altitudes nor were any of the correlations between altitudes. Therefore, valid statistical dispersion models that require the relationship between two or more of these quantities at the same altitude or between altitudes cannot be Approximations for the correlation coefficients between pressure, virtual temperature, and density at discrete altitudes may be obtained from the coefficients of variation as developed by Buell (1970). The coefficient of variation is the standard deviation divided by the mean. The mean values and the standard deviations are taken from Table II. A model for the profile of monthly and annual mean pressure, virtual temperature, and density that is in excellent agreement with the respective statistical mean values is given by Table IV. This agreement results because the physical relationships, given by the hydrostatic equation and the equation of state, were used to derive Table IV.. When only the monthly or annual mean values for pressure, virtual temperature, and density are required, it is recommended that Table IV be used.

#### B. Establishing Data Samples at the Required Altitude Levels

This section describes the computational procedures used to establish data samples of the thermodynamic RRA parameters at the RRA data levels. References are cited only when an equation given is one of many available in the literature or when an equation is stated in an unusual form.

# B.1. Conversion of Data Recorded in Geopotential Heights to Geometric Altitude

The upper air rocketsonde observations used to obtain the table values above 30 km were recorded in terms of geometric altitude and can be interpolated directly to the altitude intervals shown in the tables. However, the radiosonde observations used to obtain the tabular values below 30 km were recorded in terms of geopotential heights. The change of coordinates from geopotential height to geometric altitude (h to z) is accomplished by calculating a table of geopotential heights which correspond exactly to the geometric altitudes at which the atmospheric parameters are tabulated. The radiosonde observations are then interpolated to these geopotential heights. The relationship used to calculate geometric altitude from geopotential height is

$$H = (r^{\dagger}z)/(r^{*}z)$$
 , (49)

where

r' = gr\*/9.80665

and

$$\mathbf{r}^* = -2\mathbf{g}_{\phi}/(\partial \mathbf{g}_{\phi}/\partial \mathbf{z}_{\mathbf{0}})$$

 $g_{\phi}$  is the sea level gravity at the latitude  $\phi$  corresponding to the proper location. This value is given by (List, 1968)

$$g_{\phi} = 9.780356 \ (1 \pm 5.2885 \times 10^{-3} \sin^2 \phi - 5.9 \times 10^{-6} \sin^2 (2\phi)) \ .$$
 (50)

 $\frac{\partial g_{\phi}}{\partial z_{0}}$  is the rate of change of gravity at the sea level. This quantity is given by the equation

$$\frac{\partial g_{\phi}}{\partial z_{0}} = -3.085462 \times 10^{-6} + 2.27 \times 10^{-9} \cos (2\phi) - 2 \times 10^{-12} \cos (4\phi) . \tag{51}$$

The units used for gravity are m/s<sup>2</sup>, while the units for  $\frac{\partial g_{\phi}}{\partial z_{0}}$  are s<sup>-2</sup>.

The resulting table of values of H obtained by using even increments of 2 in equation (49) is shown in Table IV of the RRA. The values of H above 30 km are not used in the interpolation of original data but are included for the convenience of the user.

## B.2. Calculations on the Original Rawinsonde Data Records

It was necessary to interpolate the information from the original rawinsonde data records to the geometric altitudes specified as the RRA data levels. The parameters for which this interpolation was required were the temperature, dew point, and pressure. The other parameters were calculated from the interpolated values at each RRA data level. These "derived" parameters were the water vapor pressure, density, and virtual temperature.

## B.2.1. Calculation of the Geopotential Height at Significant Levels

Two somewhat different interpolation procedures were used to obtain data at the levels shown in the tables from radiosonde and rocketsonde observations. The procedure used to interpolate radiosonde observations begins with the calculation of virtual temperature at each data level in a sounding. The virtual temperature was computed by

al distribution of the second of the second

$$T_{V} = T/(1. - 0.379 (e/p))$$
 , (52)

where  $T_{v}$  and T are in degrees K and e and p are in millibars.

The radiosonde soundings contain a mix of data taken at "mandatory" and "significant" levels. Pressure, temperature, and dew point information was given in these soundings at both types of levels. However, geopotential height information was only given at the mandatory levels. The heights at the significant levels were "filled in" (calculated) hydrostatically using pressure and temperature data from these levels. This procedure permitted the use of most of the significant level data in the calculation of the RRA tables. The equation used for this process was

$$H_s = Hm + 29.2712617 * \frac{(T_{vs} - T_{vm})}{2} * ln(P_s/P_m)$$
, (53)

where the subscripts s and m denote quantities at significant and mandatory levels. This equation was not used if the difference between two adjacent mandatory levels was greater than 200 mb. All soundings with such data gaps were rejected for use in compiling the RRA.

#### B.2.2. Temperature

Radiosonde temperatures were interpolated logarithmically with respect to pressure using the equation

$$T = T_U + (T_L - T_U) \frac{\ln p - \ln p_L}{\ln p_U - \ln p_L},$$
 (54)

where the subscripts U and L indicate values at the nearest data levels in the actual sounding above and below the interpolated level.

#### B.2.3. Pressure

The pressure values in each radiosonde sounding were interpolated to the RRA data levels using the equation

$$p = pL \exp\left(\frac{H_{L} - H_{U}}{29.27126!7 (0.5) (T_{V_{U}} + T_{V_{L}})}\right)$$
 (55)

where the subscript L indicates virtual temperature, geopotential, and pressure values at the data level below and closest to the level at which data were required.

## B.2.4. Dew-Point Temperature

Dew-point values were interpolated logarithmically with respect to pressure using the equation

$$T_{d} = T_{dU} + (T_{dL} - T_{dU}) \left( \frac{\ln p - \ln p_{L}}{\ln p_{U} - \ln p_{L}} \right) . \tag{56}$$

The subscripts U and L indicate data at the nearest upper and lower data levels in a sounding.

## B.2.5. Derived Water Vapor Pressure

The water vapor pressure is calculated from the interpolated dewpoint values at the RRA data levels using Teten's approximation:

$$7.5(T_{d} - 273.15)/(T_{d} - 35.86)$$
e = 6.11 mb × 10 (57)

#### B.2.6 Derived Density

The density values derived from radiosonde observations were calculated at the RRA data levels using the equation

$$\rho = 348.36787 \text{ p/T}_{v}$$
 (58)

## B.2.7 Derived Virtual Temperature

The virtual temperature values are calculated at the RRA data levels for each sounding using the equation

$$T_v = T/(1 - 0.379(e/p))$$
 , (59)

where Tv and T are in degrees K and p and e are the pressure and vapor pressure, respectively, in millibars.

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## B.3. Calculations on the Original Rocketsonde Data Records

The rocketsonde data records used to calculate the RRA table values above 30 km were given in terms of geometric altitude. For this reason, slightly different calculations were required to convert the recorded data values to values at the RRA data levels. The pressure, temperature, and density were all interpolated to the RRA data levels; moisture-related parameters (virtual temperature, water vapor pressure, and dew point) were not calculated, since atmospheric moisture at altitudes above 30 km was considered to be negligible.

No interpolation was done across gaps in the pressure or temperature data within a sounding larger than 7000 r. Data values at the RRA levels within such a gap were set to missing.

## B.3.1. Temperature

Rocketsonde temperatures were interpolated linearly with respect to geometric altitude using the equation

$$T = T_U + (T_L - T_U) \frac{Z - Z_L}{Z_U - Z_L}$$
 (60)

where the subscripts U and L indicate values at the nearest data level in the actual sounding above and below the interpolated level.

## B.3.2. Pressure

The pressure values in each rocketsonde sounding were interpolated to the RRA data levels using the equation

$$P = P_{\tilde{L}} \exp \left( -\frac{g_{\phi}}{R^*} \frac{M(Z - Z_{\tilde{L}})}{Tv} \cdot W^2 \right)$$
 (61)

where 
$$\overline{T_V} = \frac{Tv_U + Tv_L}{2}$$
 and  $W = \frac{r^*}{\left(r^* + Z + \frac{Z - Z_L}{2}\right)}$ .

## B.3.3 Density

Rocketsonde density values were interpolated using the equation

$$\rho = \rho_{\mathbf{L}} \exp \left( -\frac{g_{\phi}^{\mathbf{M}}}{\mathbf{R}^*} \frac{(\mathbf{Z} - \mathbf{Z}_{\mathbf{L}})}{\overline{\mathbf{T}_{\mathbf{V}}}} \cdot \mathbf{W}^2 \right) , \qquad (62)$$

where W is specified in Section III.B.3.2.

## C. Computation of Statistical Parameters for Tables II and III

The procedure used for computing the monthly and annual means, standard deviations, and skewness values from the data values at the RRA data levels was accomplished in three steps. Initially, certain statistical sums were calculated and stored as the soundings in the data base were processed. These sums were then used to calculate the monthly statistics given in the RRA tables. The annual statistics were then calculated from these stored sums and the monthly statistics.

## C.1. Stored Statistical Sums

The sums which were calculated were

$$\sum Q$$
,  $\sum Q^2$ , and  $\sum Q^3$ ,

where Q is any one of the quantities given in the thermodynamic part of the RRA.

## C.2. Calculation of the Monthly Statistics

## C.2.1. Monthly Means

The mean monthly values of the thermodynamic RRA quantities were calculated using the equation

$$\bar{Q} = \sum Q/N_Q$$
,

where  $N_Q$  is tre number of observed values of the quantity Q for a given month.

## C.2.2 Monthly Standard Deviations

The monthly standard deviations of the thermodynamic RRA quantities were calculated using the equation

$$\sigma_{Q} = \sqrt{\frac{(N_{Q} \Sigma' Q^{2}) - (\Sigma Q)^{2}}{N_{Q} \cdot (N_{Q} - 1)}} . \tag{63}$$

## C.2.3 Monthly Skewness Values

The monthly skewness values of the wind speed and of the thermodynamic RRA quantities are calculated using the equation

$$\alpha_{\mathbf{Q}} = \frac{M3_{\mathbf{Q}}}{\sigma_{\mathbf{Q}}^3}$$

where M3  $_{\mbox{\scriptsize Q}}$  is the third moment of the quantity Q,  $\sigma_{\mbox{\scriptsize Q}}$  is its standard deviation, and

$$M_{3Q} = \left[ \frac{\Sigma_{Q}^{3}}{N_{Q}} - \frac{3\Sigma_{Q}\Sigma_{Q}^{2}}{N_{Q}^{2}} - \frac{2\Sigma_{Q}^{3}}{N_{Q}^{3}} \right] \cdot \frac{N_{Q}^{2}}{(N_{Q} - 1)(N_{Q} - 2)} \quad . \tag{64}$$

## C.3. Calculation of the Annual Statistics

Equations (63) and (64), used to calculate the monthly values of the standard deviations and skewness values, involve taking the differences between two pairs of large sums containing Q\*\*2 and Q\*\*3, where Q is any thermodynamic RRA quantity. Using these equations to compute the annual statistics would have resulted in a substantial loss of precision, as these sums become larger by several orders of magnitude in such a case. This problem was avoided by calculating the annual means, standard deviations, and skewness values from the monthly statistics.

## C.3.1. Annual Mean Values

The annual mean values of the thermodynamic RRA quantities were calculated using the equation

$$Q_{ANN} = Q_A/N_Q$$

where  $\boldsymbol{\hat{Q}}_A$  is the total of all observed values of Q and N  $_Q$  is the total number of observations of Q.

#### C.3.2. Annual Standard Deviations

The annual standard deviations of the thermodynamic RRA quantities were calculated using the equation

$$\sigma Q_{ANN} = \sqrt{\frac{1}{N_Q} \sum_{i=1}^{12} (N_{Qi} \sigma_{Qi}^2) + \frac{1}{N_Q} \sum_{i=1}^{12} (N_{Qi} \overline{Q}_i^2) - Q_{ANN}^2} , \qquad (65)$$

where  $N_{Q_i}$  = the number of data values for Q in month i (i = 1 to 12) and Qi = the monthly mean of Q and  $\sigma_{Qi}$  = the standard deviation of quantity Q in month i.

## C.3.3. Annual Skewness Values

The annual skewness values of the thermodynamic RRA quantities are calculated using the equation

$$M3Q_{ANN} = \frac{1}{N} \sum_{i=1}^{12} (N_{Qi} M_{3Qi}) + \frac{3}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} \overline{Q}_{i} \sigma_{Qi}^{2})$$

$$+ \frac{1}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} Q_{i}^{3}) - \frac{3\overline{Q}_{ANN}}{NQ_{ANN}} \sum_{i=1}^{12} (N_{qi} Q_{i}^{2})$$

$$- \frac{3\overline{Q}_{ANN}}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} \sigma_{Qi}^{2}) + 2\overline{Q}_{ANN}^{3} , \qquad (66)$$

where  $M_{3Q}$  = the third moment about the mean of quantity Q in month i and  $M_{3Q}$  = the annual third moment about the mean of the quantity Q.

(66)

## D. Derived Monthly Mean and Annual Mean Model Atmospheres

A set of modeled monthly mean and annual mean hydrostatic values of pressure and density was calculated from the lowest RRA data level (0 km, mean sea level) upwards to 30 km, and from 30 km upwards to 70 km. The integration from 0 to 30 km was computed independently of the integration from 30 to 70 km because of the difference in data sources. The two different values for 30 km are provided for comparison. When 30 km data are required, the values given in the 0 to 30 km table should be used. These hydrostatically modeled mean values, which are given in Table IV, are useful as a check on the validity of the pressure and density values given in Table II. In most cases, the values in Tables II and IV for any given data level are within 1 percent of each other. The hydrostatic pressure values in Table IV were calculated using the equation

$$p_1 = p_0 \exp \left( -\frac{0.034162 (H_1 - H_0)}{0.5 (T_{v_1} + T_{v_0})} \right) , \qquad (67)$$

where,  ${\rm H_1}$  -  ${\rm H_0}$  is in meters and a "0" subscript refers to values at the RRA data level immediately below the level being checked.  ${\rm p_0}$  at the lowest data level is set equal to the RRA mean pressure;  ${\rm p_1}$ , calculated for the next highest data level, is taken as  ${\rm p_0}$  for the level above that. This process is repeated for all the other RRA data levels. The hydrostatic density corresponding to the hydrostatic pressures is calculated from these pressures and the RRA virtual temperature values using the formula

$$\rho_{\rm H} = 348.36786 \ P_{\rm H}/T_{\rm v}$$
 , (68)

where  $\rho_{\mbox{\scriptsize H}}$  and  $P_{\mbox{\scriptsize H}}$  are the hydrostatic density and pressure shown in Table IV of the RRA.

## E. Thermodynamic Quantities Derivable from the Basic Tables

Several other quantities can be calculated from the statistics listed in Tables II and III. The equations given in this section can be used to calculate the approximate mean values of these quantities at each RRA data level. It is not possible to infer or derive any information concerning the standard deviation or skewness values of these quantities from the data in Tables II and III of the RRA.

### TABLE E. LIST OF PRIMARY PHYSICAL CONSTANTS

- P<sub>o</sub> = standard atmospheric pressure at sea level =  $1.013250 \times 10^5$  Newton/m<sup>2</sup> = 2116.22 lb/ft<sup>2</sup>
- $\rho_0$  = standard atmospheric density at sea level = 1.2250 kg/m<sup>3</sup> = 0.673 \*\*\* 1b/ft<sup>3</sup>
- $T_{O}$  = standard temperature & sea level = 288.15 K = 15.0°C = 59.0°F
- $g_0$  = standard gravity at sea level at latitude  $45^{\circ}32^{\circ}33^{\circ}$ = 9.80665 m/s<sup>2</sup>
- s = Sutherland's constant used in calculation of dynamic viscosity = 110.4 K
- $T_{I}$  = ice-point temperature at  $P_{O}$  = 273.15 K
- β = constant used in calculation of dynamic viscosity
  - = 1.458 × 10<sup>-6</sup> kg/sec m K<sup>1/2</sup> = 7.3025 × 10<sup>-7</sup> lb/sec ft R<sup>1/2</sup>
- γ = ratio of specific heat of air at constant pressure to specific heat of air at constant volume = 1.4
- $C_{\rm D}$  = mean effective collision diameter of air molecules = 3.65  $\times$   $10^{-10}$  m = 1.1975  $\times$   $10^{-9}$  ft
- $N_a$  = Avogodro's constant =  $6.022169 \times 10^{26}/kg \text{ mol} = 2.73179 \times 10^{26}/lb \text{ mol}$
- R\* = gas constant = 8.31432 Joule/mol K
- $R' = gas constant for dry air = 2.8704 \times 10^2 Joule/kg K$
- M = molecular weight of dry air = 28.966 gm/mol

## E.1. Mean Air-Particle Speed

The mean air particle speed, V, is the arithmetic average of the speeds of all air particles in the volume element being considered. For a valid average to occur, there must be a sufficient number of particles involved to represent mean conditions. The equation for "V" for dry air is:

$$V = \sqrt{\frac{8}{\pi} \cdot \frac{R^*T}{M}} \quad . \tag{69}$$

A computational form for dry air, using tabulated values, is:

$$V = \sqrt{7.3094 \times 10^2 \times T}$$
 , (m/s) (70)

where T is the temperature in degrees K from Table II. Equation (69), when corrected for moist air, becomes:

$$V = \sqrt{\frac{8}{\pi} \cdot R' T_{\mathbf{v}}} \quad . \tag{71}$$

The computational form for moist air is:

$$V = \sqrt{7.3094 \cdot 10^2 \cdot T_{v}}, \quad (m/s)$$
 (72)

where  $\mathbf{T}_{\mathbf{v}}$  is the virtual temperature in degrees K from Table III.

#### E.2. Mean Free Path

The mean free path, L, is the mean value of the distance traveled by each neutral air particle, in a selected air parcel, between successive collisions with other particles in that parcel. A meaningful average requires that the selected parcel be large enough to contain a substantial number of particles. The equation for L is given by:

$$L = \left(\frac{\sqrt{2}}{2\pi}\right) \left(\frac{R*T}{N_a C_d^2 P}\right) , \qquad (73)$$

where  $C_{\rm d}$  is the effective collision diameter of the mean air molecules. The 1976 standard atmosphere value of 3.65  $\times$  10<sup>-10</sup> is valid for the range of altitudes in the RRA.

A computational form for moist air, using tabulated values, is:

$$L = 2.335 \times 10^{-7} \frac{T}{P} \text{ (meters)}$$
 , (74)

where T is the temperature in degrees K from Table II and P is the pressure, in mb, from Table II.

A form of (73) to correct L for moist air is:

$$L = \left(\frac{\sqrt{2}}{2\pi}\right) \frac{R'MT_{v}}{N_{a} C_{d}^{2}} . \tag{75}$$

The computational form for moist air is:

$$L = 2.3325 \times 10^{-7} \frac{T_{v}}{P} \text{ (meters)} ,$$
 (76)

where  $T_{\mathbf{v}}$  is the virtual temperature in degrees K from Table III and P is the pressure in mb from Table II.

#### E.3. Mean Collision Frequency

The mean collision frequency V is considered to be the average speed of air particles contained in an air parcel divided by the mean free path of the particles inside that parcel. Computationally this is equivalent to:

$$V_{c} = \frac{V}{L} (sec^{-1}) \qquad . \tag{77}$$

To determine  $V_c$  for dry air, use V and L from equations (70) and (74). To determine  $V_c$  for moist air, use V and L from equations (72) and (76).

## E.4. Speed of Sound

The expression for the speed of sound,  $C_s$ , in dry air, in m/s is

$$C_{s} = \sqrt{\frac{\gamma R * T}{M}} \quad . \tag{78}$$

To compute C for dry air from tabulated values, use:

$$C_s = \sqrt{4.0185 \times 10^2 \times T}$$
 . (m/s) (79)

where T is the temperature in degrees K from Table II. One form for the speed of sound in moist air is:

$$C_s \approx \sqrt{\gamma R' T_V}$$
 , (80)

where  $T_{v}$  is the virtual temperature from Table III. A computational form for moist air is:

$$C_s \approx \sqrt{4.0185 \times 10^2 T_y}$$
 , (m/s) . (81)

## E.5. Dynamic Coefficient of Viscosity

The coefficient of dynamic viscosity,  $\mu$ , is defined as a coefficient of internal friction developed where gas regions move adjacent to each other at different velocities. The following expression is taken from the U.S. Standard Atmosphere (1976):

$$\mu = \frac{\beta + T^{3/2}}{T + S} . \tag{82}$$

The computational form is:

$$\mu = \frac{(1.458 \times 10^{-6}) \text{ T}^{3/2}}{\text{T} + 110.4} , \left(\frac{\text{kg}}{\text{s·m}}\right)$$
 (83)

where T is temperature in degrees K from Table II.

## E.6. Kinematic Coefficient of Viscosity

The kinematic coefficient of viscosity, designated as  $\eta$ , is defined to be the ratio of the dynamic coefficient of viscosity of a gas to its density, or:

$$\gamma = \mu/\rho \quad . \tag{84}$$

The computational form is:

$$\eta = 1.0 \times 10^3 \, \mu/g \, , \, (m^2/s) \, , \, (85)$$

where u is the dynamic coefficient of viscosity from equation (83) and  $\rho$  is the density in g m<sup>-3</sup> from Table II.

## E.7. Coefficient of Thermal Conductivity

The empirical expression used for the coefficient of thermal conductivity, designated as  $K_{\rm t}$ , is given in the 1976 Standard Atmosphere as:

$$K_t = \frac{2.65019 \times 10^{-3} \cdot T^{3/2}}{T + 245.4 \times 10^{-(12/T)}}$$
, (watts/m-deg K) (86)

where T is in degrees K.

## E.8. Refractive Modulus and Refractive Index

The refractive modulus or refractivity (Selby and McClatchey. 1975: Smith and Weintraub, 1953) is defined as N, where

$$N = (n - 1) \cdot 10^6 \tag{87}$$

and n is the refractive index.

For microwave frequencies below approximately 30 GHz (equivalent to wavelengths above 1 cm), N, the refractive modulus, is given by the empirical equation

$$N = 77.6 \frac{P}{T_d} + 3.73 \times 10^5 \frac{e}{T^2}$$
 (dimensionless) , (88)

where E and P are in millibars and T and  $\mathbf{T}_{\mathbf{d}}$  are in degrees K.

The following expression is valid for the visible and infrared wavelengths shorter than approximately 30  $\mu m$  (0.03 mm).

$$N = 77.6 \frac{P}{T} + 0.584 \frac{P}{T} \text{ dimensionless} . \tag{89}$$

where  $\lambda$  is the wavelength in microns and T is in degrees K.

The expression for N for the wavelength from 0.03 mm to 1 cm is an extremely complex function of wavelength.

#### CHAPTER IV. CONCLUSIONS AND RECOMMENDATIONS

#### Conclusions

This document satisfies the technical objectives established for the Range Reference Atmosphere committee by the Range Commanders Council ideteorology Group. Upper air statistics and model: for wind and thermodynamic quantities for the specific site have been derived in a consistent and uniform manner which will be used in publications for all other assigned site locations. These Range Reference Atmospheres represent an improvement over the previously published Range Reference Atmospheres because of the availability of more extensive upper air data bases and the adaptation of more advanced statistical techniques. A statistical measure of central tendency (mean values) and a measure of dispersion (standard deviation with respect to the mean values) for monthly and annual reference periods have been tabulated for all variables in a consistent manner from data bases that have been edited and quality controlled in the same manner. Further, a statistical measure for symmetry (skewness coefficient which involves the third statistical moment) has been tabulated for all variables except the zonal and meridional wind components. Even with these improvements, the user of these Range Reference Atmospheres must recognize certain limitations of the statistical tabulations. Namely:

- 1) The wind profile structure with respect to altitude cannot be modeled from the RRA statistics because the inter-level and cross-level correlations were not computed.
- 2) The profile structure with respect to altitude for any of the thermodynamic variables or any quantities derivable from these variables cannot be modeled because the prerequisite correlations were not computed. However, the profile of monthly and annual means for pressure, virtual temperature, and density are in agreement (Table IV) with the hydrostatic equation and the equation of state.

The preceding limitations are cited to prevent a misuse of the RRAs. More extensive statistical tabulations were beyond the scope of this committee's task. As greater insight is gained through usage of these RRAs, many adaptations of the statistical tabulations for specific engineering and scientific applications are envisioned.

#### Recommendations

It is recommended that the wind and thermodynamic statistical tabulations and attendant models contained in the RRAs be used as a standard reference source, as may be appropriate, by the Ranges and Range users. It is further recommended that the respective Range Staff Meteorologist or responsible agency staff member be consulted for the applicability of the Range Reference Atmospheres for specific engineering applications.

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#### CONVERSION UNITS

## Physical Constants and Conversion Factors

Numerical values in this document are given in the International System of Units (SI, Système International d'Unités). The values in parentheses are equivalent U. S. Customary Units, which are English units adapted for use by the United States of America. The SI and U. S. Customary Units provided in Table F are those normally used for measuring and reporting atmospheric data.

By definition, the following fundamental conversion factors are exact:

Type	U. S. Customary Units	Metric
Length Mass Time Temperature	1 U.S. yard (yd) 1 avoirdupois pound (lb) 1 second (s) 1 degree Rankine (°R)	0.9144 meter (m) 453.59237 gram (g) 1 second (s) 9/5 degree Kelvin (°K)

To aid in the conversion of units, conversion factors based on the above fundamental conversion factors are given in Table F.

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TABLE F. FACTORS FOR CONVERSION UNITS

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TABLE	1. 1	WIND STAT	TISTICAL PA	RAMETERS.		JA	NUARY		
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2.000		3.45	.2475	-5.62	2.84	10.19	3.36	16	431.
3.000	-7.18 -6.50	3.35	.1623	92	3.21	8.10	3.42	.29	430.
4.000	-6.59	4.53	.1650	51	3.12	7.73	3.75	.57	429.
5.000	-7.54	4.91	1998	58	3.20	8.66	4.97	.26	428.
5.000 6.000	-8.84	5.49	.1735	-1.08	3.72	10.04	4.74	. 15	428.
7.000	-9.49	5.92	.1788	-1.60	4.38	10.97	5.14	.25	427.
8.000	-9.07	6.23	.1478	-2.08	4.44	10.87	5.18	.56	428.
9.000	-7.54	6.16	.0873	-2.28	4.46	9.75	4.97	.49	427.
	-5.37	5.87	.0565	-2.11	4.08	8.16	4.32	,44	427.
10.000 11.000	-3.58	5.82	.9856	~1.25	4.20	7.07	3.98	.75	427.
	-2.45	6.18	.0620	. 16	5.15	7.40	3.98	.75	425.
12.000	-2.25	6.34	.0297	. <del>9</del> 0	5.55	7.76	4.06	.84	424.
13.000	-2.48	6.67	.0579	1.24	5.84	8.16	4.42	.83	423.
14.000	-3.23	6.87	.0010	.80	٠٤.٤٠	ช.วร์	4.78	.64	463.
15.000 16.000	-4.75	6.84	1005	45	5.95	8.95	4.98	.60	416.
	-6.55	6.72	2230	-1.68	5.01	9.53	5.00	.71	284.
17.000	-8.33	5.94	1630	-2.09	4.27	10.12	4.95	.48	278
18.000	-7.34	5.90	1056	51	3.49	8.74	4.98	.70	279.
19.000	-2.89	7.74	1115	36	2.46	7.24	4.67	.85	275.
20.000	-2.47	10.81	1614	11	2.36	10.19	4.93	.64	270.
21.000	-4.71	13.09	1130	.11	2.39	12.32	6.84	.34	261.
22.000	-6.78	12.89	.0543	.26	2.99	12.56	7.93	.45	261.
23.000	-7.70	10.75	.0975	.50	2.27	11.38	7.09	.77	250.
24.000	-8.21	10.82	.0840	.83	3.14	11.98	7.15	.93	251.
25.000	-6.78	10.53	0240	.68	3.18	10.80	7.11	.59	249.
26.000	-4.86	11.60	.0562	.51	2.62	10.52	7.37	.80	237.
27.000	-3.19	13.90	.1697	.68	2.65	12.28	7.52	.55	214.
28.000	-3.07	15.65	.2139	.82	2.87	14.51	7.21	.51	212.
29.000	-3.97	16.66	.2590	.61	3.29	16.00	6.87	.25	189.
30.000	-4.90	17.10	-2414	.28	2.93	15.75	6.55	22	156.
3≥.000	98	20.52	.0115	.05	4.07	19.39	7.57	.07	73.
34.000	-4.93	29.93	.1793	-1.05	4.38	19.82	9.19	.27	73.
36.000	-6.41	18.06	0956	-1.62	4.65	17.44	9.15	.54	73.
38.000	-7.45	14.82	0579	81	5.89	14.51	9.89	.87	73.
40.000	-10.10	:3 54	~ .0157	.69	5.73	15.60	9.36	.57	73.
42.000	-13.10	13.54	0281	1.60	7.14	18.23	8.59	.24	73.
44.000	-16.72	14.68	.0835	2.46	8.30	21.05	11.16	.55	73.
46.000	-24.98	17.65	0639	3.67	9.21	28.85	14.09	.07	73.
48.000	-29.41	20.24	!377	3.44	11.44	33.96	16.24	.15	72.
50.000	-21.84	23.82	1'127	2.29	13.09	30.60	16.68	.64	72.
52.000	-5.80	22.50	.1979	1.13	14.55	24.24	12.56	. 44	72.
54.000	6.69	15.97	-0374	2.37	13.33	18.90	11.01	.50	71.
56.000	:3.42	16.35	0802	.73	12.51	21.46	11.81	.98	69.
58.000	20.17	15.23	.2127	-3.54	12.18	25.79	11.41	.17	63.
60.000	27.07	20.31	.1634	-3.61	12.79	32.66	15.78	.49	53.
62.000	30.09	23.37	.2279	65	14.14	36.50	17.59	.30	44.
64.000	37.03	25.40	.0905	-1.64	14.42	43.46	17.98	.09	35.
66.000	37.68	21.40	1434	-1.58	14.99	42.13	17.85	05	33. 31.
68.000	30.73	17.92	.0835	.20	14.87	36.10	13.06	.33	29.
70.000	23.65	14.49	.0218	-1.74	20.59	32.45	11.21	06	29.
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	1. 2 ≈ 913660		ISTICAL PA EIN MISSLE			FE	BRUARY		
· Z	MEAN U	5.D. U	R(U,V)	MEAN V	S.D. V	MEAN HS	S.D. WS	SKEW WS	NOBS
KM	M/S	M/S		M/S	M/S	M/S	M/S	JACK HJ	11005
.002	-7.06	2.08	.0521	-3.60	1.86	8.16	1.97	.05	398.
1.000	-9.93	3.66	.1992	-2.62	2.48	10.60	3.57	.12	401.
2.000	-7.29	4.23	. 1456	63	2.70	8.08	3.67	.52	401.
3.000	-5.56	4.61	.1366	09	2.88	6.57	3.45	.32	401.
4.000	-5.96	5.35	.2468	~.13	3.07	7.69	3.79	.37	401.
5.000	-6.72	5.78	.2171	42	3.24	8.44	4.23	.40	401.
6.000	-7.52	6.55	.1927	99	4.09	9.64	4.92	.36	400.
7.000	-7.42	6.82	.0853	-1.75	4.25	9.91	4.95	.46	400.
9.000	-6.05	6.83	0599	-1.94	4.27	9.22	4.49	.42	399.
9.000	-4.18	6.91	0144	-1.71	4.12	8 23	4.15	.57	399.
10.000	-2.42	6.95	0045	-1.11	4.47	7.69	4.60	.68	395.
11.000	-1.14	7.18	06:2	10	5.48	8.05	4.25	.82	394.
12.000	-1.03	7.09	0813	.ن8	6.26	8.42	4.48	.65	394.
13.000	-1.25	7.32	1054	.97	7.13	9.13	4.83	.63	394.
14.000	+0.5-	7.27	1492	.36	7.87	9.73	4.93	.63	394.
15.000	-3.49	7.31	1895	88	7.61	10.03	4.85	.47	389.
16.000	-5.46	6.98	2472	-1.27	6.14	9.67	4.90	.55	261.
17.000	-7.19	6.45	3049	-1.45	4.60	9.70	4.72	.54	256.
18.000	-6.07	6.33	0749	53	3.77	8.18	4.96	.91	255.
19.000	-1.14	6.92	0001	45	2.29	6.35	3.77	.95	253.
20.000	-1.33	10.53	~.0796	26	2.33	9.97	4.28	.35	251.
21.000	-3.11	12.91	1198	.26	2.34	11.99	6.14	.32	242.
22.000	-4.90	12.92	1801	.39	2.71	11.41	8.23	.72	242.
23.000	~4.84	10.26	1719	.06	2.16	10.02	5.72	1.17	233.
24.000	-4.68	10.96	1016	03	2.98	10.55	6.27	.75	229.
25.000	-4.19	12.59	0952	.39	3.03	11.59	7.12	.32	228.
26.000	-3.38	14.11	.0409	.48	2.23	12.44	7.76	.34	220.
27.000	-3.09	15.75	.1468	.59	2.44	14.01	8.18	.19	211.
28.000	-3.72	16.84	.1606	.56	2.68	15.67	7.65	.15	209.
29.000	-4.83	17.63	.1846	.64	2.88	17.07	7.08	.00	187.
30.000	~5.94	17.80	.1721	.77	2.64	17.72	6.64	~.24	162.
غد.050	-4.09	:8.7ů	.1228	.00	3.51	17.72	8.00	10	S'1.
34.000	-9.68	17.90	.3839	~.25	3.97	18.64	8.86	14	64.
36.000	~14.25	16.61	0113	91	3.49	19.87	9.71	10	64.
38.000	-15.67	16.02	.1713	92	4.50	20.62	9.76	.11	64.
40.000	-16.14	14.76	.1419	1.09	5.36	19.85	10.60	.28	63.
42.000	-18.31	15.46	.1617	1.83	6.40	21.76	11.95	.06	63.
44.000	-15.11	17.49	.1940	2.43	7.03	20.88	12.26	.60	63.
46.000	-12.17	16.44	0036	3.36	8.38	19.39	10.97	.53	63.
48.00 <b>0</b>	-1.80	16.85	.1244	2.23	7.57	15.38	10.45	.92	63.
50.000	6.29	15.45	.0497	3.61	8.42	16.55	9.21	.61	63.
52.000	13.05	17.51 .	.2138	4.59	9.41	21.55	10.85	.98	62.
54.000	20.26	15.69	.1302	3.32	9.43	24.27	12.83	.20	€2.
56.000	25.60	16.53	.3031	1.95	10.14	29.05	13.71	01	59.
58.000	30.18	17.21	.3218	-1.17	11.11	33.08	15.31	25	53.
60.000	35.28	19.58	.2281	-4.53	11.41	38.89	16.16	43	47.
62.000	31.60	22.72	.4171	-5.71	14.34	38.68	16.03	58	38.
<b>64.000</b>	30.15	22.82	.5703	-1.44	15.65	37.25	16.54	.04	32.
66.000	31.51	20.23	.3507	.50	17.29	36.61	18.66	.29	28.
68.000	26.93	18.93	.0420	. 30	18.72	34.50	13.91	.49	28.
70.000	27.01	15.70	0383	-1.35	16.59	32.71	13.05	.24	28.

TABLE STATION	1. 3 = 913660	HIND STA	TISTICAL PA	WRAMETERS.		М	ARCH		
Z	MEAN U	S.D. U			<b>-</b>		•		
KM	M/S	M/S	R(U,Y)	MEAN V	5.D. V	MEAN WS	S.D. KS	SKEW WS	NOBS
.002	-6.71	2.11	.2016	M/S	M/S	M/S	M/S		
1.000	-8.95	3.45	.3222	-2.72	2.19	7.61	1.97	46	426,
2.000	-6.20	3.87	.0601	-1.86 21	2.67	9.56	3.33	04	428.
3.000	-4.52	4.14	.0988	.18	2.53	6.94	3.42	.47	427.
4.000	-4.28	4.38	.1126	06	2.52	5.89	3.03	.60	425.
5.000	-4.87	5.12	.2446	28	2.78	5.96	3.11	.51	426.
6.000	-5.31	6.15	.2524	87	3.19	6.77	3.78	.76	425.
7.000	-4.72	6.81	.2499	-1.56	4.09	8.01	4.39	.62	423.
8.000	-3.28	7.05	.2327	-1.84	4.83	8.45	4.80	.58	423.
9.000	-1.35	7.17	.2373	-1.36	4.90	8.17	4.58	.70	422.
10.000	.29	7.46	.2654	-1.56	4.92	7.67	4.51	1.16	422.
11.000	1.26	7.81	.2430	54	5.22	7.87	4.60	1.11	423.
12.000	1.93	7.89	.1471	.49	6.15	8.69	4.99	.98	423.
13.000	2.21	8.39	.0590	.54	6.41	9.06	5.06	.83	422.
14.000	1.64	8.39	63 <del>3</del> 5	69	6.98	9.64	5.45	1.00	419.
15.000	.15	8.06	1821	-2.07	b.€+	9.48	5.35	. 74	418.
16.000	-2.13	7.98	0915	~3.15	6.13	8.99	5.09	.87	415.
17.000	-4 39	7.65	0135	-2.18	4.84 4.05	8.85	4.80	0ל.	279.
18.000	-4.07	8.05	0428	92		8.65	4.88	.76	275.
19.000	-1.01	7.88	0519	92 43	3.49	8.01	5.48	1 51	273.
20.000	-1.13	9.90	0437	45 04	2.34	7.23	4.04	.91	272.
21.000	-2.84	11.55	0304		2.31	9.27	4.30	.17	265.
22.000	-4.45	11.58	0377	.21	2.62	10.70	5.80	. 38	255.
23.000	-4.21	9.54	0596	.21 .10	2.72	10.77	6.71	.76	253.
24.000	-3.72	10.83	0666	.13	2.27	9.36	5.11	1.04	244.
25.000	-4.11	12.66	.0763		2.86	9.85	6.48	.76	249.
26.000	-4.61	14.55	.1149	.41 .70	2.54	10.80	8.17	.60	248.
27.000	-5.75	16.22	.1463	.92	2.28	12.78	8.64	-40	235.
28.000	-6.73	17.39	.1969	.92 .75	2.52	15.10	8.61	.28	204.
29.000	-8.08	18.13	.1303		2.50	16.85	8.33	.09	203.
30.000	-8.99	18.10	.2078	.76 .98	2.93	18.21	8.37	14	171.
32.000	-13.10	15.72	0794	.98	5.63	18.54	8.43	38	170.
34.000	-16.36	13.53	0977		3.87	18.49	9.48	09	69.
36.000	-18.64	13.20	.0186	.61	3.91	19.30	9.61	05	69.
38.000	-20.82	11.84	.2262	19	4.53	21.10	9.78	12	€9.
40.000	-15.22	14.57	.0551	1.44 1.95	5.50	22.97	9.02	11	69.
42.000	-7.55	16.68	.1952	1.22	5 67	19.65	10.96	.65	69.
44.000	1.97	17.55	0496	.51	5.41	15.57	11.00	1.20	69.
46.000	13.12	15.00	0040	2.00	7.63	17.24	8.29	.74	69.
48.000	19.99	15.16	.0481		6.95	17.68	11 61	.55	69.
50.000	23.82	17.65	.1950	2.92	7.23	22.88	12.84	.23	69.
52.000	30.53	18.42	.1172	5.69 6.40	7.38	27.22	14.93	.29	69.
54.000	36.38	17.53	.1020		8.42	33.36	16.40	. 32	70.
56.000	37.70	18.96	.1368	4.92	8.07	38.14	16.24	03	69.
58.000	34.58	21.60	.1573	3.82	9.22	39.58	17.54	08	64.
60.000	30.02	22.79		.40	8.14	36.81	19.24	.21	54.
62.000	27.53	21.66	.0453	41	9.16	34.42	17.72	.40	48.
64.000	26.70	19.06	1626	.62	14.68	34.00	16.61	1.46	38.
66.000	29.94	16.16	.1342	-2.59	15.26	33.55	13.34	.13	33.
68.000	31.14	17.53	.0729	-1.09	15.47	34.86	13.09	.77	29.
70.000	27.16	22.17	.0567	1.14	14.00	35.27	14.82	. 34	26.
	-7.40	25.17	3432	4.57	13.42	33.92	16.24	.25	26.

TABLE STATION	1. 4 = 913660	ATR GNIN	ristical PA Ein Missle	ARAMETERS.		A	PRIL		
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	skew ws	NOBS
KM	M/S	M/S		H/S	M/S	M/S	M/S	SVEN NO	כפטא
-002	-6.47	2.28	.2764	-1.90	2.45	7.22	2.13	48	422.
1.000	-8.58	4.01	.3460	91	2.98	9.36		23	427.
2.000	-6.23	4.23	. 1653	.22	2.69	7.29	3.29	.21	427.
3.000	-3.94	4.11	.0133	.40	2.65	5.61	2.84	.65	427.
4.000	-2.46	4.13	.0462	.40	2.77	4.88	2.66	.93	428.
5.000	-1.28	4.46	.0806	.43	2.97	4.75	5.85	.89	428.
6.000	38	4.96	.1382	цų	3.32	5.10	3.15	.94	428.
7.000	.65	5.34	.2363	.23	3.75	5.62	3.38	1.01	428.
8.000	2.41	5.96	.2267	.09	4.38	6.67	4.00	.72	428.
9.000	4.43	5.51	.1926	.50	4 65	7 AZ	4.73	.78	428.
10.000	6.17	6.94	.1507	1.58	5.19	9.41	5.20	.73	427.
11.000	7.65	7.31	.104B	2.69	F.66	10.93	5.60	.62	426.
12.000	8.87	7.85	.0595	2.72	5.92	12.10	6.01	.43	424.
13.000	9.86	8.38	0211	2.04	6.39	13.02	6.23	.42	422.
14.000	9.61	8.43	0567	.36	6.47	12.80	6.45	.52	421.
15.000	8.32	8.08	0006	-1.13	5.84	11.61	5.91	.62	418.
16.000	4.74	7.23	.0639	-2.04	4.40	8.67	4.78	.90	274.
17.000	1.15	6.52	.0469	-2.20	3.79	5.84	4.01	1.16	267.
18.000	-1.77	6.19	.1183	-1.28	3.16	6.28	3.68	1.08	267.
19.000	-1.59	7.59	.1359	32	2.41	7.25	3.64	.60	265.
20.000	-2.45	9.77	.0888	04	5.55	8.88	5.21	.56	261.
21.000	-3.79	10.02	0383	.43	2.53	9.22	6.00	.80	252.
22.000	-4.55	8.82	0266	.42	2.53	8.72	5.36	.97	253.
23.000	<del>-</del> 5.91	8.64	.0128	.27	2.06	8.82	6.00	.71	245.
24.000	-7.42	11.35	.0298	.24	3.06	11.15	8.29	.76	243.
25.000	-9.07	13.00	0362	.47	2.50	13.11	9.25	.54	240.
26.000	-10.14	14.28	.1301	.85	2.15	14.89	9.47	.34	225.
27.000	-12.45	14.80	.0901	1.05	2.48	16.96	9.65	.02	194.
28.000	-13.62	15.26	.0287	.81	2.45	17.94	19.12	.02	193.
29.000	-15.38	15.09	0641	.76	2.84	19.03	10.50	09	168.
30.000	-16.58	14.60	0707	.78	2.38	19.43	10.78	22	157.
32.000	-13.37	15.14	0536	.57	3.61	17.18	11.14	02	197.
34.000	-17.60	13.61	1166	~.46	3.36	19.05	11.95	02	60.
36.000	-20.79	11.01	.1639	06	4.07	21.56	10.24	.15	60. 61.
38.000	-18.33	10.54	0250	.65	5.06	19.49	9.62	.16	61.
40.000	-10.45	10.74	.1379	1.33	4.24	13.64	7.55	.71	61.
42.000	-2.03	12.59	.2424	1.36	5.33	11.57	7.54	.52	
44.000	3.50	10.53	.1175	2.80	6.85	11.30	6.96	.84	61. 61.
46.000	4.67	11.43	0369	2.10	5.20	11.36	8.04	1.65	61.
48.000	7.14	11.23	.0663	4.60	6.06	12.48	8.83	1.56	
50.000	10.17	10.97	1136	7.31	7.80	16.13	8.72	.87	61.
52.000	13.33	14.31	2193	6.19	7.81	18.72	11.37		60.
54.000	16.27	14.85	4154	5.30	8.80	21.21	11.76	.84 .81	60.
56.000	21.10	13.65	4251	2.22	10.19	24.61	11.47		57.
58.000	20.35	13.19	.3208	-2.00	8.18	23.39	10.44	.39	50.
60.000	22.07	13.50	.1737	-3.21	8.57	24.74	11.73	.38	44.
62.000	21.69	15.84	.2045	-2.93	10.05	24.74 26.18	11.76	.47	34.
64.000	23.36	18.30	.2145	-2.30	8.20	27.30	14.10	.33 05	28.
66.000	23.80	19.65	1544	-6.66	10.89	28.23	17.60		23.
68.000	17.04	27.42	0537	-12.57	14.11	28.23 33.19		.23	22.
70.000	4.44	29.36	0793	-12.20	13.58	32.58	16.27	09	21.
				14.60	13.35	36,38	10.18	23	19.

name of a Ministration of the Control of the Contro

Math   Mrs		1. 5 - 913660	ATR GNIW	TISTICAL P LEIN MISSL	ARAMETERS. E RAMGE		N	IAY		
M/S	Z	MEAN U				S.D. V	MEAN US	S O GC	CVCII I V	
1.000						M/S			SVEH MS	N095
1.0000 -8.54 3.61 2464 -3. 2.52 9.05 3.25 -18 443. 3.000 -5.96 4.02 .0644 .60 2.40 6.65 3.23 .51 442. 3.000 -5.96 4.02 .0644 .60 2.40 6.65 3.23 .51 442. 5.000 -2.47 4.05 .0544 .60 2.40 6.65 3.23 .51 442. 5.000 -2.47 4.05 .0544 .60 2.40 6.65 3.22 1.51 442. 6.000 -1.10 4.47 .1168 .49 3.29 4.67 2.92 1.21 442. 6.000 -2.45 5.19 .1017 .31 3.95 6.18 3.22 6.6 439. 9.000 4.15 5.59 .0665 .63 4.45 7.39 3.76 6.87 439. 11.000 5.67 6.21 .0564 1.69 4.90 6.67 4.73 .88 442. 9.000 4.15 5.59 .0665 .63 4.45 7.39 3.76 6.87 439. 11.000 7.22 7.3 -0.065 2.44 6.09 10.64 5.71 1.01 437. 12.000 8.92 7.48 -0.066 2.44 6.09 10.64 5.71 1.01 437. 12.000 8.92 7.48 -0.066 2.40 6.47 12.16 5.92 6.5 1.10 1.31 1.30 1.52 8.02 -0.254 1.66 6.89 13.60 6.39 13.60 6.39 14.51 1.55 1.50 11.55 7.58 1.056 -1.10 6.6 6.89 13.60 6.39 13.60 6.39 14.52 1.50 11.55 1.50 11.50 11.50 11.55 7.58 1.05 -1.10 6.6 6.87 13.60 6.39 13.60 6.39 14.52 1.50 11.				.2922	-1.30				- 13	4.70
3.000					3.					
1.000						2.38	8.00			
5.000 -2.47 4.05 .0249 .59 2.58 5.62 3.06 .88 442. 6.000 -1.10 4.47 1.168 .49 3.29 4.87 2.92 1.21 442. 6.000 -1.10 4.47 1.168 .49 3.29 4.87 2.92 1.21 442. 8.000 2.45 5.19 1.1017 .31 3.50 5.07 2.83 .88 442. 8.000 2.45 5.191017 .31 3.95 6.18 3.22 .68 493. 9.000 4.15 5.50 .0685 .63 4.45 7.35 3.76 .87 433. 10.000 5.57 6.21 .0858 1.59 4.90 9.67 4.73 .82 437. 11.000 7.22 7.330085 2.44 6.09 10.64 5.71 1.01 437. 12.000 8.92 7.880084 1.69 4.00 6.79 1.73 .82 .50 434. 13.000 10.52 8.020254 1.86 6.89 13.60 6.89 .37 432. 13.000 11.55 8.070255 1.02511 6.27 15.92 6.22 .21 423. 16.000 8.82 6.27 .235830 4.35 10.45 5.19 .30 265. 17.000 5.20 5.80 1.38869 3.48 7.55 5.99 3.30 6.57 17.00 5.20 5.80 1.38889 3.48 7.55 5.99 3.50 6.94 273. 19.000 -2.79 7.25 0.16522 2.59 6.95 4.31 82 271. 19.000 -2.79 7.25 0.16522 2.59 6.95 4.31 82 271. 19.000 -5.6.8 7.24 0.055  .61 2.33 9.78 5.99 3.8 253. 22.000 -8.76 7.01 0.0555  .61 2.33 9.78 5.99 3.8 253. 23.000 -12.35 10.86 0.088  .44 2.29 18.29 11.2913 225. 24.000 -14.72 12.960090 5.3 2.33 16.39 10.43 11.2213 225. 25.000 -14.72 13.76 0.072 7.0 2.009 13.56 0.09 11.55 1.90 10.43 11.2225 2.00 12.8 11.29 1.3 25. 26.000 -14.76 7.01 0.0555  .61 2.33 9.78 5.99 3.8 253. 24.000 -12.35 10.86 0.088  .44 2.29 18.29 10.43 11.2233 25. 25.000 -19.41 13.76 0.072 7.0 2.09 13.56 0.09 1.28 10.93 11.2225 2.00 1.29 1.29 0.09 7.3 3.9 3.00 2.00 1.29 1.50 1.36 0.09 1.35 0.09							6.85			
5.000							5.62			
7.000								2.86		
8.000 2.45 5.19 .1017 .31 3.95 6.18 3.22 6.69 439. 9.000 4.15 5.50 .06865 .63 4.45 7.35 3.76 .87 439. 10.000 5.67 6.21 .0584 1.69 4.90 8.67 4.73 .62 437. 11.000 7.22 7.30085 2.44 6.09 10.64 5.71 1.01 437. 12.000 8.92 7.480464 6.40 6.47 12.16 5.92 .60 434. 11.000 10.52 8.020254 1.86 6.89 13.60 6.39 .37 432. 11.000 11.55 8.17 .0015 .55 .10 6.89 13.60 6.39 .37 432. 11.000 11.55 7.58 .1025 -111 6.27 13.60 6.39 .37 432. 11.000 8.82 6.27 .2358 -30 4.36 10.45 5.19 .30 265. 11.000 8.82 6.27 .2358 -30 4.36 10.45 5.19 .30 265. 11.000 1.16 6.05032091 3.27 5.98 3.50 .89 273. 18.000 1.16 6.05032091 3.27 5.98 3.50 .89 273. 20.000 -2.79 7.25 .016522 2.59 6.95 4.31 .82 271. 20.000 -5.03 7.660035 .37 2.18 7.76 5.33 .86 6.52 271. 21.000 -6.8: 7.24 .0549 .83 2.43 8.74 5.45 .96 253. 22.000 -8.76 7.01 .0555 .61 2.33 9.78 5.99 .38 653. 23.000 -12.56 10.86 .0888 .44 2.93 14.12 8.94 .21 233. 25.000 -14.72 12.46 .0090 5.3 2.33 14.12 8.94 .21 233. 25.000 -19.41 13.62 .0688 .44 2.93 14.12 8.94 .21 233. 25.000 -19.41 13.62 .0688 .44 2.29 18.29 11.2913 215. 26.000 -20.99 12.86 .0099 .72 2.42 21.75 11.80 -48 173. 29.000 -20.99 13.56 .0099 .72 2.42 21.75 11.80 -48 173. 24.000 -17.33 14.79 .0552 .93 3.51 19.62 12.29 .25 198. 29.000 -20.69 13.56 .0099 .72 2.42 21.75 11.80 -48 173. 24.000 -17.33 14.79 .0552 .93 3.51 19.62 12.29 .25 198. 29.000 -20.69 13.56 .0099 .72 2.42 21.75 11.80 -48 173. 24.000 -17.33 14.79 .0552 .93 3.51 19.62 12.99 .00 73. 25.000 -19.41 13.76 .0772 .70 2.49 20.52 12.29 .25 198. 26.000 -19.41 13.62 .0688 .44 2.93 15.95 11.95 11.95 .25 20.95 .90 .90 73. 24.000 -19.41 13.62 .0689 .49 2.93 15.95 11.99 .90 .90 73. 25.000 -19.41 13.76 .0772 .70 2.49 2.55 12.29 .25 198. 26.000 -19.41 13.76 .0772 .70 2.49 2.55 12.29 .25 198. 27.000 -19.41 13.62 .0688 .49 2.91 13.90 11.99 .70 2.90 .90 73. 28.000 -19.41 2.20 .916 .918 .919 11.99 .90 .90 73. 29.000 -20.69 12.85 .009 .93 3.00 1.99 11.99 .70 .90 .90 .90 .90 .90 .90 .90 .90 .90 .9								2.92	1.21	
9.000 4.15 5.53 .0685 .63 4.95 7.39 3.76 87 438. 10.000 5.67 6.2! .0584 1.69 4.90 6.67 4.73 .82 437. 11.000 7.22 7.30085 2.44 6.09 10.64 5.71 1.01 437. 12.000 8.92 7.480464 2.40 6.47 12.16 5.92 .60 439. 13.000 10.52 8.020254 1.66 6.89 13.60 6.39 .37 432. 14.000 10.52 8.020254 1.66 6.89 13.60 6.39 .37 432. 15.000 11.55 8.02 .60 1025 -11 6.27 13.92 6.22 .21 423. 16.000 8.62 6.27 .235830 4.36 10.45 5.19 .30 265. 17.000 5.20 5.80 138868 3.48 7.63 3.86 6.55 277. 19.000 -2.79 7.25 .016522 2.59 6.95 4.31 82 271. 20.000 -5.03 7.660035 .37 2.18 7.76 5.34 .86 268. 27.000 -8.76 7.01 .0555 .61 2.33 8.74 5.45 8.22 .82 2.21 2.20 2.20 2.20 2.20 2.20 2.20 2.2									.88	
10.000								3.22	.68	
11.000 7.22 7.13 -0.0055 2.44 6.09 10.66 5.71 1.01 437. 12.000 8.92 7.48 -0.046 2.40 6.47 12.16 5.92 6.0 434. 13.000 10.52 8.02 7.025 1.86 6.89 13.60 6.38 .37 432. 14.000 11.52 8.17 .0015 .35 0.00 13.60 6.39 .37 432. 15.000 11.65 7.58 .1025 -111 6.27 13.92 6.22 .21 423. 16.000 8.82 6.27 .2358 -30 4.35 10.45 5.19 .30 265. 17.000 5.20 5.80 1.388 -68 3.48 7.63 3.86 .65 277. 18.000 .16 6.05 -0.320 -91 3.27 5.99 3.50 .84 273. 19.000 -2.79 7.25 .0165 -22 2.59 6.95 4.31 .02 271. 20.000 -5.03 7.66 -0.035 .37 2.18 7.76 5.34 .86 268. 22.000 -5.03 7.66 -0.035 .37 2.18 7.76 5.34 .86 268. 22.000 -6.86 7.24 0.0545 83 2.43 8.74 5.45 8.99 38 253. 23.000 -10.57 8.24 0.0805 .40 1.86 11.55 7.21 .26 234. 24.000 -12.35 10.86 .0888 .44 2.93 11.15 7.21 .26 234. 24.000 -12.35 10.86 .0888 .44 2.93 11.15 9.94 21 233. 25.000 -14.72 12.46 -0.0900 .53 2.33 16.39 10.43 .11 227. 26.000 -18.44 13.62 .0886 .44 2.29 18.29 11.29 -1.3 215. 27.000 -18.49 13.56 .0090 .93 3.50 2.17 11.29 -1.3 215. 28.000 -19.41 13.56 .0090 .93 3.50 2.173 12.23 -25 10.9 13.60 .0090 .72 2.42 21.75 11.80 -48 173. 34.000 -20.99 12.86 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.99 12.86 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -21.23 11.94 -2.352 2.66 3.31 21.34 10.81 -0.9 73. 34.000 -21.23 11.94 -2.352 2.66 3.31 21.34 10.81 -0.9 73. 34.000 -20.99 12.86 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.99 12.86 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.89 13.55 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.89 13.55 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.89 13.55 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.89 13.55 .0099 .72 2.42 21.75 11.90 -48 173. 34.000 -20.89 13.55 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.89 13.55 .0099 .72 2.42 21.75 11.80 -48 173. 34.000 -20.89 13.55 .0096 .61 6.36 10.16 5.77 .89 3.44 10.81 -0.9 73. 34.000 -20.89 13.55 .0096 .61 6.36 10.16 5.77 .89 3.44 10.81 -0.9 73. 34.000 -20.89 13.50 .0096 .70 3.50 4.9 11.11 11.11 4.0 59. 34.000 -3.73 26.75 .11 9.0052 .39 9.29 25.52 11.11 11.17 4.0 59. 34.000 -3.73 26.75 .11 9.0052 .39									.87	
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15.000										
16.000       8.82       6.27       .2358      30       4.36       10.95       5.29       .21       423         17.000       5.20       5.80       .1398      68       3.48       7.63       3.86       .65       277         18.000       .16       6.05      0220      91       3.27       5.98       3.50       .94       273         19.000       -2.79       7.25       .0165      22       2.59       6.95       4.31       .62       271         20.000       -5.03       7.66       -0035       .37       2.18       7.76       5.34       .06       268         27.000       -6.8       7.24       .0594       .93       2.43       9.74       5.99       .38       .253         22.000       -8.76       7.01       .0555       .61       2.33       9.78       5.99       .38       .253         23.000       -12.36       10.86       .0808       .44       2.93       14.12       8.94       .21       .233         25.000       -14.72       12.46       .0090       .53       2.33       16.39       10.43       .11       .227       .20       .20       11.2										
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21.000         -6.8:         7.24         .0549         .83         2.43         8.74         5.45         .96         253.           22.000         -8.76         7.01         .0555         .61         2.33         9.78         5.99         .38         253.           23.000         -12.35         10.86         .0888         .44         2.93         14.12         8.94         .21         233.           25.000         -14.72         12.46        0090         .53         2.33         16.39         10.43         .11         227.           26.000         -16.80         13.20        0537         .44         2.29         18.29         11.29        13         215.           27.000         -16.80         13.20        0537         .44         2.29         18.29         11.29        13         215.           27.000         -18.44         13.62         .0060         .41         2.52         19.72         11.95        25         200.           29.000         -20.69         13.55         .0409         .93         3.02         21.73         12.23        34         173.           30.000         -20.69         12.86	20.000									
22.000 -8.76 7.01 .0555 .61 2.33 9.78 5.99 .38 253. 23.000 -10.67 8.24 .0805 .40 1.96 11.55 7.21 .26 234. 24.000 -12.36 10.86 .0888 .44 2.93 14.12 8.94 .21 233. 25.000 -14.72 12.460090 .53 2.33 16.39 10.43 .11 227. 26.000 -16.80 13.200537 .44 2.29 18.29 11.2913 215. 27.000 -18.44 13.62 .0080 .41 2.52 19.72 11.9525 200. 28.000 -19.41 13.76 .0772 .70 2.40 20.52 12.2925 199. 29.000 -20.69 13.56 .0409 .93 3.02 21.73 12.2334 173. 30.000 -20.99 12.86 .0098 .72 2.42 21.75 11.8048 173. 32.000 -17.33 14.79 .0532 .93 3.51 19.62 12.09 .00 73. 34.000 -20.48 11.942362 .26 3.31 21.34 10.8109 73. 36.000 -21.22 9.16198002 3.87 21.70 8.83 .00 73. 38.000 -18.20 8.73 .0137 .56 4.94 19.11 8.16 113 73. 49.000 -1.19.20 8.73 .0137 .56 4.94 19.11 8.16 113 73. 49.000 -5.39 8.23 .0956 .61 5.36 10.16 5.77 .79 73. 44.000 -5.39 8.23 .0956 .61 5.36 10.16 5.77 .79 73. 48.000 -7.39 9.31 .1003 1.81 5.29 10.94 7.20 1.26 73. 48.000 -9.56 12.85 .0319 3.08 6.87 15.14 9.07 .80 72. 54.000 -9.56 12.85 .0319 3.08 6.87 15.14 9.07 .80 72. 54.000 -5.74 16.192286 4.03 7.65 19.05 10.26 .44 57. 58.000 -7.33 21.13 .0808 1.77 8.78 21.19 11.17 .40 59. 54.000 -7.33 21.13 .0808 1.77 8.78 21.19 11.17 .40 59. 54.000 -7.35 26.01 .0263 -8.95 11.21 27.70 16.16 .95 46.	21.000									
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27.000 -18.44			12.46	0030			15.39			
27.000 -18.44			13.20	0537						
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34.000       -20.48       11.94       -25362       .26       3.31       21.34       10.81      09       73.         36.000       -21.22       9.16      1980      02       3.87       21.70       8.83       .00       73.         38.000       -18.20       8.73       .0137       .56       4.94       19.11       8.16       .13       73.         40.000       -11.92       9.78       .2121       1.81       4.95       13.95       6.75       .25       73.         42.000       -6.04       7.75       .0095       2.16       5.19       10.04       5.15       .26       73.         46.000       -7.39       9.31       .1003       1.81       5.29       10.94       7.20       1.26       73.         48.000       -8.38       10.58       .1210       3.56       6.95       13.16       8.33       .68       72.         50.000       -9.56       12.85       .0319       3.08       6.87       15.14       9.07       .80       72.         52.000       -8.33       14.52      1519       4.25       7.00       15.90       9.60       .93       72.         54.00						2.42	21.75		. –	
36.000 -21.22 9.16 -1.98002 3.87 21.70 8.83 .00 73. 38.000 -18.20 8.73 .0137 .56 4.94 19.11 8.16 .13 73. 40.000 -1.1.92 9.74 .2121 1.81 4.55 13.95 6.75 .25 73. 42.000 -6.04 7.75 .0095 2.16 5.19 10.04 5.15 .26 73. 44.000 -5.39 8.23 .0956 .61 6.36 10.16 5.77 .79 73. 46.000 -7.39 9.31 .1003 1.81 5.29 10.94 7.20 1.26 73. 48.000 -6.38 10.58 .1210 3.66 6.95 13.16 8.33 .88 72. 50.000 -9.56 12.85 .0319 3.08 6.87 15.14 9.07 .80 72. 52.000 -8.33 14.521519 4.25 7.00 15.90 9.60 .93 72. 54.000 -5.74 16.192286 4.03 7.63 17.04 8.69 .59 71. 56.000 -6.96 17.930563 3.39 9.56 19.05 10.26 .44 57. 58.000 -7.33 21.13 .0808 1.77 8.78 21.19 11.17 .40 59. 60.000 -7.44 26.14 .3291 1.34 7.33 23.75 14.84 .65 51. 64.000 -3.73 26.51 .0097 -1.04 10.86 25.90 12.51 .31 48. 64.000 -3.73 26.51 .0097 -1.04 10.86 25.90 12.51 .31 48. 64.000 -7.35 28.01 .0263 -8.85 11.21 27.70 16.16 .95 46.						3.51	19.62	12.09		
38.000         -18.20         9.16        1980        02         3.87         21.70         8.83         .00         73.           38.000         -18.20         8.73         .0137         .56         4.94         19.11         8.16         .13         73.           49.000         -1.92         9.78         .2121         1.81         4.55         13.95         6.75         .25         73.           42.000         -6.04         7.75         .0095         2.16         5.19         10.04         5.15         .26         73.           44.000         -5.39         8.23         .0956         .61         6.36         10.16         5.77         .79         73.           46.000         -7.39         9.31         .1003         1.81         5.29         10.94         7.20         1.26         73.           48.000         -6.38         10.58         .1210         3.56         6.95         13.16         8.33         .68         72.           50.000         -9.56         12.85         .0319         3.08         6.87         15.14         9.07         .80         72.           52.000         -8.33         14.52        1519							21.34	10.81		
88.000       -18.20       8.73       .0137       .56       4.94       19.11       8.16       .13       73.         40.000       -11.92       9.78       .2121       1.81       4.55       13.95       6.75       .25       73.         42.000       -6.04       7.75       .0095       2.16       5.19       10.04       5.15       .26       73.         44.000       -5.39       6.23       .0956       .61       6.36       10.16       5.77       .79       73.         46.000       -7.39       9.31       .1003       1.81       5.29       10.94       7.20       1.26       73.         48.000       -8.38       10.58       .1210       3.56       6.95       13.16       8.33       .69       72.         50.000       -9.56       12.85       .0319       3.08       6.87       15.14       9.07       .80       72.         52.000       -8.33       14.52      1519       4.25       7.00       15.90       9.60       .93       72.         54.000       -5.74       16.19      2286       4.03       7.63       17.04       8.69       .59       71.         56.000 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>21.70</td> <td>8.83</td> <td>.00</td> <td></td>							21.70	8.83	.00	
42.000         -6.04         7.75         .0095         2.16         5.19         10.04         5.15         .25         73.           44.000         -5.39         8.23         .0956         .61         6.36         10.16         5.77         .79         73.           46.000         -7.39         9.31         .1003         1.81         5.29         10.94         7.20         1.26         73.           48.000         -8.38         10.58         .1210         3.56         6.95         13.16         8.33         .68         72.           50.000         -9.56         12.85         .0319         3.08         6.87         15.14         9.07         .80         72.           52.000         -8.33         14.52        1519         4.25         7.00         15.90         9.60         .93         72.           54.000         -5.74         16.19        2280         4.03         7.63         17.04         8.69         .59         71.           58.000         -6.96         17.93        0563         3.39         9.56         19.05         10.26         .44         67.           58.000         -7.33         21.13         .0809 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>8.16</td> <td>.13</td> <td></td>								8.16	.13	
44.000       -5.39       6.23       .0956       .61       6.36       10.16       5.77       .79       73.         46.000       -7.39       9.31       .1003       1.81       5.29       10.94       7.20       1.26       73.         48.000       -8.38       10.58       .1210       3.56       6.95       13.16       8.33       .68       72.         50.000       -9.56       12.85       .0319       3.08       6.87       15.14       9.07       .80       72.         52.000       -8.33       14.52      1519       4.25       7.00       15.90       9.60       .93       72.         54.000       -5.74       16.19      2280       4.03       7.63       17.04       8.69       .59       71.         56.000       -6.96       17.93       -0563       3.39       9.56       19.05       10.26       .44       67.         58.000       -7.33       21.13       .0808       1.77       8.78       21.19       11.17       .40       59.         62.000       -7.44       26.14       .3291       1.34       7.33       23.75       14.84       .65       51.         64.00			-					6.75	.25	
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15.000 5.61 7.57 .175144 5.43 9.56 5.20 .58 394. 16.000 3.29 7.05 .111439 4.12 7.63 4.38 1.32 258. 17.00068 5.66 .012040 3.44 5.71 3.43 1.01 255. 18.000 -4.92 6.28048777 3.06 7.39 4.34 .53 256. 19.000 -6.88 5.300617 .04 2.43 7.90 4.34 .53 256. 20.000 -8.25 5.04 .0354 .22 2.21 8.87 4.44 2.4 251. 21.000 -10.59 6.06 .0853 .77 2.60 11.34 5.26 .04 245. 22.000 -12.89 7.92 .0755 .87 2.42 13.47 7.35 .03 244. 23.000 -14.98 9.60 .0016 .79 2.00 15.46 9.05 .10 233. 24.000 -16.79 11.500777 .64 2.85 17.57 10.67 .03 232. 25.000 -18.49 12.54 .0512 .87 2.45 19.17 11.7607 228. 26.000 -19.93 13.64 .0410 .83 2.29 20.56 12.90 -1.15 218. 27.000 -21.65 14.260374 .64 2.80 22.46 13.2524 196. 28.000 -24.87 13.28 .0859 .97 2.61 25.14 12.0534 195. 29.000 -24.87 13.28 .0959 .97 2.61 25.14 12.0534 195. 29.000 -24.96 10.920943 54 3.29 20.56 10.9015 73. 34.000 -22.88 9.57 .082358 3.01 24.22 9.1903 72. 38.000 -24.01 9.34 .0667 -1.31 3.63 24.94 9.0031 72. 38.000 -24.01 9.34 .0067 -1.31 3.63 24.94 9.0031 72. 38.000 -24.98 11.63 .0960 .87 2.21 25.27 11.4845 163. 24.000 -20.22 9.73 .0090 1.46 4.56 21.24 4.99 9.0031 72. 38.000 -24.99 9.17 .0661 .27 4.99 2.265 9.7505 72. 40.000 -20.29 10.57 .06604 1.79 5.65 21.55 9.79 .23 73. 44.000 -20.29 10.57 .06604 1.79 5.65 21.25 9.79 .23 73. 45.000 -20.12 17.54 .0060 5.35 1.18 5.89 24.99 11.30 .30 73. 25.000 -25.41 14.80 .0398 4.97 8.65 21.25 9.79 .23 73. 25.000 -25.41 14.80 .0398 4.97 8.65 21.25 9.79 .23 73. 25.000 -25.41 14.80 .0398 4.97 8.65 21.25 9.79 .23 73. 25.000 -25.41 14.80 .0398 4.97 8.65 21.25 9.79 .23 73. 25.000 -25.41 14.80 .0398 4.97 8.65 21.25 9.11 1.36 14.46 4.56 21.24 9.19 1.36 14.46 55. 25.000 -25.41 14.80 .0398 4.97 8.65 21.25 9.19 10.70 .15 73. 25.000 -25.41 14.80 .0398 4.97 8.65 21.25 9.19 10.70 .15 73. 25.000 -25.41 14.80 .0398 4.97 8.65 27.98 13.54 3.9 72. 25.000 -25.41 14.80 .0398 4.97 8.65 27.98 13.54 3.9 72. 25.000 -25.41 14.80 .0398 4.97 8.65 27.98 13.54 3.9 72. 25.000 -25.41 14.80 .0398 4.97 8.65 27.98 13.54 3.9 72. 2	14.000									
16.000	15.000	5.61	7.57							
17.000	16.000	3.29								
18.000	17.000	68								
19.000	18.000									
20.000         -8.25         5.04         .0354         .22         2.21         8.87         4.44         .24         251           21.000         -10.59         6.06         .0853         .77         2.60         11.34         5.26         .04         245           22.000         -12.89         7.92         .0755         .87         2.42         13.47         7.35         .03         244           23.000         -14.98         9.60         .0016         .79         2.00         15.46         9.05         .10         233           25.000         -16.79         11.50        0777         .64         2.85         17.57         10.67         .03         232           25.000         -18.49         12.54         .0512         .87         2.45         19.17         11.76         -07         228           25.000         -19.93         13.64         .0410         .83         2.29         2.56         12.90         -15         218           27.000         -21.65         14.26        0374         .64         2.80         22.46         13.25         -24         196           28.000         -24.87         12.28         .0859 <td>19.000</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>200.</td>	19.000									200.
21.000	20.000									253.
22.000 -12.89	21.000									
23.000 -14.98	22.000									
24.000	23.000									
25.000 -18.49 12.54 .0512 .87	24.000									
26.000         -19.93         13.64         .0410         .83         2.29         20.56         12.90        15         218.           27.000         -21.65         14.26        0374         .64         2.80         22.46         13.25        24         196.           28.00L         -23.01         13.28        0223         .58         2.34         23.38         12.95        34         195.           29.000         -24.87         12.28         .0859         .97         2.61         25.14         12.05        47         170.           30.000         -24.87         12.28         .0859         .97         2.61         25.14         12.05        47         170.           30.000         -24.86         10.92        0943         .54         3.29         24.78         10.69        15         73.           34.000         -23.88         9.57         .0823        58         3.01         24.22         9.19        03         72.           38.000         -24.01         9.34         .0657         -1.31         3.63         24.44         9.00        31         72.           40.000         -20.21         9.73 <td>25.000</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	25.000									
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28.00L -23.01 13.280223 .58 2.34 23.38 12.8534 195. 23.000 -24.87 12.28 .0859 .97 2.61 25.14 12.0547 170. 30.001 -25.09 11.63 .0960 .87 2.21 25.27 11.4845 169. 32.000 -24.46 10.920943 54 3.29 24.78 10.6915 73. 34.000 -23.88 9.57 .082358 3.01 24.22 9.1903 72. 36.000 -24.01 9.34 .0067 -1.31 3.63 24.44 9.0031 72. 38.000 -21.94 9.17 .0261 .27 4.96 22.65 8.7505 72. 40.000 -20.24 9.73 .0090 1.46 4.56 21.24 6.73 .15 72. 42.000 -20.29 10.570604 1.78 5.65 21.55 9.79 .23 73. 44.000 -21.92 10.760535 1.18 5.89 22.90 10.35 .56 73. 46.000 -23.92 11.500185 2.29 5.94 24.84 11.30 .30 73. 48.000 -25.81 11.371557 3.82 5.67 27.92 10.70 .15 73. 50.00C -27.54 11.610092 5.35 7.42 29.11 11.36 .14 73. 52.000 -20.12 17.540076 3.51 9.04 24.03 14.46 .44 67. 56.000 -14.78 18.31 .0621 2.42 10.96 22.81 12.43 .71 64. 56.000 -2.46 13.74 .1434 3.63 10.90 16.04 7.86 .34 45. 62.010 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 54.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46	27.000									
29.000       -24.87       12.28       .0859       .97       2.61       25.14       12.05      47       170.         30.000       -25.09       11.63       .0960       .87       2.21       25.27       11.48      45       169.         32.000       -24.46       10.92      0943       54       3.29       24.78       10.69      15       73.         34.000       -24.01       9.34       .0067       -1.31       3.63       24.44       9.00      31       72.         38.000       -21.94       9.17       .0261       .27       4.95       22.65       9.75      05       72.         40.000       -20.24       9.73       .0090       1.46       4.56       21.24       8.73       .15       72.         42.000       -20.29       10.57      0604       1.78       5.85       21.55       9.79       .23       73.         44.000       -21.92       10.76      05355       1.18       5.89       22.90       10.35       .56       73.         48.000       -26.81       11.37      1557       3.82       5.67       27.92       10.70       .15       73.	28.000									
30.000 -25.09 11.63 .0960 .87 2.21 25.27 11.4845 163. 32.000 -24.46 10.920943 54 3.29 24.78 10.6915 73. 34.000 -23.88 9.57 .082358 3.01 24.22 9.1903 72. 36.000 -24.01 9.34 .0067 -1.31 3.63 24.44 9.0031 72. 38.000 -21.94 9.17 .0261 .27 4.99 22.65 9.7505 72. 40.000 -20.24 9.73 .0090 1.46 4.56 21.24 8.73 .15 72. 42.000 -20.29 10.570604 1.79 5.85 21.55 9.79 .23 73. 44.000 -21.92 10.760535 1.18 5.89 22.90 10.35 .56 73. 46.000 -23.92 11.500185 2.29 5.94 24.84 11.30 .30 73. 48.000 -26.81 11.371557 3.82 5.67 27.92 10.70 .15 73. 50.000 -27.54 11.610092 5.35 7.42 29.11 11.36 .14 73. 52.000 -25.41 14.80 .0398 4.97 8.85 27.98 13.54 .39 72. 54.000 -20.12 17.540076 3.51 9.04 24.03 14.46 .44 67. 56.000 -5.14 17.38 .0487 1.26 11.18 18.39 10.54 .46 56. 60.000 -2.46 13.74 .1434 3.63 10.90 16.04 7.86 .34 45. 62.010 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 54.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46									-	
32.000 -24.46 10.920943 54 3.29 24.78 10.6915 73. 34.000 -23.88 9.57 .082358 3.01 24.22 9.1903 72. 36.000 -24.01 9.34 .0067 -1.31 3.63 24.44 9.0031 72. 38.000 -21.94 9.17 .0261 .27 4.96 22.65 9.7505 72. 40.000 -20.24 9.73 .0090 1.46 4.56 21.24 8.73 .15 72. 42.000 -20.29 10.570604 1.79 5.85 21.55 9.79 .23 73. 44.000 -21.92 10.760535 1.18 5.89 22.90 10.35 .56 73. 44.000 -23.92 11.500185 2.29 5.94 24.84 11.30 .30 73. 48.000 -26.81 11.371557 3.82 5.67 27.92 10.70 .15 73. 50.000 -27.54 11.610092 5.35 7.42 29.11 11.36 .14 73. 52.000 -25.41 14.80 .0398 4.97 8.85 27.98 13.54 .39 72. 54.000 -20.12 17.540076 3.51 9.04 24.03 14.46 .44 67. 56.000 -14.78 18.31 .0621 2.42 10.96 22.81 12.43 .71 64. 56.000 -5.14 17.380487 1.26 11.18 18.39 10.54 .46 56. 60.000 -2.46 13.74 .14.34 3.63 10.90 16.04 7.86 .34 45. 62.010 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 54.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46 36.	30.000									
34.000       -23.88       9.57       .0823      58       3.01       24.22       9.19      03       72.         36.000       -24.01       9.34       .0067       -1.31       3.63       24.44       9.00      31       72.         38.000       -21.94       9.17       .0261       .27       4.99       22.65       9.75      05       72.         40.000       -20.24       9.73       .0090       1.46       4.56       21.24       8.73       .15       72.         42.000       -20.29       10.57      0604       1.79       5.85       21.55       9.79       .23       73.         44.000       -21.92       10.76      0535       1.18       5.89       22.90       10.35       .56       73.         46.000       -23.92       11.50      0185       2.29       5.94       24.84       11.30       .30       73.         48.000       -26.81       11.37      1557       3.82       5.67       27.92       10.70       .15       73.         50.000       -27.54       11.61      0092       5.35       7.42       29.11       11.36       .14       73.										
38.000         -24.01         9.34         .0057         -1.31         3.63         24.44         9.00        31         72.           38.000         -21.94         9.17         .0261         .27         4.99         22.65         9.75        05         72.           40.000         -20.24         9.73         .0090         1.46         4.56         21.24         8.73         .15         72.           42.000         -20.29         10.57        0604         1.78         5.85         21.55         9.79         .23         73.           44.000         -21.92         10.76        0535         1.18         5.89         22.90         10.35         .56         73.           46.000         -23.92         11.50        0185         2.29         5.94         24.84         11.30         .30         73.           48.000         -26.81         11.37        1557         3.82         5.67         27.92         10.70         .15         73.           50.000         -27.54         11.61        0092         5.35         7.42         29.11         11.36         .14         73.           52.000         -25.41         14.80										
38.000 -21.94 9.17 .C261 .27 4.96 22.65 8.75 -0.05 72. 40.000 -20.24 9.73 .0090 1.46 4.56 21.24 8.73 .15 72. 42.000 -20.29 10.570604 1.76 5.85 21.55 9.79 .23 73. 44.000 -21.92 10.760535 1.18 5.89 22.90 10.35 .56 73. 44.000 -23.92 11.500185 2.29 5.94 24.84 11.30 .30 73. 48.000 -26.81 11.371557 3.82 5.67 27.92 10.70 .15 73. 50.000 -27.54 11.610092 5.35 7.42 29.11 11.36 .14 73. 52.000 -25.41 14.80 .0398 4.97 8.85 27.98 13.54 .39 72. 54.000 -20.12 17.540076 3.51 9.04 24.03 14.46 .44 67. 56.000 -14.78 18.31 .0621 2.42 10.96 22.81 12.43 .71 64. 56.000 -5.14 17.380487 1.26 11.18 18.39 10.54 .46 56. 60.000 -2.46 13.74 .1434 3.63 10.90 16.04 7.86 .34 45. 62.010 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 54.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46 36.										
40.000       -20.24       9.73       .0090       1.46       4.56       21.24       8.73       .15       72.         42.000       -20.29       10.57      0604       1.79       5.85       21.55       9.79       .23       73.         44.000       -21.92       10.76      0535       1.18       5.89       22.90       10.35       .56       73.         46.000       -23.92       11.50      0185       2.29       5.94       24.84       11.30       .30       73.         48.000       -26.81       11.37      1557       3.82       5.67       27.92       10.70       .15       73.         50.000       -27.54       11.61      0092       5.35       7.42       29.11       11.36       .14       73.         52.000       -25.41       14.80       .0398       4.97       8.85       27.98       13.54       .39       72.         54.000       -20.12       17.54      0076       3.51       9.04       24.03       14.46       .44       67.         58.000       -5.14       17.38      0487       1.26       11.18       18.39       10.54       .46       56.      <	38.000									
42.000       -20.29       10.57      0604       1.7a       5.85       21.55       9.79       .23       73.         44.000       -21.92       10.76      0535       1.18       5.89       22.90       10.35       .56       73.         46.000       -23.92       11.50      0185       2.29       5.94       24.84       11.30       .30       73.         48.000       -26.81       11.37      1557       3.82       5.67       27.92       10.70       .15       73.         50.000       -27.54       11.61      0092       5.35       7.42       29.11       11.36       .14       73.         52.000       -25.41       14.80       .0398       4.97       8.85       27.98       13.54       .39       72.         54.000       -20.12       17.54      0076       3.51       9.04       24.03       14.46       .44       67.         56.000       -14.78       18.31       .0621       2.42       10.96       22.81       12.43       .71       64.         58.000       -5.14       17.38      0467       1.26       11.18       18.39       10.54       .46       56.										
44.000       -21.92       10.76      0535       1.18       5.89       22.90       10.35       .56       73.         46.000       -23.92       11.50      0185       2.29       5.94       24.84       11.30       .30       73.         48.000       -26.81       11.37      1557       3.82       5.67       27.92       10.70       .15       73.         50.000       -27.54       11.61      0092       5.35       7.42       29.11       11.36       .14       73.         52.000       -25.41       14.80       .0338       4.97       8.85       27.98       13.54       .39       72.         54.000       -20.12       17.54      0076       3.51       9.04       24.03       14.46       .44       67.         56.000       -14.78       18.31       .0621       2.42       10.96       22.81       12.43       .71       64.         58.000       -5.14       17.38      0467       1.26       11.18       18.39       10.54       .46       56.         60.000       -2.46       13.74       .1434       3.63       10.90       16.04       7.86       .34       45.										
46.000       -23.92       11.50      0185       2.29       5.94       24.84       11.30       .30       73.         48.000       -26.81       11.37      1557       3.82       5.67       27.92       10.70       .15       73.         50.000       -27.54       11.61      0092       5.35       7.42       29.11       11.36       .14       73.         52.000       -25.41       14.80       .0398       4.97       8.85       27.98       13.54       .39       72.         54.000       -20.12       17.54      0076       3.51       9.04       24.03       14.46       .44       67.         56.000       -14.78       18.31       .0621       2.42       10.96       22.81       12.43       .71       64.         50.000       -5.14       17.38      0487       1.26       11.18       18.39       10.54       .46       56.         60.000       -2.46       13.74       .1434       3.63       10.90       16.04       7.86       .34       45.         62.010       4.00       16.22       .0318       .45       13.46       18.97       9.53       .56       37. <tr< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr<>										
48.000       -26.81       11.37      1557       3.82       5.67       27.92       10.70       .15       73.         50.000       -27.54       11.61      0092       5.35       7.42       29.11       11.36       .14       73.         52.000       -25.41       14.80       .0398       4.97       8.85       27.98       13.54       .39       72.         54.000       -20.12       17.54      0076       3.51       9.04       24.03       14.46       .44       67.         56.000       -14.78       18.31       .0621       2.42       10.96       22.81       12.43       .71       64.         58.000       -5.14       17.38      0487       1.26       11.18       18.39       10.54       .46       56.         60.000       -2.46       13.74       .1434       3.63       10.90       16.04       7.86       .34       45.         62.010       4.00       16.22       .0318       .45       13.46       18.97       9.53       .56       37.         54.000       7.97       15.71       .0118       -4.28       12.30       19.92       8.61       .46       36. <td></td>										
50.00C       -27.54       11.61      0092       5.35       7.42       29.11       11.36       .14       73.         52.000       -25.41       14.80       .0398       4.97       8.85       27.98       13.54       .39       72.         54.000       -20.12       17.54      0076       3.51       9.04       24.03       14.46       .44       67.         56.000       -14.78       18.31       .0621       2.42       10.96       22.81       12.43       .71       64.         58.000       -5.14       17.38      0487       1.26       11.18       18.39       10.54       .46       56.         60.000       -2.46       13.74       .1434       3.63       10.90       16.04       7.86       .34       45.         62.030       4.00       16.22       .0318       .45       13.46       18.97       9.53       .56       37.         54.000       7.97       15.71       .0118       -4.28       12.30       19.92       8.61       .46       36.										
52.000 -25.41 14.80 .0398 4.97 8.85 27.98 13.54 .39 72. 54.000 -20.12 17.540076 3.51 9.04 24.03 14.46 .44 67. 56.000 -14.78 18.31 .0621 2.42 10.96 22.81 12.43 .71 64. 58.000 -5.14 17.380487 1.26 11.18 18.39 10.54 .46 56. 60.000 -2.46 13.74 .1434 3.63 10.90 16.04 7.86 .34 45. 62.010 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 64.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46 36.										
54.000     -20.12     17.54    0076     3.51     9.04     24.03     14.46     .44     67.       56.000     -14.78     18.31     .0621     2.42     10.96     22.81     12.43     .71     64.       58.000     -5.14     17.38    0487     1.26     11.18     18.39     10.54     .46     55.       60.000     -2.46     13.74     .1434     3.63     10.90     16.04     7.86     .34     45.       62.030     4.00     16.22     .0318     .45     13.46     18.97     9.53     .56     37.       54.000     7.97     15.71     .0118     -4.28     12.30     19.92     8.61     .46     36.										
56.000 -14.78 18.31 .0621 2.42 10.96 22.81 12.43 .71 64. 58.000 -5.14 17.380487 1.26 11.18 18.39 10.54 .46 56. 60.000 -2.46 13.74 .1434 3.63 10.90 16.04 7.86 .34 45. 62.010 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 64.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46 36.		-20.12								
58.000 -5.14 17.380467 1.26 11.18 18.39 10.54 .46 55. 60.000 -2.46 13.74 .1434 3.63 10.90 16.04 7.86 .34 45. 62.010 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 54.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46 36.										
60.000 -2.46 13.74 .1434 3.63 10.90 16.04 7.86 .34 45. 62.030 4.00 16.22 .0318 .45 13.46 18.97 9.53 .56 37. 54.000 7.97 15.71 .0118 -4.28 12.30 19.92 8.61 .46 36.										
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58.000 -1.03 23.93 .2679 -7.72 14.60 26.47 11.24 .37 34. 70.000 -15.27 29.04 .1218 -13.10 19.05 36.70 15.24 - 05 30										

New York   New York	TABLE STATION	1. 7 = 913560		ISTICAL PA			J	ULY		
M/S   M/S	Z	MEAN U	5.D. U	R(U,V)	HEAN V	S.D. V	MEAN HS	S.D. US	פעדט טפ	MODE
1.000	KM	H/5	M/S	Ť	H/S				then no	.,,,,,,
1.000         -6.21         4.28         1.543         .59         2.91         7.45         3.19         1.8         400         3.000         -6.33         3.5         .0935         3.8         2.58         7.37         3.02         .39         411         401         3.000         -6.63         7.63        0152         .74         2.55         7.43         2.99         .11         401         400         -6.73         3.53        05536         .76         2.72         7.52         3.00         .37         401         5.000         -6.59         3.77        0877         .55         2.80         7.46         3.19         .48         401         5.000         -6.500         -8.000         -4.97         4.10         .0483         3.56         6.86         3.30         3.29         .64         400         8.000         -4.11         4.97         .0297         .49         3.28         .62         3.03         .63         400         .60         8.00         .46         3.03         .62         400         .80         8.00         .40         .80         3.03         .62         400         .80         3.02         .75         300         .60         3.03         .75	.002	-4.02	2.95	.2371	10				.06	399.
2.000				. 1543	.58	2.91				
3.000			3.°.	.0435	.83	2.58	7.37	3.02		
5.000						2.55		2.98		
6.000 -5.80							7.52	3.04	.37	401.
7 000         -4,97         4,10         .0483         .36         2.99         6.30         3.28         .64         400.           8 .000         -4,11         4,47         .0297         .49         3.26         6.21         3.03         .63         400.           9,000         -3.18         4,96         .0535         .81         3.59         6.25         3.05         .57         400.           11,000         -1.50         6.37         .1414         1.08         3.99         6.46         3.52         .75         399.           12,000         -35         7.15         .2053         .88         5.91         8.22         4.90         .89         399.           13,000         .93         8.12         .2235         .15         6.70         9.30         5.01         .89         399.           14,000         .267         7.76         .2701         .16         5.48         8.61         4.81         .69         377.           15,000         .267         7.76         .2701         .16         5.48         8.61         4.81         .69         379.           15,000         .263         .417         .293         .271								3.19	.48	401.
8.000 -4.11 4.47 .0297 .49 3.26 6.21 3.03 .63 400. 9.000 -3.18 4.96 .0535 .81 3.58 6.23 3.05 .57 400. 10.000 -2.37 5.49 .1414 1.08 3.99 6.46 3.22 .75 399. 11.000 -1.50 6.37 .1635 1.38 5.02 7.39 3.89 .76 395. 11.000 -1.50 6.37 .1635 1.38 5.02 7.39 3.89 .76 395. 11.00035 7.15 .2053 .88 5.91 8.22 4.40 .89 389. 13.000 .93 8.12 .2235 .15 6.70 9.30 5.01 .96 387. 14.000 .2.21 8.45 .2731 .39 6.70 9.30 5.01 .96 387. 15.000 2.67 7.76 .2701 .16 5.48 8.61 4.81 .69 379. 16.000 .40 5.74 .1774 .30 3.72 6.09 3.14 .61 272. 17.000 -3.28 4.71 -0.259 -0.2 3.19 5.75 3.16 .79 263. 18.090 -7.94 4.95 .0697 -30 2.83 8.82 4.22 .47 261. 19.000 -9.69 4.01 .0209 .01 2.53 10.08 3.84 .04 256. 20.000 -11.18 4.34 -0.418 .57 2.35 11.50 4.18 13 248. 21.003 -13.43 6.19 .0538 .74 2.34 13.76 5.95 .12 240. 22.000 -18.31 9.58 1.147 .65 2.01 18.55 9.37 .04 224. 24.000 -20.26 11.27 .0782 .87 2.58 2.05 811.01 -0.07 224. 25.000 -22.18 12.28 .0592 .70 2.43 22.46 12.02 -2.20 214. 26.000 -27.64 10.24 10.77 .94 2.59 2.11 .0629 .9.1 18.55 9.37 .04 224. 27.000 -28.68 11.27 .0782 .87 2.92 2.90 10.59 2.13 2.78 11.20 -5.57 174. 28.000 -20.26 11.27 .0782 .87 2.90 2.18 23.73 12.45 -31 201. 27.000 -27.64 10.24 .1077 .94 2.79 2.18 23.73 12.45 -31 201. 27.000 -27.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -28.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -28.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.59 15.36 10.67 .19 3.52 29.81 6.65 .07 59. 38.000 -23.59 15.38 -1.440 3.40 6.71 3.55 4.11 9.55 59. 38.000 -23.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.69 9.45 .0448 .66 2.20 27.08 9.40 -27 136. 32.000 -23.69 9.45 .0448 .86 6.60 -0.65 4.99 .00 10.54 11.44 .65 56. 32.000 -23.69 9.45 .0448 .86 6.60 -0.65 4.99 .00 10.90 10.90 10.90 10.90 10.90 10.90 10.90 10.90 10.90 10.90								3.38	.56	401.
9.000 -3.18 4.96 .0535 .81 3.59 6.25 3.05 .57 402. 10.000 -2.37 5.49 .1414 1.08 3.99 6.46 3.22 .75 399. 11.000 -1.50 6.37 .1635 1.39 5.02 7.39 3.89 .76 395. 12.000 -355 7.15 .2053 .88 5.91 8.22 4.40 .89 389. 13.000 .93 8.12 .2235 .15 6.70 5.00 .93 5.01 .96 387. 14.000 .2.1 8.45 .270199 6.74 5.00 5.01 .96 387. 15.000 .2.67 7.76 .2701 .16 5.48 8.61 4.81 .69 379. 15.000 .40 5.74 .1774 .30 3.72 6.09 3.14 .61 272. 17.000 -3.28 4.71025902 3.19 5.75 3.16 .79 263. 18.090 -7.94 4.95 .069730 2.83 8.82 4.22 4.7 261. 19.000 -9.69 4.01 .0209 .01 2.53 10.08 3.84 .04 256. 20.000 -11.18 4.340418 .57 2.35 11.50 4.81 1.3 248. 21.000 -13.43 6.19 .0538 .74 2.34 13.76 5.95 .12 240. 22.000 -18.31 9.590376 .94 2.35 16.15 7.75 .20 239. 23.000 -80.51 11.27 .0782 .87 2.58 20.58 11.0107 224. 25.000 -22.65 11.27 .0782 .87 2.58 20.58 11.0107 224. 25.000 -25.60 10.71028 .47 2.77 2.78 11.01 .2961 174. 28.000 -26.63 11.42 .1221 .69 2.21 26.49 11.2961 174. 29.000 -26.68 12.51 .0628 .43 2.49 25.95 12.2057 174. 29.000 -27.64 10.24 .1077 .94 2.77 27.84 11.1056 142. 20.000 -27.04 10.25 11.26 .09 3.49 25.90 10.59 11.2961 174. 29.000 -27.00 -27.01 10.59053 3.73 5.60 3.99 0.50 10.71 3.55 9.95 12.20 2.14 2.20 2.14 2.20 2.20 2.20 2.20 2.20 2.20 2.20 2.2									-64	400.
10.000							6.21	3.03	.63	403.
11.000 -1.50 6.37 .1635 1.38 5.02 7.39 3.89 .76 395. 12.000 -35 7.15 .2053 .88 5.91 8.22 4.40 .89 389. 13.000 .93 8.12 .2235 .15 6.70 9.30 5.01 .96 387. 14.000 c.21 8.45 .275199 6.74 5.00 5.01 .96 387. 15.000 2.67 7.76 .2701 .16 5.48 8.61 4.81 .69 379. 15.000 .40 5.74 .1774 .30 3.72 6.09 3.14 .61 272. 17.000 -3.28 4.71025902 3.19 5.75 3.16 .79 263. 18.000 -7.94 4.95 .069730 2.83 8.82 4.22 47 261. 19.000 -9.69 4.01 .0209 .01 2.53 10.08 3.84 .04 256. 20.000 -11.18 4.340419 .57 2.35 11.50 4.18 .13 248. 21.003 -13.43 6.19 .0538 .74 2.34 13.76 5.95 .12 240. 22.000 :5.65 7.980376 .84 2.35 16.15 7.75 .20 239. 23.000 -18.31 9.58 1.427 .0782 .87 2.43 22.46 12.0220 244. 24.000 -20.26 11.27 .0782 .87 2.58 20.58 11.0107 224. 25.000 -22.18 12.28 .0592 .70 2.43 22.46 12.0220 214. 26.000 -26.53 11.42 .0582 .79 2.13 2.59 2.59 12.2057 174. 29.000 -26.63 11.42 .0792 .87 2.49 25.95 12.2057 174. 29.000 -26.63 11.34 .1024 .1077 .94 2.77 27.84 10.1056 142. 20.000 -25.60 10.710716 .00 3.49 25.90 10.54 17 58. 34.000 -25.60 10.710716 .00 3.49 25.90 10.54 17 58. 35.000 -25.60 10.710716 .00 3.49 25.90 10.54 17 58. 36.000 -27.20 7.81 .092606 3.56 27.08 9.4027 156. 37.000 -26.63 11.35 .0021 3.06 5.84 3.49 25.90 10.54 17 58. 37.000 -26.60 9.45 .0048 66 2.20 27.08 9.4027 156. 38.000 -27.20 7.81 .092606 3.55 27.43 7.80 11.955 142. 20.000 -27.69 10.24 .1077 .99 2.71 27.89 10.1056 142. 20.000 -27.69 10.54 .1077 .99 2.71 27.89 10.1056 174. 20.000 -27.69 10.54 .1077 .99 2.71 27.89 10.1056 192. 38.000 -30.48 10.59073015 4.41 30.84 10.45 .05 59. 38.000 -30.48 10.59073015 4.41 30.84 10.45 .05 59. 38.000 -30.58 11.02 .002209 4.92 21.00 11.4135 59. 38.000 -30.58 11.02 .002209 4.92 21.00 11.4135 59. 38.000 -30.58 11.02 .002299 4.92 21.00 11.41 .8343 59. 44.000 -34.50 15.88 .0639073015 4.41 30.84 10.45 .00 59. 38.000 -30.58 11.02 .002299 4.92 21.00 11.41 .89 59. 59.000 -8.65 18.33 .274 4.23 9.91 20.23 10.06 5.59 59. 59.000 -8.65 18.33 .2774 -23 11							6.23	3.05		400.
12,000									.75	399.
13.000									.75	395.
i+,000         c.21         8,45         .2701        59         6.7+         5.00         5.53         .55         385.           15,000         2.67         7.76         .2701         .16         5.48         8.61         4.81         .69         379.           16,000         .40         5.74         .1774         .30         3.72         6.09         3.14         .61         272.           17,000         -3.28         4.71         -0.0259         -0.02         3.19         5.75         3.16         .79         263.           18,000         -7.94         4.95         .0697         -30         2.83         8.02         4.22         .47         261.           19,000         -9.69         4.01         .0209         .01         2.53         10.08         3.84         .09         256.           20,000         -13,43         6.19         .0538         .74         2.35         11.50         4.18         .13         249.           22,000         15.85         7.98        0376         .84         2.35         16.15         7.75         .20         239.           23,000         -18.31         9.58         1.1427									.89	389.
15.000										397.
16.000										385.
17.000										379.
18.090										
19.000										
20.000       -11.18       4.34      0419       .57       2.35       11.50       4.18       .13       246         21.000       -13.43       6.19       .0538       .74       2.34       13.76       5.95       .12       240         22.000       -15.85       7.98      0376       .84       2.35       16.15       7.75       .20       239         23.000       -18.31       9.58       .1427       .85       2.01       18.55       9.37       .04       224         24.000       -20.26       11.27       .0762       .87       2.58       20.58       11.01      07       224         25.000       -22.18       12.28       .0592       .70       2.43       22.46       12.02      20       214         26.000       -23.51       12.68       .0762       .59       2.13       23.73       12.45      31       201         27.000       -25.68       12.51       .0628       .43       2.49       25.95       12.20      57       174         28.000       -26.63       11.42       .1077       .94       2.77       27.84       10.10      56       142										
21.003 -13.43 6.19 .0538 .74 2.34 13.76 5.95 .12 240. 22.000 :5.85 7.980376 .84 2.35 16.15 7.75 .20 239. 23.000 -18.31 9.58 .1427 .85 2.01 18.55 9.37 .04 224. 24.000 -20.65 11.27 .0782 .87 2.58 20.58 11.0107 224. 25.000 -22.18 12.28 .0592 .70 2.43 22.46 12.0220 214. 26.000 -23.51 12.68 .0762 .59 2.13 23.73 12.4531 201. 27.000 -26.68 12.51 .0628 .43 2.49 25.95 12.2057 174. 28.000 -26.33 11.42 .1221 .69 2.21 26.49 11.2961 174. 29.000 -27.64 10.24 .1077 .94 2.77 27.84 10.1056 142. 20.000 -26.96 9.45 .0448 .66 2.20 27.08 9.4027 156. 32.000 -25.60 10.710716 .00 3.49 25.90 10.54 .17 58. 34.000 -27.20 7.81 .092606 3.56 27.43 7.80 .12 59. 36.000 -25.57 8.99 .050119 3.52 29.81 8.6507 59. 38.000 -25.57 8.99 .050119 3.52 29.81 8.6507 59. 38.000 -30.58 11.20 .033202 4.92 21.00 11.9135 59. 40.000 -33.58 11.20 .033202 4.92 21.00 11.9135 59. 44.000 -34.59 15.381440 3.40 6.71 35.54 11.8343 59. 44.000 -37.28 16.671283 3.73 5.76 37.90 16.6803 58. 50.000 -28.47 17.051627 4.13 11.40 27.67 14.91 5.45 59. 55.000 -10.84 17.29 .1795 4.23 9.91 20.23 10.96 .57 52. 58.000 -28.57 20.18 .2257 3.57 14.08 22.10 12.46 .55 56. 56.000 -1.08 15.38 .067932 12.89 17.48 9.42 3.8 33. 64.000 -1.68 21.720100 -10.49 11.04 24.71 15.75 1.47 31.									.84	256.
22.000         15.85         7.98        0376         .94         2.35         16.15         7.75         .20         239.           23.000         -18.31         9.58         .1427         .95         2.01         18.55         9.37         .04         224.           24.000         -20.265         11.27         .0782         .87         2.58         20.58         11.01        07         224.           25.000         -22.18         12.28         .0592         .70         2.43         22.46         12.02        20         214.           26.000         -23.51         12.68         .0762         .59         2.13         23.73         12.45        31         201.           27.000         -25.68         12.51         .0628         .43         2.49         25.95         12.20        57         174.           29.000         -25.64         10.24         .1077         .94         2.77         27.84         10.10        56         142.           20.000         -26.96         9.45         .0448         .66         2.20         27.08         9.40        27         156.           32.000         -25.60         10.71					_				.13	248.
23.000 -18.31									.12	240.
24.000         -20.26         11.27         .0782         .87         2.58         20.58         11.01        07         224.           25.000         -22.18         12.28         .0592         .70         2.43         22.46         12.02        20         214.           26.000         -23.51         12.68         .0762         .59         2.18         23.73         12.45        31         201.           27.000         -25.68         12.51         .0628         .43         2.49         25.95         12.20        57         174.           28.000         -26.33         11.42         .1221         .69         2.21         26.49         11.29        61         174.           29.000         -27.64         10.24         .1077         .94         2.77         .27.84         10.10        56         142.           20.000         -26.96         9.45         .0448         .66         2.20         27.08         9.40        27         135.           32.000         -25.60         10.71        0716         .00         3.49         25.90         10.54         .17         58.           34.000         -27.20         7.81					.84					
25.000         -22.18         12.28         .0592         .70         2.43         22.46         12.02        20         214.           26.000         -23.51         12.68         .0762         .59         2.13         23.73         12.45        31         201.           27.000         -25.68         12.51         .0628         .43         2.49         25.95         11.20        57         174.           28.000         -26.63         11.42         .1221         .69         2.21         26.49         11.29        61         174.           29.000         -27.64         10.24         .1077         .94         2.77         27.84         10.10        56         142.           20.000         -26.96         9.45         .0448         .66         2.20         27.08         9.40        27         136.           32.000         -25.60         10.71        0716         .00         3.49         25.90         10.54         .17         58.           34.000         -27.20         7.81         .0926        06         3.52         29.81         8.65        07         59.           38.000         -30.48         10.59										
26.000       -23.51       12.68       .0762       .59       2.18       23.73       12.45      31       201.         27.000       -25.68       12.51       .0628       .43       2.49       25.95       12.20      57       174.         29.000       -26.33       11.42       .1221       .69       2.21       25.99       11.29      51       174.         29.000       -27.64       10.24       .1077       .94       2.77       27.84       10.10      56       142.         20.000       -26.96       9.45       .0448       .66       2.20       27.08       9.40      27       136.         32.000       -25.60       10.71      0716       .00       3.49       25.90       10.54       .17       58.         34.000       -27.20       7.81       .0926      06       3.56       27.43       7.80       .12       59.         36.000       -29.57       8.99       .0501      19       3.52       29.81       8.65      07       59.         40.000       -30.48       10.59      0730      15       4.41       30.84       10.45       .06       59.										
27.000         -25.68         12.51         .0628         .43         2.49         25.95         12.20        57         174.           28.000         -26.33         11.42         .1221         .69         2.21         26.49         11.29        61         174.           29.000         -27.64         10.24         .1077         .94         2.77         27.84         10.10        56         142.           20.000         -26.96         9.45         .0448         .66         2.20         27.08         9.40        27         136.           32.000         -25.60         10.71        0716         .00         3.49         25.90         10.54         .17         58.           34.000         -27.20         7.81         .0926        06         3.55         27.43         7.90         .12         59.           36.000         -25.57         8.99         .0501        19         3.52         29.81         8.65        07         59.           38.000         -30.48         10.59        0730        15         4.41         30.84         10.45         .06         59.           40.000         -23.79         12.26										
28.000       -26.33       11.42       .1221       .69       2.21       26.49       11.29      51       174.         29.000       -27.64       10.24       .1077       .94       2.77       27.84       10.10      56       142.         20.000       -26.96       9.45       .0448       .66       2.20       27.08       9.40      27       136.         32.000       -25.60       10.71      0716       .00       3.49       25.90       10.54       .17       58.         34.000       -27.20       7.81       .0926      06       3.56       27.43       7.80       .12       59.         36.000       -29.57       8.99       .0501      19       3.52       29.81       8.65      07       59.         38.000       -30.48       10.59      0730      15       4.41       30.84       10.45       .06       59.         4c.000       -30.58       11.20       .0232      09       4.92       21.00       11.81      35       59.         4c.000       -34.01       13.51      0021       3.06       5.84       34.42       11.83      20       59. <tr< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr<>										
29.000       -27.64       10.24       .1077       .94       2.77       27.84       10.10      56       142.         20.000       -26.96       9.45       .0448       .66       2.20       27.08       9.40      27       136.         32.000       -25.60       10.71      0716       .00       3.49       25.90       10.54       .17       58.         34.000       -27.20       7.81       .0926      06       3.56       27.43       7.80       .12       59.         36.000       -25.57       8.99       .0501      19       3.52       29.81       8.65      07       59.         40.000       -30.48       10.59      0730      15       4.41       30.84       10.45       .06       59.         40.000       -30.58       11.20       .0232      09       4.92       31.00       11.81      35       59.         42.000       -23.79       12.26       .0543       1.19       5.64       34.42       11.83      43       59.         44.000       -34.01       13.51      0021       3.06       5.94       34.96       12.89       .03       59.										
20.000       -26.96       9.45       .0448       .66       2.20       27.08       9.40      27       136.         32.000       -25.60       10.71      0716       .00       3.49       25.90       10.54       .17       58.         34.000       -27.20       7.81       .0926      06       3.56       27.43       7.80       .12       59.         36.000       -29.57       8.99       .0501      19       3.52       29.81       8.65      07       59.         38.000       -30.48       10.59      0730      15       4.41       30.84       10.45       .06       59.         40.000       -30.48       10.59      0730      15       4.41       30.84       10.45       .06       59.         40.000       -30.58       11.20       .0232      09       4.92       31.00       11.81      35       59.         42.000       -23.79       12.26       .0543       1.19       5.64       34.42       11.83      43       59.         44.000       -34.01       13.51      0021       3.06       5.84       34.86       12.89       .03       59.										
32.000       -25.60       10.71      0716       .00       3.49       25.90       10.54       .17       58.         34.000       -27.20       7.81       .0926      06       3.56       27.43       7.80       .12       59.         36.000       -25.57       8.99       .0501      19       3.52       29.81       8.65      07       59.         38.000       -30.48       10.59      0730      15       4.41       30.84       10.45       .06       59.         40.000       -30.58       11.60       .0543       1.19       5.64       34.42       11.83      43       59.         42.000       -23.79       12.26       .0543       1.19       5.64       34.42       11.83      43       59.         44.000       -34.01       13.51      0021       3.06       5.84       34.96       12.89       .03       59.         48.000       -37.28       16.67      1283       3.73       5.76       37.90       16.68      03       58.         50.000       -23.47       17.05      1627       4.13       11.40       27.67       14.81       .54       57.										
34.000       -27.20       7.81       .0926      06       3.56       27.43       7.80       .12       59.         36.000       -29.57       8.99       .0501      19       3.52       29.81       8.65      07       59.         38.000       -30.48       10.59      0730      15       4.41       30.84       10.45       .06       59.         40.000       -30.58       11.60       .0322      09       4.92       21.00       11.81      35       59.         42.000       -23.79       12.26       .0543       1.19       5.64       34.42       11.83      43       59.         44.000       -34.01       13.51      0021       3.06       5.84       34.86       12.89       .03       59.         46.000       -34.58       15.38      1440       3.40       6.71       35.54       15.00      20       59.         48.000       -37.28       16.67      1283       3.73       5.76       37.90       16.68      03       58.         50.000       -31.65       16.98      0654       3.91       7.99       33.19       16.33       .45       58.										
36.000         -25.57         8.99         .0501        19         3.52         29.81         8.65        07         59.           38.000         -30.48         10.59        0730        15         4.41         30.84         10.45         .06         59.           4C.000         -30.58         11.60         .0232        09         4.92         21.00         11.81        35         59.           42.000         -23.79         12.26         .0543         1.19         5.64         34.42         11.83        43         59.           44.000         -23.01         13.51        0021         3.06         5.84         34.86         12.89         .03         59.           46.000         -34.58         15.38        1440         3.40         6.71         35.54         15.00        20         59.           48.000         -37.28         16.67        1283         3.73         5.76         37.90         16.68        03         58.           50.000         -31.65         16.98        0654         3.91         7.99         33.19         16.33         .45         58.           52.000         -23.47         17.05 </td <td></td>										
38.000         -30.48         10.59        0730        15         4.41         30.84         10.45         .06         59.           40.000         -30.58         11.60         .0332        09         4.92         31.00         11.81        35         59.           42.000         -23.79         12.26         .0543         1.19         5.64         34.42         11.83        43         59.           44.000         -34.01         13.51        0021         3.06         5.84         34.96         12.89         .03         59.           46.000         -34.58         15.38        1440         3.40         6.71         35.54         15.00        20         59.           48.000         -37.28         16.67        1283         3.73         5.76         37.90         16.68        03         58.           50.000         -31.65         16.96        0654         3.91         7.99         33.19         16.33         .45         58.           52.000         -23.47         17.05        1627         4.13         11.40         27.67         14.81         .54         57.           54.000         -10.84         17.2										
4C.000       -30.58       11.00       .0032      09       4.02       21.00       11.81      35       59.         42.000       -23.79       12.26       .0543       1.19       5.64       34.42       11.03      43       59.         44.000       -24.01       13.51      0021       3.06       5.84       34.86       12.89       .03       59.         46.000       -34.58       15.38      1440       3.40       6.71       35.54       15.00      20       59.         48.000       -37.28       16.67      1283       3.73       5.76       37.90       16.68      03       58.         50.000       -31.65       16.96      0654       3.91       7.99       33.19       16.33       .45       58.         52.000       -23.47       17.05      1627       4.13       11.40       27.67       14.81       .54       57.         54.000       -16.59       15.24       .1209       5.44       8.25       21.71       11.44       .62       56.         56.000       -10.84       17.29       .1795       4.23       9.91       20.23       10.96       .57       52.										
42.000       -23.79       12.26       .0543       1.19       5.64       34.42       11.83      43       59.         44.000       -34.01       13.51      0021       3.06       5.84       34.86       12.89       .03       59.         46.000       -34.58       15.38      1440       3.40       6.71       35.54       15.00      20       59.         48.000       -37.28       16.67      1283       3.73       5.76       37.90       16.68      03       58.         50.000       -31.65       16.98      0654       3.91       7.99       33.19       16.33       .45       58.         52.000       -23.47       17.05      1627       4.13       11.40       27.67       14.81       .54       57.         54.000       -16.59       15.24       .1209       5.44       8.25       21.71       11.44       .62       56.         56.000       -10.84       17.29       .1795       4.23       9.91       20.23       10.86       .57       52.         58.000       -8.85       18.33       .2274       2.30       12.10       21.20       10.41       .68       45.										
44.000       -34.01       13.51      0021       3.06       5.84       34.86       12.89       .03       59.         46.000       -34.58       15.38      1440       3.40       6.71       35.54       15.00      20       59.         48.000       -37.28       16.67      1283       3.73       5.76       37.90       16.68      03       58.         50.000       -31.65       16.96      0654       3.91       7.99       33.19       16.33       .45       58.         52.000       -23.47       17.05      1627       4.13       11.40       27.67       14.81       .54       57.         54.000       -16.59       15.24       .1209       5.44       8.25       21.71       11.44       .62       56.         56.000       -10.84       17.29       .1795       4.23       9.91       20.23       10.86       .57       52.         58.000       -8.85       18.33       .2274       2.30       12.10       21.20       10.41       .68       45.         60.000       -6.37       20.18       .2257       3.57       14.08       22.10       12.62       .60       41.										
46.000         -34.58         15.38        1440         3.40         6.71         35.54         15.00        20         59.           48.000         -37.28         16.67        1283         3.73         5.76         37.90         16.68        03         58.           50.000         -31.65         16.96        0654         3.91         7.99         33.19         16.33         .45         58.           52.000         -23.47         17.05        1627         4.13         11.40         27.67         14.81         .54         57.           54.000         -16.59         15.24         .1209         5.44         8.25         21.71         11.44         .62         56.           56.000         -10.84         17.29         .1795         4.23         9.91         20.23         10.86         .57         52.           58.000         -8.85         18.33         .2274         2.30         12.10         21.20         10.41         .68         45.           60.000         -6.37         20.18         .2257         3.57         14.08         22.10         12.62         .60         41.           62.000         -1.08         15.38 <td></td>										
48.000       -37.28       16.67      1283       3.73       5.76       37.90       16.68      63       58.         50.000       -31.65       16.98      0654       3.91       7.99       33.19       16.33       .45       58.         52.000       -23.47       17.05      1627       4.13       11.40       27.67       14.81       .54       57.         54.000       -16.59       15.24       .1209       5.44       8.25       21.71       11.44       .62       56.         56.000       -10.84       17.29       .1795       4.23       9.91       20.23       10.86       .57       52.         58.000       -8.85       18.33       .2274       2.30       12.10       21.20       10.41       .68       45.         60.000       -6.37       20.18       .2257       3.57       14.08       22.10       12.62       .60       41.         62.000       -1.08       15.38       .0679      32       12.89       17.48       9.42       .38       33.         64.000       -1.61       14.43       .0537       -4.13       13.47       18.06       8.56       .51       32.      <										
50.000       -31.65       16.96      0654       3.91       7.99       33.19       16.33       .45       58.         52.000       -23.47       17.05      1627       4.13       11.40       27.67       14.81       .54       57.         54.000       -16.59       15.24       .1209       5.44       8.25       21.71       11.44       .62       56.         56.000       -10.84       17.29       .1795       4.23       9.91       20.23       10.86       .57       52.         58.000       -8.85       18.33       .2274       2.30       12.10       21.20       10.41       .68       45.         60.000       -6.37       20.18       .2257       3.57       14.08       22.10       12.62       .60       41.         62.000       -1.08       15.38       .0679      32       12.89       17.48       9.42       .38       33.         64.000       -1.61       14.43       .0537       -4.13       13.47       18.06       8.56       .51       32.         65.009       -4.50       15.62       .0957       -5.73       13.10       19.00       10.20       .44       32. <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>										
52.000         -23.47         17.05        1627         4.13         11.40         27.67         14.81         .54         57.           54.000         -16.59         15.24         .1209         5.44         8.25         21.71         11.44         .62         56.           56.000         -10.84         17.29         .1795         4.23         9.91         20.23         10.86         .57         52.           58.000         -8.85         18.33         .2274         2.30         12.10         21.20         10.41         .68         45.           60.000         -6.37         20.18         .2257         3.57         14.08         22.10         12.62         .60         41.           62.000         -1.08         15.38         .0679        32         12.89         17.48         9.42         .38         33.           64.000         -1.61         14.43         .0537         -4.13         13.47         18.06         8.56         .51         32.           65.009         -4.50         15.62         .0957         -5.73         13.10         19.00         10.20         .44         32.           68.000         -12.88         21.72										
54.000     -16.59     15.24     .1209     5.44     8.25     21.71     11.44     .62     56.       56.000     -10.84     17.29     .1795     4.23     9.91     20.23     10.86     .57     52.       58.000     -8.85     18.33     .2274     2.30     12.10     21.20     10.41     .68     45.       60.000     -6.37     20.18     .2257     3.57     14.08     22.10     12.62     .60     41.       62.000     -1.08     15.38     .0679    32     12.89     17.48     9.42     .38     33.       64.000     -1.61     14.43     .0537     -4.13     13.47     18.06     8.56     .51     32.       65.009     -4.50     15.62     .0957     -5.73     13.10     19.00     10.20     .44     32.       68.000     -12.88     21.72    0100     -10.49     11.04     24.71     15.75     1.47     31.										
56.000     -10.84     17.29     .1795     4.23     9.91     20.23     10.86     .57     52.       58.000     -8.85     18.33     .2274     2.30     12.10     21.20     10.41     .68     45.       60.000     -6.37     20.18     .2257     3.57     14.08     22.10     12.62     .60     41.       62.000     -1.08     15.38     .0679    32     12.89     17.48     9.42     .38     33.       64.000     -1.61     14.43     .0537     -4.13     13.47     18.05     8.56     .51     32.       65.009     -4.50     15.82     .0957     -5.73     13.10     19.00     10.20     .44     32.       68.000     -12.88     21.72    0100     -10.49     11.04     24.71     15.75     1.47     31.										
58.000     -8.85     18.33     .2274     2.30     12.10     21.20     10.41     .68     45.       60.000     -6.37     20.18     .2257     3.57     14.08     22.10     12.62     .60     41.       62.000     -1.09     15.38     .0679    32     12.89     17.48     9.42     .38     33.       64.000     -1.61     14.43     .0537     -4.13     13.47     18.05     8.56     .51     32.       65.009     -4.50     15.82     .0957     -5.73     13.10     19.00     10.20     .44     32.       68.000     -12.88     21.72    0100     -10.49     11.04     24.71     15.75     1.47     31.										
60.000     -6.37     20.18     .2257     3.57     14.08     22.10     12.62     .60     41.       62.000     -1.08     15.38     .0679    32     12.89     17.48     9.42     .38     33.       64.000     -1.61     14.43     .0537     -4.13     13.47     18.06     8.56     .51     32.       65.009     -4.50     15.62     .0957     -5.73     13.10     19.00     10.20     .44     32.       68.000     -12.88     21.72    0100     -10.49     11.04     24.71     15.75     1.47     31.										
62.000 -1.08 15.38 .067932 12.89 17.48 9.42 .38 33. 64.000 -1.61 14.43 .0537 -4.13 13.47 18.06 8.56 .51 32. 65.009 -4.50 15.62 .0957 -5.73 13.10 19.00 10.20 .44 32. 68.000 -12.88 21.720100 -10.49 11.04 24.71 15.75 1.47 31.										
64.000 -1.61 14.43 .0537 -4.13 13.47 18.06 8.56 .51 32. 65.009 -4.50 15.62 .0957 -5.73 13.10 19.00 10.20 .44 32. 68.000 -12.88 21.720100 -10.49 11.04 24.71 15.75 1.47 31.										
65.009 -4.50 15.62 .0957 -5.73 13.10 19.00 10.20 .44 32. 68.000 -12.88 21.720100 -10.49 11.04 24.71 15.75 1.47 31.										
68.000 -12.88 21.720100 -10.49 11.04 24.71 15.75 1.47 31.										
	70.000	-18.20	25.04	0023	-15.35	13.09	32.81	15.75	.47	31.

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Z	HEAN U	5.D. U	R(U.Y)	HEAN V	S.D. V	HEAN HS	S.D. KS	SKEH HS	NO95
101	H/5	H/S		H/S	M/S	M/5	MS		
.002	-3.15	3.04	.2058	.27	2.34	4.61	1.85	.33	425.
1.000	-5.17	4.12	.1392	.79	2.71	6.53	2.99	.07	421.
2.000	-5.73	3.88	.0345	.79	2.44	6.72	3.06	.26	421.
3.000	-6.29	3.65	.1275	.66	2.47	7.07	3.07	.19	421.
4.000	-6.78	3.62	-1100	.59	2.63	7.5:	3.19	.20	422.
5.000	-6.93	3.79	-0749	_44	3.04	7.79	3.33	.25	423.
6.000	-6.62	3.99	.1262	.36	2.99	7.57	3.40	.27	423.
7.000	-5.83	4.27	-0810	.43	2.89	6.99	3.43	.49	424.
8.000	-4.88	4.45	. 3627	.37	2.98	6.46	3.29	.43	424.
9.000	-e ŭi	r 61	00PS	.31	3.31	6.35	3.29	. 39	424.
10.000	-3.32	5.54	.0056	.34	3.72	6.58	3.50	.44	424.
11.000	-2 36	6.51	0204	.24	4.83	7.44	3.95	.65	425.
12.000	-1.39	7.19	.0554	21	5.41	7.94	4.45	.67	421.
13.000	36	7.85	-1385	79	6.11	8.67	4.94	-69	4:8.
14.000	.92	8.04	.1846	-1.13	6.49	8.97	5.31	.78	416.
15.000	1.20	7.41	.2143	78	6.05	8.35	4.87	1.01	410.
16.000	-1.32	5.76	. 1539	22	4.09	6.25	3.54	.99	278.
17.000	-5.59	4.12	-0331	- 18	3.02	6.87	3.18	-40	272.
18.000	-9.03	4.09	.0770	33	3.01	9.69	3.69	.10	270.
19.000	-10.05	4.41	.1632	19	5.58	10.46	4.02	21	258.
20.000	-11.54	5.28	.0675	.25	2.13	11.8i	5.12	.05	264.
2:.000	-13.71	7.45	.0722	.29	2.57	14.13	7.09	.12	258.
22.000	-16.12	9.58	-0993	.58	2.31	16.44	9.42	.18	254.
23.000	-18.37	11.25	.1059	.66	2.03	18.63	11.02	-10	245.
24.000	-20.18	12.82	0126	.53	2.45	20.53	12.51	-99	244.
25.000	-21.86	13.05	- 0857	.58	2.58	22.15	12.83	14	242.
26.000	-55.60	12.76	.0506	.63	2.12	23.02	12.56	23	225.
27.000	-23.52	12.48	.1588	1.22	2.57	23.90	12.05	28	195.
28.000	-23.67	12.09	.0326	1.19	2.31	23.88	11.95	12	193.
29.000	-24.40	12.02	0449	.95	3.09	24.79	11.64	24	152.
30.000 32.009	-24.21	11.05	1125	.71	2.60	24.41	10.95	03	148.
	-27.23	9.91	.0210	-07	3.20	27.45	ყ.ც2	- 11	85.
34.000 35.000	-29.73 -32.97	19.44 11.14	0060	93	3.36	29.95	10.36	38	88.
38.000	-34.50		0693	84	3.54	33.19	11.05	19	89.
40.000	-35.80	14.04	1984	. 14	4.58	34.88	13.84	.14	88.
42.000	-34.10	16.50 15.91	3307	æ	5.15	35.25	16.32	•33	88.
44.000	-31.36	15.9:	2152	1.35	5.13	34.59	15.72	-54	89.
46.000	-28.28	17.27	1116 1089	.80 2.90	6.00	32.22	16.33	-46	89.
48.000	-21.45	17.77	1118	2.90 3.09	5.82	29.88	16.11	.72	68.
50.000	-15.44	16.92	2171	3.45	6.47	23.76	16.19	1.07	88.
52.000	-10.07	15.71	0579	3.43 4.36	6.51	19.59	13.91	1.34	88.
54.000	-7.65	17.49	0575	3.24	7.24	16.98	11.37	1.26	89.
56.000	-5.53	13.83	0917	2.77	8.09 9.65	16.95	12.26	2.48	86.
58.000	-2.06	14.79	.0231	.18	9.63 8.62	15.55 15.31	8.85 7. <i>7</i> 4	.65	83.
60.000	-1.50	15.77	1431	-2.19	11.42	17.59	7.74 8.48	.71 .64	77.
62.000	3.49	16.70	1059	-3.82	11.05	18.64	8.50	-64	66. 53.
64.000	7.88	15.67	.0752	-5.30	9.98	18.00	10.34	.75	53.
66.000	13.6!	13.57	.0673	-6.52	11.61	20.42	9.96	.63	53. 52.
63.000	10.92	14.89	.0082	-4.94	14.72	21.20	11.26	.03 41	51.
70.000	5.81	14.52	.1195	-8.84	14.87	21.10	9.57	13	49,
				J.0.		20	٠. ٠.		73,

	1. 9 - 913660	HIND STAT	TISTICAL PA LEIN MISSLE	NRAMETERS. E RANGE		SEP	TEMBER		
Z	MEAN U	5.D. U	R(U,V)	HEAN V	S.D. V	MEAN HS	S.D. WS	SKEH HS	
101	H/S	M/S		H/S	M/S	H/S	H/S	SKEW MS	NOBS
.002	-2.34	3.C8	.2541	.39	5,88	4.41	1.97	.49	
1.200	-3.98	4_44	.2925	.95	3.54	6.35	2.93		425.
2.000	-4.46	4.23	.2554	-80	3.31	6.43	2.84	-42	426.
3.000	-5.26	3.99	.2853	-66	3.26	6.80	2.87	.40	426.
4.000	-5.85	3.85	.3007	.64	3.39	7.21	2.97	.25	425.
5.000	-5.87	3.99	.2928	.44	3.46	7.26	3.14	. 34	425.
6.000	-5.56	4.20	.2134	.33	3.25	6.92	3.14	.32	424.
7.000	-5.18	4.21	.2276	.32	3.25	6.57		.57	423.
8.000	-4.51	4.25	.2561	.26	3.51	6.42	3.33	.47	424.
9.000	-3.92	4.77	.1658	.15	3.71		3.09	-55	424.
10.000	-3.31	5.56	.1819	07	4.01	6.41	3.27	.71	.,24.
11.000	-2.67	6.66	.2377	40	5.05	6.56	3.69	1.05	425.
12.000	-1.92	7.51	.2512	-1.14	6.05	7.63	4.34	1.16	424.
13.000	-1.22	8.57	.2555	-1.99	7.11	8.60	4.90	1.05	424.
14.000	49	9.09	.2410	-2.48	7.58	9.91	5.56	.99	423.
15.000	63	8.29	.3540	-1.65	6.38	10.53	5.54	.95	420.
16.000	-3.20	6.87	-3416	-1.12	4.45	9.18 7.70	5.28	1.00	416.
17.000	-6.64	4.85	.1409	70	3.21	7.70	4.32	.81	267.
18.600	-7.87	4.51	.0959	91	2.71	8.60	3.93	.52	258.
19.000	-9.09	4.57	.0547	~. 13	2.58	9.60	4.04	.35	253.
20.000	-10.39	6.12	0037	.rs	2.24	13.88	4.25	.05	246.
21.000	-12.45	8.66	0392	.38	2.53		5.65	.19	244.
22.000	-14-63	10.13	0868	.24	2.04	13.10	6.07	. 15	235.
23.000	-16.80	11.47	.0294	.24	1 87	14.94 17.07	9.88	- 16	234.
24.000	-18.94	12.95	.1195	.31	2.47	19.49	11.22	.09	228.
<b>ප</b> 5.009	-20.54	13.24	.0453	.52	2.61	21.11	12.36 12.60	.00	228.
26.000	-21.20	12.69	.0455	.84	2.38	21.61		11	224.
27.000	-21.37	12.47	.0330	.93	3.08	21.90	12.25 11.95	18	213.
28.000	-20.35	11.99	.1107	.94	2.39	20.63	11.79	10 .14	199.
29.000	-20.86	12.14	.0785	.79	2.98	21.48	11.42	.95	192.
39.000	-20.27	11.22	.0925	.27	2.29	20.58	10.87	. 95 . 24	147.
32.000	-21.66	11.67	.0427	83	2.84	22.00	11.39		147.
34.000	-22.74	13.91	1770	-1.13	5.91	23.54	12.87	.00	87.
35.000	-24.40	15.40	2515	.52	3.69	25.52	13.96	27 21	97.
38.000	-23.90	17.57	1996	.64	4.37	25.93	15.04	es	87.
40.600	-20.53	18.50	0502	.:8	بر وذ.ب	23.46	15.78	.58 .50	87.
42.000	-15.16	17.61	.0558	1.45	5.38	19.53	13.71	. 30 .:37	<b>37.</b>
44.000	-7.73	14.71	0572	2.19	6.70	15.00	9.95	136	87. 87.
46.000	-1.96	11.68	0587	-48	5.57	10.65	7.35	2.08	96.
48.000	2.28	11.32	<b>2059</b>	1.64	6.01	10.70	7.51	1.58	86.
50.000	2.39	10.64	2576	2.73	6.87	11.50	6.28	.91	86.
52.000	3.9:	11.32	2784	4.36	7.66	12.95	7.20	.82	86.
54.000	5.10	14.05	3053	4.82	8.28	15.55	8.43	.91	85.
56.000	8.C2	15.24	3523	2.67	9.48	17.37	9.44	.71	84.
59.000	10.27	16.00	3455	.04	10.70	19.50	9.59	.49	76.
60.000	8.32	15.05	2742	-2.56	10.86	18.61	8.36	.45	61.
62.000	11.19	13.34	~.1856	-2.70	9.65	18.09	8.49	.15	45.
54.000	12.52	14.24	.0449	-4.12	10.73	19.70	9.91	.59	41
66.000	11.22	13.21	.2805	97	10.83	17.95	9.57	.57	i
59.000	6.64	10.42	.2479	-06	12.54	16.05	6.87	. 33	42.
70.000	3.71	12.55	0097	2.54	12.62	16.24	8.21	. 79	42.

THE PARTY OF THE P

TABLE I. 10 HIND STATISTICAL PARAMETERS. STATION = 913860 KHAJALEIN MISSLE RANGE				OCTOBER					
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	5.D. 45	SKEH WS	41000
KM	M/S	M/S		M/S	M/S	M/S	M/S	SVEM M2	NOBS
.002	-2.58	3.79	.2757	. 35	2.94	5.00	2.18	1.47	443.
1.000	-3.88	5.77	:ess.	.82	3.50	6.94	3.60	.74	447.
2.000	-4.32	5.56	.1405	.60	3.37	7.00	3.49	.57	447.
3.000	-4.54	5.26	.1715	. 44	3.36	6.93	3.42	.65	449.
4.000	-4.64	5.23	.1973	.28	3.37	6.92	3.52	.47	449.
5.000	-4.34	5.11	.1883	. 19	3.86	6.85	3.56	.53	449.
6.900	-4.05	4.83	.1701	.10	3.93	6.56	3.49	.72	448.
7.000	-3.39	4.65	.1741	11	3.93	6.12	3.34	.93	447.
8.000	-2.50	4.84	.1962	11	4.20	5.97	3.40	.89	447.
9.000	B1	5.33	.2039	13	4,44	6.23	3.53	.82	447.
10.000	-1.22	G. 12	.1865	18	4,83	6.00	3.79	.64	446.
11.000	39	7.43	.1624	43	5.62	8.27	4.30	.71	446.
12.000	.60	8.46	.1653	84	6.56	9.45	5.12	.62	441.
13.000	1.67	9.62	.1777	-1.28	7.72	10.97	6.00	.69	438.
14.000	2.19	10.03	.2585	-1.36	7.80	11.29	6.35	.69	435.
15.000	1.80	10.24	.2635	-1.25	6.76	13.76	6.28	.55	434.
16.000	33	9.15	.2502	~1.88	4.59	9.03	5.16	.72	272.
17.000	-3.83	6.82	.1874	-1.98	3.19	7.48	4.38	.74	267.
18.000	-5.59	5.54	.05'+3	-1.39	3.11	7.50	4.15	.80	268.
19.000	-5.74	5.55	0146	66	2.51	7.33	4.07	.37	267.
0.000ء	-6.85	7.93	.0543	. 19	2.25	8.93	5.78	.26	262.
21.000	-9.11	10.42	0594	.24	2.44	11.61	7.90	.20	251.
22.000	-12.04	12.08	1008	.03	2.32	13.97	10.03	.15	251.
23.000	-14.53	13.00	0974	.04	1.98	15.84	11.53	27	245.
24.000	-16.74	14.07	0011	. 13	2.87	18.32	12.27	.01	244.
25.000	-17.56	13.50	0155	.54	2.94	18.86	12.00	03	242.
26.000	-16.76	12.20	.1062	.60	2.49	17.64	11.18	.10	234.
27.000	-15.5)	12.18	.1335	.54	2.94	16.66	11.14	.38	214.
28.000	-14.18	11.75	.0286	.59	2.55	14.96	11.01	.79	214.
29.000	-12.96	12.44	.0394	.70	3.10	14.77	10.69	1.00	176.
30.000	-12.17	12.34	0'+07	.49	2.52	13.95	10.59	.99	172.
32.000	-13.19	13.70	1250	62	3.20	16.24	10.30	.05	bb.
34.000	-12.35	14.33	.0192	81	3.41	16.00	10.62	.24	65.
36.000	-10.!5	14.94	.0769	14	3.91	15.25	10.34	.43	65.
38.000	-6.0	15.08	0856	1.17	4.73	13.88	9.62	.99	65.
40.000	52	13.30	1858	.16	4.61	11.29	8.29	1.52	65.
42.000	5.57	12.85	.0556	~1.38	4.66	12.46	7.91	.83	65,
44.000	10.18	13.46	.2516	95	5.71	15.91	7.5	.58	65.
46.000	16.45	11.64	.1588	2.62	5.51	18.42	10.16	39	65.
48.000	20.12	11.74	1131	5.42	5.21	21.89	10.91	.40	35.
50.000	24.52	13.69	3225	5.32	7.51	26.86	12.25	.58	65.
52.000	28.92	16.46	2529	3.66	5 53	30.00	15.97	.33	66.
54.000	32.90	17.38	−.078≎	1.15	6.66	33.89	15.74	08	66.
56.000	35.15	16.75	.0053	72	8.05	36.31	16.19	.08	65.
58.000	34.01	21.42	.0215	-1.22	8.13	37.32	16.92	14	60.
60.000	32.87	20.11	.2480	-3.76	8.90	36.15	16.34	29	52.
62.000	30.06	22.02	.1521	-2.55	9.68	34.26	17.56	26	42,
64.000	33.29	19.88	0016	95	10.24	35.22	19.10	08	36.
66.000	36.98	16.95	1547	-3.03	10.65	38.88	16.17	.16	34.
68.000 70.000	34.76	14.29	2285	-1.93	11.10	36.85	13.31	16	33.
70.000	19.98	16.61	.1956	-1.50	11.80	25.58	12.40	.98	31.

TABLE STATION	1. 11 = 913660	11 WIND STATISTICAL PARAMETERS. 3560 KHAJALEIN MISSLE RANGE				NOVEMBER				
Z	MEAN U	5.D. U	R(U.V)	MEAN V	S.D. V	45 AM 155				
KM	M/S	M/S		M/S	M/S	.1EAN WS M/S	S.D. WS	SKEW WS	NOBS	
.002	-4.55	2.52	.4217	99	2.82	5.65	M/S			
1.000	-6.63	3.86	.3662	34	3.40	7.76	2.01 3.21	.42	415.	
2.000	-6.06	3.80	.2143	.13	3.14	7.13	3.18	.18	416.	
3.000	-5.60	4.09	.1459	.07	3.28	6.96	3.21	.42	417.	
4.000	-5.43	4.42	.2659	01	3.39	6.94	3.51	.47	417.	
5.000	-5.68	5.27	.2441	- 53	3.64	7.49	4.15	.56	416	
6.000	-5.62	6.06	.2976	56	4.01	7.87	4.77	.55	416.	
7.000	-4.52	6.51	.3382	-1.02	4.27	7.69	4.78	.62	434.	
8.000	-3.04	6.84	.3452	51	4.40	7.54	4.38	.92	415.	
9.000	-1.19	7.30	.3005	48	4.49	7.47	4.39	.39	415.	
10.000	.66	7.95	.2522	.05	4.98	8.03	4.88	1.09	416.	
11.000	2.36	8.68	.2097	.70	5.50	9.08		1.05	415.	
12.000	3.36	9.03	.2240	.98	5.81	9.77	5.39 5.63	.92	4!6.	
13.000	3.80	9.65	.5080	.70	6.43	10.64	6.01	.70	413.	
14.000	3.26	9.98	.1933	40	6.6c	10.84		.80	412.	
15.000	1.31	9.53	.2482	-1.69	5.87	9.82	6.04	. 79	409.	
16.000	-2.11	8.38	-2688	-2.75	4.48	8.89	5.76	.81	403.	
17.000	-5.36	6.79	.1032	-2.52	3.58		4.81	1.06	271.	
18.000	-6.38	5.98	.0932	-1.66	3.06	8.52	4.61	.48	265.	
19.000	-4.42	6.57	.0940	47	2,44	8.12	4.74	.65	265.	
20.000	-5.11	9.13	.0795	.19		7.07	4.33	.54	259.	
21.000	-7.23	11.81	.0260	.34	2.25	9.06	5.68	.31	255.	
22.000	-10.00	12.95	.0371	.40	2.53 2.57	11.84	7.60	.13	252.	
23.000	-12.51	13.11	0855	.23	2.31	13.99	9.02	.10 .	251.	
24.000	4.43	13.54	1329	.16		15.17	10.15	.06	243.	
25.000	3.86	11.90	0534	.45	3.26	17.00	10.62	.02	238.	
26.000	~11.58	10.73	.0857	.71	3.12 2.65	15.93	9.1:5	.11	233.	
27.000	-8.73	11.21	.0560	. 95	5.85	13.38	9.80	.53	226.	
28.000	-6.55	12.36	0283	.70	2.48	11.63	8.65	1.02	206.	
29.000	-5.50	14.76	1225	.48	2.97	11.11	8.86	1.28	203.	
30.000	-4.62	15.64	0739	.17	2.79	13.35	8.83	.80	160.	
32.000	-2.49	18.30	0357	.17	3.21	:4.87	7.16	.26	155.	
34.000	2.48	17.80	.3332	.71	4.00	15.50	10.33	. 39	53.	
36.000	9.47	19.21	0361	.43	5.72	16.39	8.12	.50	52.	
38.000	14.55	20.30	3969	-1.37	5.85	19.21 22.98	10.81	16	52.	
40.000	20.05	16.49	2663	73	6.14	23.40	11.27	13	52.	
42.000	24.98	13.45	2434	1.02	5.33		:2.7!	29	ė5.	
44.000	27.33	12.90	2890	1.48	5.33 6.45	26.44 28.87	11.56	05	52.	
46.000	29.92	14.62	0138	1.87	6.76	31.21	11.07	55	52.	
48.000	30.93	15.66	.0594	1.92	7.17	32.33	13.53 14.50	56	52.	
50.000	32.54	16.80	.1679	.4,	7.63	33.57		~.58	52.	
52.000	31.10	20.89	0970	1.26	7.10	34.37	16.46	38	51.	
54.000	30.66	20.92	0212	1.05	7.91	34.22	16.42 16.29	18	51.	
56.000	31.72	18.53	.1017	11	8.16	33.91		.08	49.	
58.000	32.06	20.70	.2172	-1.07	8.96	35.60	16.22 16.26	26	46.	
60.300	28.17	24.56	.0398	.81	10.40	35.35	15.67	02 02	44,	
62.000	26.97	27.63	.2491	.25	10.87	36.90	15.20	ee	44.	
64.000	28.90	29.35	.5522	-1.41	12.90	40.39	14.34	18	39. 36.	
66.000	29.15	24.09	.3533	-3.21	11.75	36.11	15.17	18		
58.000	22.98	21.47	.1338	-5.35	13.47	31.11	14.63	.33	35. 35.	
70.000	6.04	20.91	1701	-4.03	15.56	23.50	12.84	.05	37. 34.	
						-5.50	12.04	.05	37.	

	I. 12 = 913660		ISTICAL PA			DE			
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEH WS	NOBS
KM	M/S	M/5		M/S	M/S	M/S	M/S		11000
.002	-6.83	2.06	.1079	-2.91	2.33	7.82	1.92	06	429.
1.000	-10.07	3.58	.1491	-P.40	3.07	10.89	3.30	27	433.
2.000	-8.12	4.02	.0193	98	2.9!	8.88	3.54	.04	434.
3.000	-7.25	4.51	.0260	34	2.83	8.20	3.72	.20	434.
4.000	-7.99	4.92	.0593	76	3.10	9.00	4.15	.25	434.
5.000	-9.12	5.73	.0919	-1.43	3.84	10.38	4.99	.35	433.
6.000	-9.65	6.36	.1741	-2.00	4.51	11.33	5.43	.35	433.
7.000	-9.07	5.84	.2334	-2.32	<b>५.8</b> 5	11.27	5.68	.35	433.
8.000	-6.98	7.18	.2897	-2.54	5.08	10.03	5.64	.48	43!.
9.000	-4.41	7.40	.3080	-1.72	3.32	3.55	5.2!	·ōė	430
10.000	-2.13	7.52	.2918	59	5.67	8.27	5.01	1.26	428.
11.000	38	7.89	.2177	.50	6.12	8.69	4.92	1.13	428.
12.000	.24	7.90	.1959	1.03	6.13	8.89	4.68	.69	427.
13.000	.31	8.10	. 1534	.85	6.31	9.13	4.76	.61	425.
14.000	20	7.94	.0821	52	6.36	8.92	4.90	-66	425.
15.000	-1.99	7.44	.0399	-2.24	5.75	8.53	4.86	.80	421.
16.000	-4.61	6.11	.0248	-2.79	4,45	8.14	4.46	.74	277.
17.000	-8.06	5.53	0731	-5.68	3.98	9.77	4.78	.46	275.
18.000	-9.23	6.08	0118	-1.49	3.78	10.49	5.34	.68	271.
19.000	-5.19	7.94	.0177	62	2.68	7.98	4.93	.87	265.
20.000	-3.36	10.48	0639	.17	2.33	9.87	5.38	.29	260.
21.000	-5.90	12.61	1413	.66	2.66	12.19	7.23	.17	250.
25.000	-8.49	13.34	0750	- 39	2.84	13.48	ទ.72	.20	249.
53.000	-10.42	12.33	0327	.22	2.25	13.91	8.47	.23	245.
24.000	-11.92	i1.90	0526	07	2.93	14.84	8.47	- 13	241.
25.000	-9.45	9.79	0034	.43	3.28	11.78	7.55	.51	239.
26.000	-6.29	9.91	.1711	.96	2.45	9.13	7.81	1.03	222.
27.000	-3.21	13.02	. 1787	1.05	2.85	11.42	7.67	.91	204.
28.000	-2.06	16.47	.2204	.91	2.93	14.67	7.93	.47	204.
29.000	50	18.76	.2547	.86	3.33	17.74	6.91	.07	178.
30,000	1.10	20.54	.2441	.74	3,19	19.59	6.91	. 15	173.
32.000 34.000	6.51	21.61	.0845	-46	4.83	20.59	10.18	.60	70.
36.00C	7.70	23.02	0169	03	6.31	22.41	10.96	.24	70.
38.000	7.64	19.60	.1580	.96	7.58	19.23	11.25	.45	70.
40.000	8.66 11.26	17.65 17.07	.3985	04	7.87	17.69	11.50	.53	70.
42.000	12.58	16.80	.3503	41	7.65	18.04	12.17	.65	70.
44.000	11.16	18.48	.2685	2.25	8.18	19.13	11.99	.25	70.
45.000	8.33	18.25	.3822 .3560	3.23	9.17	20.77	11.18	.61	70.
48.000	7.22	18.18	.0939	3.87 1. <del>3</del> 7	9.66	19.99	10.52	.24	70.
50.000	7.30	22.26	1727	1.69	9.34 9.64	19.13	10.16	.79	70.
52.900	9.91	21.93	2766	.34		21.62	13.09	1.15	70.
54.000	11.08	24.22	31!5	.92	10.31 12.56	22.16	13.74	1.03	70.
56.000	12.07	23.50	2036	3.20	9.66	24.53 24.44	16.09	1.47	68.
58.000	15.13	24.23	0119	2.58	9.46	26.47	14.05 14.30	.41 .18	66. SS
60.000	17.83	25.59	0955	.08	11.04	29.26	15.13	.18	66. 58.
62.000	21.65	25.60	.0251	-4.61	10.50	31.09	16.94	.57	58. 45.
64.000	21.20	21.31	.0393	-2.61	10.59	26.85	10.57	.77	40.
66.000	21.39	21.44	.3249	-4.54	12.97	27.36	17.92	.66	36.
58.000	21.15	27.54	.0108	-1.99	13.93	31.92	19.21	.69	36.
70.000	14.20	29.73	2361	3.37	17.40	33.56	15.75	.52	36.
						00			501

	1. 13 - 913660	HIND STAT	TISTICAL PA EIN MISSLE	ARAMETERS.	ANNUAL				
Z	MEAN U	S.D. U	R(U,V)	MEAN V	S.D. V	MEAN WS	S.D. WS	SKEW WS	44000
КM	M/S	M/S		M/S	M/S	M/S	M/S	SVEM M2	NOBS
.002	-5.15	3.15	.4388	-1.39	2.82	6.36	2.43	.08	501.0
1.000	-7.42	4.58	.3731	68	3.23	8.59	3.63	.12	5049.
2.000	-6.37	4.27	.1536	. 13	2.90	7.48	3.35	.39	5078.
3.000	-5.72	4.31	.1175	.27	2.86	6.98	3.30	.39	5079.
4.000	-5.63	4.62	.1637	. 17	3.02	7.04	3.56	.56	5078.
5.000	-5.64	5.25	.1916	07	3.38	7.36	4.09		5077.
6.000	-5.42	5.89	.2367	30	3.79	7.62	4.51	.72 .87	5075.
7.000	-4.67	6.27	.2536	51	4.05	7.54	4.59	1.01	5065.
8.000	-3.32	6.51	.2258	66	4.28	7.34	4.28	.95	5057. 5059.
ā.00n	-1.77	ร. 78	.2037	38	4.42	7.26	4.13	.99	5059. 5055.
10.000	41	7.23	.2034	. 13	4.80	7.52	4.35	1.04	
11.000	.80	7.94	.1726	.72	5.63	8.52	4.84	1.01	5047.
12.000	1.72	8.48	.1582	. 74	6.14	9.28	5.40	.84	5040.
13.000	2.41	9.19	.1347	. 38	6.78	10.19	5.69	.81	5012.
14.000	2.61	9.46	.1161	43	6.83	10.45	5.90	.77	4991. 4973.
15.000	1.84	9.28	.1113	-1.05	6.19	9.88	5.60	.74	4973. 4918.
15.000	69	8.29	.1103	-1.45	4.70	8.42	4.76	.65	3278.
17.000	-3.86	7.12	.0347	-1.40	3.80	7.83	4.45	.79	3208.
18.000	-5.82	6.52	0080	92	3.27	8.15	4.64	.73	3208.
:9.000	-4.91	7.21	9067	32	2.47	7.94	4.39	.52	3151.
20.000	-5.70	9.16	0437	. 15	2.27	9.74	5.19	.31	3100.
21.000	-7.77	10.85	0441	.44	2.51	11.73	6.95	.33	2994.
22.000	-9.90	11.59	0356	.43	2.53	12.94	8.47	.44	2984.
23.000	-11.54	11.82	0346	. 36	2.10	13.77	9.37	.55	2869.
24.000	-12.89	13.20	0259	.35	2.89	15.44	10.52	.48	2656.
25.000	-13.42	13.88	0234	.56	2.77	16.07	11.08	.43	2814.
26.000	-13.30	14.65	.0596	.68	2.35	16.37	11.40	.40	2671.
27.000	-13.26	15.85	.0886	.78	2.70	17.47	11.41	.36	2411.
28.000	-13.22	16.52	.0885	.77	2.53	18.21	11.12	.34	2390.
29.000	-13.60	17.36	.0729	.78	2.99	19.54	10.69	.23	2006.
30.000	-13.64	17.39	.0733	.62	2.60	19.81	10.18	.15	1968.
32.000	-13.72	18.57	.0133	.18	3.59	ċû.7ù	10.00		334.
34.000	-15.28	18.70	.0677	36	3.89	21.85	11.03	.01	832.
36.000	-16.34	19.00	.0290	30	4.49	22.68	11.62	.13	833.
38.000	-15.55	19.68	0408	. 17	5.31	22.39	12.54	.49	833.
40.000	-12.99	20.55	0366	.66	5.41	20.91	13.60	.89	832.
42.000	-10.14	21.53	.0114	1.35	5.90	20.51	13.54	.87	833.
44.000	-7.67	22.23	.0247	1.62	6.96	20.81	13.13	.91	833.
46.000	-6.13	23.65	0247	2.50	7.08	21.29	14.18	.77	832.
48.000	-4.11	25.14	0429	3.2!	7.32	22.19	14.90	.82	829.
50.000	-1.03	25.47	0497	3.73	8.38	22.87	14.56	.87	827.
52.000	3.87	25.18	0422	3.94	9.19	23.21	14.53	.82	826.
54.000	8.29	24.82	1030	3.37	9.29	23.65	14.99	.92	807.
56.000	1:.29	24.51	0845	2.21	9.91	24.75	14.86	.74	769.
58.000	13.75	24.27	0:18	01	9.93	25.60	14.98	.71	697.
60.000	14.87	25.35	0.746	-1.02	10.95	27.20	15.74	.61	600.
62.000	16.54	24.71	.0582	-1.99	11.95	27.96	15.89	.69	490.
64.000	17.82	24.14	.2012	-2.89	11.92	28.10	16.27	.64	446.
65.000	17.90	23.81	. 1558	-3.98	12.64	28.39	16.15	.65	423.
68.000	13.56	25.46	-1609	-4.34	14.14	28.58	15.41	.67	412.
70.000	6.25	26.29	.1359	-4.79	15.37	28.18	15.17	.65	400.

	COBON	1	413.	150 t	, c	0.00	מיני	47.8°	425.	423.	¥06.	397.	380.	n :	5/4.	36.	353.	278.	274.	274.	270.	267.	253.	253	, o	, n	מגל		20.	187.	186.	68.	68.	5 8	60	69	.69		6.7	. 22	63.	63.	59.	51.	33	1 %		; ø
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	a vaca		413.	429.			י ממ ממ	, 65 65	425.	423.	406.	397.	380.		5/E.	364.	353,	278.	274.	27.4.	270.	267.	ກີ	523	ร์ ซึ่ง เ		, a	- -		187.	186.	70.	69	3 6	. 69	63	69	99.	9.5			63,	59.	51.	38.	g <u>:</u>		ij
	מאנות		.80	ž,	9.5	9		32	57	-, 56	÷9	-1.10	-1.12	79.1:	, u	+ d	04	36	<b>₹.</b> -	09	.05	±.	6	S	ก็เ	1 1	) n	מי	2 -	0.07	- 10	.65	03	77 27	2	. 39	ж. Ж.	.39		00.	. r.	86	30	67.	± .	g. :	# C	. 19
	כ כ	0/43	4.7440	4.7960	4.1210	0.000	3.3050 7.8050	3.6120	3.2110	2.9330	2.5790	2.5830	2.3030	1.91.50	01010	1.1180	1.3590	1.5410	2.1350	2.9090	1.9130	1.3099	.9487	.7519	.5516	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	ה מל ה	07-1-	21.15	7,82	. 2356	1931	.1672	os : 1 .	0460	.0629	.0486	.0453	3520.	ROUD.	. 166	.0171	.0130	90100	9870.	.0053	.0053	1 *00.
JANUARY	MC AN D	6/H3	1155.0000	155.0000	065.0000	2007.000	785 0000	709.8000	639.8000	975.6000	517.4000	464.7000	417.5000	374.5000	334.5000	263,9000	232,0000	202.1000	173.0000	143.5000	116.4000	95.8300	79.8200	66.9300	56.4100	14.7.55000 14.7.55000	40.4600	34.5700	24.04.00	21.3700	18.2+00	13.3300	9.8120	•	5.3/60	3.0390	2.3030	1.7540	1.35.78	00.0	1818.	5083	3965	3107	है। हो	. 1880	0941.	.0876
JAC	ב הונה		-1.35	-1.29			ָרָ מַלְי	; ±	6.	33	. BC	77	 66	3B	7 2				.36	51.	÷	07	٠,00	05	# ! # !	ž.	- 5	2 6	ra:		.03	61.	.28		B)	, m	12	29.	Ę.	2 9	§ .	5 -		- 08	62.	£5.	გე: -	01.
PARAMETERS.	F	- X	1.03	-:-	os		7.5	2 2	- S	1.5.1	1.87	.36	1.39	R 1	 	7.7	2	3.	1.80	3.35	2.78	2.30	P.08	P.07	98. 	8 t	, i.	บู้ บัก	יי מיני מיני	ດ ດີດ ດີ	2. 5 5. 55	3.55	3.58	3.69	÷ 6	6 G	3.90	4,75	6.06	, 10 10 10 10 10 10 10 10 10 10 10 10 10	 	2	i in	5.48	7.83	6 6	15.5	13.95
	RANGE	DEG K	301.39	301.34	292.75	688.08 20:08	24. /2 770 . kg	273.80	269.07	262.01	255.70	248.77	2	243.18	224.93	208.51	20.102	194.38	190.53	192.16	199.15	204.65	208.65	211.8	214.53	217.03	23.59	221.10	000.00	20.13	228.90	232.37	236.97	P41.77	26.7.76	257.70	262.12	266.82	270.54 1	8.1.38	270.02	20.00 E	3 6	9	258.76	254.75	80.80 6	246.38
PHODYNAMIC STATISTICAL	GACALEIN MISSLE	L RUN	80.	30.		9.6		35.	5	M +	57	64	55	SB		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7	60	59	38	¥	25	09	90.	- 0. - 0.	07	50.	99.	5	9.6	30	26	M. J.	.74	.75 .13	, «	.67	.69	6	ĸ.	5.	9	P IC	, y		Ý.	1.03	5 2.
THERMOON		r S	6058.1	1.8371	1.6237	1.5166	1.44.0	5000	1.2480	1.1749	1.1905	1.1587	1.2011	1.1675	1.1709	1.196	1.0303	1488.	.7781	.6480	.5078	.4235	.3679	.3300	. 2873	.2588	. 2389	5412	<b>1</b>	43/1.	5651	1298	. 1031	. 0846	.0710	5000.	0418	.0348	.0239	. 0256	92.50	5010	81.10	950 8650	9200.	5.00.	. 0055	. 0059
11.1	913660	5 5 5	0001.010	0008.6001	901.3000	802.2400	712.6300	559.9300	443.0600	433,5500	380.2800	332.2600	289.300n	250.8400	216.0200	159.7100	133 8900	112.7500	94.6010	79.1300	66.5480	56.2880	47.8080	40.6920	34.7350	29.6390	25.4300	21.8170	18.7430	15.1630	0.630	8.88+1	6.6664	5.0349	3.8219	ก เกราะ เกาะ	1.7332	1.3440	1.0069	.8169	.6385	DARY.	. 366c 7105	בייים	1796	1379	5,04.	.0796 .0621
TABLE	STATION	4 <u>₹</u>	8		000	.000	200.		000			000	.000		12.000	100.41	200	15.000	17.000	19.000	19.000	20.000	. 21.000	* 22.000	23.000	24.000	25.000	26.000	20,000	000.85	30.000	32.000	₹.000	36.000	38.000	40.000	44.000	46.000	48.000	50.000	52.000	000.45	20.000	20.000	62.000	64.000	65.000	68.00C 70.000

	O SBON		377.	. agr	3000	392.	392.	392.	391.	388.	Ę ;	357.	355 1		34c.	230	330	, <del>2</del>	% €	2 <u>4</u> 8.	247.	245.	236.	236.	227.	202	225.	9.9	204.	5 2		200.		65	59.	59.		0 0		59.	59.	58.	33	53.	; ;	37.	٠ م	<u>.</u>	ώ
	NOBS T		377.	, cor	y c	392.	395.	395.	391.	388	ָם מייי	367.	, 25 1, 25 1		370.	. 475 . 475	. 02.	, 60 c	24B.	248.	247.	2,45.	236.	23C.	227.	225.	າວວີ.	219.		•	200	. 20	3 6	3	₽.		63.	6		53.	59.	89	28	8.	84.	? ;	, , , ,	. 2	60
	NOBS P	1	377.	, ce	0.00	395.	392.	392.	391.	388.	191	367.	325		, 64 50 5	, 200 225		, 60 c	248.	2 <sup>1</sup> 8.	247.	245.	236.	236.	227.	223.	223.	919	, 20 d			. 680	. 0	20.0	59.	59.	59.		מי	130	59.	58.	55.	53.	ភ្នំ រ	37.	30.	<u>.</u>	ம்
	SKEM D	1	r G	8.5	,	20.	£4	37	15	ະ ເກົ	2)	 95	-1.3 E.1.3	? : !	, c	-	2 2	07	ຕິ	61.	04.	.35	.53	04.	. 20	- 09	<u>\$</u>	.17	.03 .03	ខ្ម	ā.			28.	٤.		5.6	50.	25.	.57	.53	.83	31	. 56	08.	1.07		200	9 6
	S.D. D	0/M3	4.9530	4.8380	2007	3.8900	3.6250	3.4410	2.9400	2.5270	: ::::::::::::::::::::::::::::::::::::	D. 3440	2.1950	1.5860	1.1390	06/0-1	1.1890	1.6810	2.2910	2.9320	2.0240	1.4520	1.0790	.8113	.6027	.5778	0664.	3708	.3350	. 2790	52 h	76.6		1269	1401	.0877	.0706	6490.	coco.	0408	0349	.0281	, 020 <sub>4</sub>	.0152	.0.0.	.0088	.0065	3000	.0025
FEBRUARY	MEAN D	0/M3	154.0000	124.0000	963 8000	865.8000	786.3000	709.8000	639.8000	575.5000	ניים.	464.7000	417.6000	374.8000	334.8900	223.8000	223 1000	201.000	177.8000	143.5000	116.8000	96.2500	80.1700	67.1000	56.5300	47.7200	40.5100	34.4400	29.3400	25.0300	21.3900	18.3000	0082.51	7.2250	5.3740	4.0300	3.0540	2.3250	7050	1.0850	<b>4558.</b>	.6757	.5334	.4206	. 3289	. กระนร	1960	) 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1,060
FEB	SKEN 1		E: 1-		֝֟֝֝֟֝֝֟֝֝֟֝ ֓֓֞֓֞֓֞֞֓֞֞֓֞֞֞֞֞֓֓֞֞֞֞֞֞֞֞֞֞				ð.	80.	-:	rs.	<u>.</u>	0	03	5.6	5 d				26	27	84	55	.03	ĸ.	.07	.17	90.	E	9.	5 5		. <del>.</del>	-,35	10	9.	χ. Ε	80.	90.1	- 09	±	15	0±.1	=:	60'-	 ::		
AMETERS,	5.0. 1	DEG K	= :	2.8	8 3	28	1.30	1.30	1.18	1.87	12	- 80:-	8	8	 	/ · ·	<u> </u>	5 B	27.	90 0	2.71	ភំ	.4. 14.	2.26	- 3	2.30	e.51	2,30	0.43	0 0 1	בה. ים	0 0 1	5.39	10.0	58	4,49	4.12	3. 23 3. 23	. t. 83	. w	15.37	7.40	3.83	4.97	5.66	8.36	9.08	80.0 00.0	20. ñ
HODYNAMIC STATISTICAL PARAMETERS	è ^	DEG K	301.69	301.05	200	284.72	279.45	273.87	269.13	262.14	255.78	248.89	241.23	233.18	224.97	200.7	20.00	101.00	191.88	192.88	199, 33	204.59	208.57	212.13	215.01	217.76	219.84	221.90	223.87	225.81	227 A7	229.75	234.70	24.50	252.07	258.11	263.03	268.00	272.04	# 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	272.94	269.73	266.25	261.9	257.72	255.65	253.19	251.81	255.53
AMIC STATI	. P SKEM P		 3		70.1	30.0	1 33	85	18	02	; ;	.03	01.	60.	<u>.</u>	i.	ດ ຕ		, N	97	M	35	E.	.36	.50	.63	.61	. 59	.67	99.	05	08	6 i	, u	3	3.	.47	យៈ	ត. ភូមិ	ָ ה ה	 	000	50.	.55	.57	.65	0.1.	27	. 55
THERMOOYN	S.D. P	맞	7,409	1.7471	1.5627	6198	1.3133	1.2632	1.2345	1.2200	: ::	1.2202	1.2297	1.1814	1.1638	1.1725	1.1361	1000.1	67/4d	725.1	5396	4356	3693	3292	.2907	5459.	. 2341	0412.	. 1928	. 1802	. 1582	1481	1493	+50°	0620	.0830	.0705	. 0596	.0506	77.0	0275	.0250	6210.	5410.	5110.	8600'	0800	. 0053	00.00.
	5 ¥	<b>£</b>	010.4000	0001.010	901.6000	712 8900	632,0000	558,9900	493.2000	433.7100	300,4000	332.4400	289.5100	251.0300	216.2000	185,5700	158.1700	134.0400	94 8610	79.4.50	66.8580	56.5190	47.9910	40.8570	34.8850	29.8270	25.5610	21.9360	18.8550	16.2260	13 50	12.0860	8.9409	5. 750B	3.03.3 8858	P. 9854	2,3059	1.7899	1.3557	1.0923	0000	52.35	4081	3159	. 2432	. 1862	1541.	. 1069	. 0666
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**開発できるという間隔ののの名の名は、中ではなりでは、一つののののの、「「「」」で、「ここ」「ころう」「ここ」「「** 

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	.8000	.35	196.00	٦. 19	80.	168.3000	2.3690	សុ		DC.1	; ;
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	.4871	25	208.36	1.70	<u>.</u>	95.6400	0.410		247.	247.	1. 1.
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	. 3885	. 20	214.27	1.82	09	67,5600	.6805	56	235.	235.	235.
	01 <del>1</del> 0.	.27	216.81	9.	17	57.0700	.5350		653.		, 6, 6, 6, 6, 7, 6, 8
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JULY	MEAN D	1153.0000	1153.0000	1061.0000	872.1000	783.4000	712.7000	642.0000	577.4000	519.2000	466.5000	419.0000	273.8000	299.0000	264.4000	231.5000	198,9000	166.9000	137.4000	114.1000	95.3900	67.8130	57.3800	48.6030	41.2400	35.0700	29.8900	21.8700	18.7800	13.7800	10.1800	4 5440	4.1630	3.1350	2.3730	1.8330	ביייי	5658	6718	5276	+51+·	.3197	. 2460 1604	1897	0 00	
7	SKEM 1	-1,16	-1.16	٠. چ	2	80	7.1	03	٠.04	0è	<u> </u>	51		9	82.	26	1. t	28	Ŧ.	80.	9.	8	<u> </u>	ű	<u>.</u>	07	- 5	81.	18	.36		9. 1	8.	09	٠. م	07	9 =	80	) <del>-</del>	22	06	79.	¥.	0. 0.		;
RAMETERS.	8.D. T		 8	£.	ਜ਼ਿਲ੍ਹ	đ	8	.90	8	8	08		 	3	8	1.50	1.75	2.27	กั กั		<u>.</u>	3 29		R. 08	<u>ਰ</u>	1.81	e.03	א כ א כ	2.35	3.26	91.	. n	3.6	ų. P	£4.4	5.07	ດີ່ສ	P =	6.67	6.71	7.30	7.59	7.31	9.00	19.91	
ISTICAL PA	F WAN T	301.70	301.69	8 5 6 7 7 7	, 60 , 70 , 70 , 70 , 70 , 70 , 70 , 70 , 7	278.30	272.75	267.24	261.32	254.93	247.92	240.22	הלה הלט המה המת	2.0.0	207.32	200.54	196.94	197.39	202.28	206.44	203.B4	71.0	216.89	219.19	221.58	223.77	225.75	80. P.C.	230.58	233.16	236.65	ָּבְיבָּ בּיבְּיבָ בּיבְּיבָ	253.45	258.61	263.20	264.97	200	6 5 6 6 7 6 7 6 7 6	264.91	361.35	257,65	233.61	248.63	239,98	24.40	
ODYNAMIC STATISTICAL PARAMETERS	SKEH P	8.	8.	₹.	7 - 1	- 20	83	29	10	15	ະ. ຂ	<u>.</u>		9	90	6	07	16		. 33	- F	ָרָ הַלְּיִרָּ יִי	-, 26	27	26	 34	# F	7	, ,	.87	. 32	. 6	3.5	06	=:-	3	00.1	0	6	<u> </u>	01	<u>₹</u>	6. 1	5	75.	
THERMODY	S.D.	1.4185	1.4161	1.3230	1.1505	1.0617	9435	. 8893	. 9287	. 8420	.8063	.8653	Ch06.	25.0	1288	9429	.7887	.6550	.5251	4329	.3716	3087	2804	.2604	.2406	# 10.	1893	1627	1435	. 1358	1235	+C-1.	9890.	.0693	1853.	6840.	- 120	ברים המכים	0232	.0193	.c164	.0145	¥010.	00000	ocon.	-
11.7	HEAN P	_											2004-000														19.3700			9.2164		2.6105	3.0263	2.3267	1.7985	1.3950	/ CAD .	7,77,7	5103	3955	.3051	. 2323	.1757	1306	יבאת.	
TABLE	2 2 3	000	.00	1.000	, v	200.2	n. 000	6.000	7.000	8.000	9.000	10.000	000.11	200	14.000	15,000	16.000	17.000	18.000	19.000	20.000	200.00	23.000	24.000	25.000	26.000	27,000	20.000	30.000	32.000	34.000	36.000	40.000	42.000	4.4	46.000	48.000 1000 1000 1000 1000 1000 1000 1000	30.000	24.000	56.000	58.000	60.000	62.000	64.000	, Juc	2

	NOBS D	ğ	1007	του του του	425.	ເວີ້ລີ	ָּ נְיַהְ				; <u>.</u>	- 0	900	38.	378	369.	362	268.	265.	266.	263.	623	က္က	: :	, r	, ct.	, occ	198	195.	156.	154.	91.	80°.	2 a	. 6	80.	90,	79.	9.6		7.0	77.	ر. ان	65.	48.		35.	٠ ت	ż
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	SKEM O		) o :	3	-, 53	27	.36		-1.02	-1.07	- - -	9	ייי פיי			7	04.	17	.36	ē.	. 15	ų.	38	32	23	S		9 6	. 63	17	16	٠.43	20	99.	: =	60.	-, 33	.31	75.	8 5	מי	8	21.	- 13	0.00	94	77	23	97.
	8.0.0	G/M3	3.6440 8.020	3.0560	3,1420	2.7770	2.2810	2.0340	2.0120	0168.1	. BUGU	1.7870	0188.1	0000	. מלפר	ואלו ו	1.5980	2,1960	2.2930	1.6890	1.1540	9868	7817.	.5421	5115	.4093	. 3770	5005.	2766		.2182	. 1918	1571	1888	. 0890.	.0696	.0567	S440.	.0407	. 3336	7200.		0.59	1210.	4,00	,0055	.0057	4400.	.0029
AUGUST	MEAN D	0/H3	153.0000	051.0000	963,7000	872.6000	789.8000	713.3000	642.4000	577.7000	מיייה הוכי	466, 7000	419.6000	375,3000	333.7000	254 5000	231.2000	198,0000	166,0000	137.2000	114.1000	95.6200	80.4800	67.9500	57.5000	48.7100	41.3400	35. (300	25.5400	2030.10	18,7800	13.6800	10.0800	7.4450	5.5040	3.0840	2.3510	1.8080	1.4000	1.0950	*50B.	15/0	200	3206	24.77	1910	. 1475	.1131	.0872
AUC	SKEH 1	•	. 83	20.				<u>.</u> .	6.	 	ξ.	81.	50	7 1	0.0	55	2	27	1.	.07	-,05	ş	90.	-,29	35	 55	80:-	<u>.</u>	- 3			07	08	90.	1	1	90'	01.	ű	61	9 9	ָרְיִּי מיני		ָ מַלְ	1.	00	0.	<u>.</u> .	 8.
PARAMETERS,	5.0. 1	DEG K	e :	2	2	89	æ.	£.	.87	.93	8	- !	5.	e :		: -		3 2	2,30	5.2	2.06	2.11	P. 10	2.05	<del>.</del> .	2.03 9	8 ! 	1.97	0 K	3 6	)  	3.39	3.48	3.61	. 50 . 50 . 50 . 50		£ 85	5.39	5.17	ය ල	5.08 80.0	0 -	, r , r	2 6	88	8.07	9.72	9.92	9.07
STICAL PAR	HEAN T	DEG K	301.85	19.106	28.88	283.81	278.20	272.59	267.06	261.16	254.17	247.73	233,98	231.91	25.40	60.00	10.000	197.30	198.44	202.77	206.61	209.47	211.96	214.20	216.37	218.54	220.83	222.94	00.00 00.00	20.00	230.00	232.46	236.59	₽£70	7.0.56 5.15 5.15 5.15 5.15 5.15 5.15 5.15 5	26. 27	265,59	268.51	270.53	269.67	266.94	D	203.40	75.4.	250.00 85.00	247.43	2,6,10	248.64	250.52
MIC STATIS	SKEN P			) o c	3 6	12	17	25.	¥5	88	25	 92.	ë.		ง เ	) - 1	2 -	- 5	3 5	20	07	17	23	26	29	28	٠. س		, ,		) M	92	r.	50	9.1	ה	6E.	Ŧ.	.39	.36	.33	S	, r			3 8	9	= :	12
THERMODYNAMIC STATISTICAL P.	S.D. P	æ	1.3063	1.5019	000	9734	. 9256	.8334	. 8252	.8504	.8310	.8502	. 8827	.8875	9:16	26.66	1000	9024	4799	1887	4097	. 3832	. 3362	ああ	.3201	.3033	. 2022	7.55	0622	1100	1001	1897	.1097	.0935	.0816	E 150.	9120.	5770.	.0379	.0316	. 0265	.0444	20.00	5.0.0	7000	7900 ·	.0053	8430.	.0036
11.8	13.3000 TEAN P		1010.7000	010.5000	205.5700	713.6800	632.4700	559,2100	493.1500	433.4800	380.0800	331.9500	288.8400	250.2800	215.3400	184.5500	0097.761	133.0400	מייים מייים	0228.07	67.8480	57.4920	48.9650	41.7800	35.7110	30.5550	26.2030	22.4950	19.3400	0000.01	2020	9,1273	6.8479	5.1639	3.9288	5.000g	1.7912	1.3924	1.0852	.8463	.6591	5125	59/9	. 307.	1950	1357	C 70	1080	0628
TABLE	21412	Σ:		-		3.,00							10.000											22.000	23.000	24·000	25.000	26.000	27.000	20.000	20.00	32.000	34.000	36.000	38.000	20.000	44.000	45.000	48.000	50.000	52.000	54.000	56.000	000.85	60.000	000	56.00	68,000	70.000

	O SBON		420.	423.	400°	463.	423.	423.	, 10,				405	39.7	383.	370.	358.	į		10.40	, d	233	23.5.	229.	230,	223.	215.		156.		.00	.08		G	79.	79.	79.	79.	, c	0 0		75.	63.	47.	37.	90 -	
	NOBS 1		420.	403.	, to	, F. S. S.	423.	423.			465.	1 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	, 10k	397.	383.	370.	358.		, 00.00 00.000 00.0000	0.40	1	27.7	233.	229.	230.	223.	215.		R E	3 5	చే	&	6	Š č	8	.28	75.		6 5	E		77.	ર્જુ		E,	ထို င	
	P SHOW		420.	423.	1 1 1 1 1 1		483.	423.	404	เก็บ รั	423.		406	397.	383.	370.	358.	054.	000 000 000 000 000 000 000 000 000 0		์ บัก		233.	229.	230.	223.		. 200. 200.	195.	. 65	80.	80.	, p.		. 62	79.	79.	79.	j ç	, c		75.	63,	67.	37.	က် က	15.
	CKER		59,		50.	. 03	60	***·	 	85	 			1.87	36	-1.03	ţ.,	ນ.	ខ្ញុំ	6.	200		. 6	33	.30	ű.	33	<b>3</b> !	75.	0 1	00	34			5 -	80.	.23	ວິດ: ເ	0.5	70.	2 0	3 -	<u> </u>	1.28	.73	.16	98. 89.
	c .	G/M3	6.0930	6.0950	3.0450	2.7080	2.4110	2.1420	2.0400	1.9390	1.8380	1.7650	0100.	5166	.9735	1.2560	1.65.20	2.1500	0.4620	00.00.	0.52.1	2500	5510	.4673	.4638	£644.	1510	9114	3050	בינים. הכינים	.2630	. 1863	1,488	.1139	5050°	1690.	.0515	,0384	.0330	1020.	8810. 8810	8 5	9110	.0103	.0091	5000.	.0034
SEPTEMBER	CONSTR	G/M3	1153.0000	152.0000	0000.0001	872.4000	789.5000	712.9000	642.1000	577.4000	519,0000	456.2000	418. /000 475 5000	335,5000	299,0000	264.6000	231.6000	198.9000	167.3000	138.1000	314.5000	97.0400	68.0500	57.4600	48.5609	41.2300	35.0600	29.8600	25.4700	67.7.00	13.5360	10.0000	7.3860	5.4930	4.1160	2,3800	1.8450	0044.1	1.1220	8778	Subo.	P000.	445	+69d	.2009	. 1545	6960.
SE	1 575	-	58		5.1.5	,	60.	60.	\$	. 20	٠ پ	ų.	÷ .	G.	63	.68	θħ.	33	53	21.	٥. :	. t	2 6			<u> </u>	29	2.	08	9.6		37	18	න්. වේ.	<u>.</u>	17	2	.08	.20	.30	90.1	5 -	- 1	# T	61.	<u> </u>	37
PARAMETERS.	6	050 K	1.46	1.47	Br.	3 8	9	66.	8	9. 8.	÷.	5		. A	1.23	¥.	1.40	88	o.37		 8	ับ บัง		ò Ē	2.09	2.00	₽.	2.18	1.82	86 A	- ×	3.63	4.03	3.93	4.57	67. h	4.03	4.89	4.76	50.7	. 35 1	7.0	90.0	50.0 0	10.08	11.17	10.03 8.14
STICAL	RANGE	- MX 37	301.91	301.89	71.762	08.882 20.20	278.25	272.69	267.20	261.36	255.08	9.50 0.10	240 45	20.200	25.50	207.44	200,69	197.09	197.21	201.41	205.57	208.75	617.55	20.00	218.57	220.78	222.91	225.06	227.30	229.21	20.00	23.05 23.05 30.05	845.80	252.25	258.70	968 83	270.05	269.82	270.07	269.41	269.92	000.07	ממלי הת	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	94.5	242.87	945.33 847.83
100 YNAMIC STATISTICAL	MAJALEIN MISSLE			50.	,	5 H					•		- 05 -		- ā	3	84.	Q+.	55	.57	99.	75.	25.		ָ מילי		•	-		a, i	•		9.	61'	6g :	- 6			.05	•	- 0		-			6.	. 5. . 5.
THERMOON	KHAJAL		1.3917	1.3906	1.3104	100	1.1055	1.0078	1.0113	1.0090	66+6	1056.	.9935	9100	0.000	9334	.8722	. 7958	9459.	.5614	11811	. 4612	1) to 1	1814	7.60	3733	. 2932	. 2600	.2247	5,01.	BC/1.	ייים ביי מינים -	1098	6780.	.0733	. USI 3	6650.	.0328	0.50	. 0223	.0186	7510	÷ : :	0.00	00.28	7900	.0057 0039
6 '!!	32. 16.	L	1010,4000	1010.2000	902.0700	803.3400	672 4500	559.2400	493.2100	433.5700	330.2100	332.1300	289.0900	2000	0000.013	157.5700	133.4300	112.5200	94,7040	79.8590	67.6180	57.4240	48.8880	41.6910	35.6500	26.1290	22.4320	19.2920	16.6150	14.3230	12, 3730	9.1411	5.2052	3.9719	5.0501	2.3512	1.430P	1.1153	. 8599	.6784	. 5288	4120	.3197	. 2454	10/01	.1077	2180. 9830.
TABLE	STATION	4 Z	1 000	_	000.1								10.000				15,000	16.000	17.000	19.000	19.000	20.000	21.000	22.000	23.000	25.000	26.000	27.000	29.000	29,000	30.000	36.000	36.000	39.000	40.000	42.000	46.000	48.000	50.000	52.000	54.000			60.000	64.030	66.000	68.000

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	NOBS D	438	440.	£.		ָּבְּילָ מַיּ	440,	440.	439.	447	435.	, 400.	; ; ;	394.	380.	374.		ນ ນິດ ເຄີ	30.5		ų, Š	?¥3.	237.	₹;	- *	636.	602	182.	179.	38.	59.	, or	38.	59.	200	20 8	ត់ខ្លាំ	59,	59	8		196	, M	ູ້ຕູ	15.	<u>.</u>
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	S.D. D	5000 10000	5.9920	3.4300	3.4330	27.82.4	2.4600	2.4130	2.1330	. 3336	2.0470	1.9050	1500	1.0220	1.3650	1.5580	1.8900	6.0420 c.0420	מים בי	0386.1	74.11	.6208	.5290	.5359	0101	0194.	FOCK	3341	.2820	. 1920	1330	1438	.0803	.0757	.0562	1550	, 050.	.0280	.0232	.0197	.0161	55.0	6500	1.00	04:00	.0025
OCTOBER	MEAN D	6773 1153.0000	1153.0000	1060.0000	963,2000	759 3000	712.7000	641.9000	577. 7000	£10,000c	466.0000	418.5000	3.35.4000	298,9000	264.3000	231,5000	199.6000	159.6000	158.5000	95.8600	80.4100	67,7400	57,1800	48.3000	40.9300	34 . 7600	28.000	21.6300	18.5400	13.5100	9.9910	7. 3980 H. 4080	4.1340	3,1590	2.4330	0288.	חמצו ו	8890	, 7004	. 5552	.4335	.3395	י מטמי מטמי	. 1570	1212	+260 '
ŏ	SKEH 1	10.1-			<u>.</u>		17	08	58	2.		ה ה ה	9-3	64	32	.00		07	- 1	000		60	. t3	32	のナ・ ・	99			61	- 09	60	ສຸດ	100	<u>.</u>	39	ų.	01.	9	(A)	39	62.	30	7 5	7	.0.	ų.
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11, 10	E & P	ביים ביים ביים ביים ביים ביים ביים ביים	010,1000	902.0000	803.2200	713.5900	559.2000	493, 1900	433.6000	389.2100	332,1400	269,1300	20.0000	185.0300	157.6100	133.5000	112.9550	94.6830	79.0030	47.1270	48,6220	41.4460	35.4100	30,2750	25.9650	22, 3040	18, 1980	3.50	12,3380	9,1905	6.940	5.2570	3.1012	2.4028	1.8658	1.450W	1.1366	2 69	5393	1614.	. 3243	-020-	*DGI.	6111	.0871	.0662
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TABLE 11. 11 STATION = 913660	11	THERYCONNALIC STATISTICAL PARAMETERS	IC STATISTICAL	STICAL PAR	AMETERS.	(O.:	COVEMBER	c c	0 512/3	0	F 02	S S S
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1010	000	1.5543	<u>*</u> !	301.76	1.46	88	1153.0000	6.1990	න. ස	u		
-	7000	1.6083	<u> </u>	301.75 50.75	7.47	83	1153.0000	5.1840 2.6590	. e3	£ 5	415.	£ 50.
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717 2800	2800	7,56	20.1	28. 12	1.10	16	871.3000	3.1400	-, 09	416.	416.	416.
	32.	- 2467 - 1	06	279.61	1.16	=:-	788.4000	3.0090	30	416.	£18.	416.
	0090	1.2191	15	273.08	1.13	.38	711.3000	2.6170	.69	416.	. t	476.
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	02:00	1.2117	1	240.04	 	7, 1	375 3000	1.5130	67	39+.	39. 30.	394.
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	200	9661	- 70	208.09	<b>.</b>	-1.25	263,9000	1.3740	64	363.	363.	363.
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	3.0458	.0906	-,39	256.39	3.87	07	4.1410	.0955	8.	9		ġ.
	3491	.0751	45	262.06	3.64	18	3, 1250	.0801	1.37			
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52.000	6699	.0323	<u>.</u>	200 200 200 200 200 200 200 200 200 200		76	57.83	.0263	, v	<b>*</b>	45.	, t.t.
•	ביים היים היים	#660 #660	0 00	250.53	5.59	03.1	.5380	.0222	<del>*</del> * * · ·	43.	το. Έ	ξ.
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	S.D. D	1 9570	4.9983	4.2760	4.1540	3.4110	3.1470	6.8350	ייי מימני	25.5	2.2020	2.0540	1.6130	1.1950	1.1740	1.3500	מממט .	1.0030	081416	1.9330	1.3897	.9168	.7552	.5603	.5686	146/0	3485	2012.	Ċ	.1849	1868	1516	956	.0673	7290.	9250.	.0447	7140.	9000	1990.	יייים.	.0163	.0132	<b>1010</b>	.0088	.0053	1000	
DECEMBER	MEAN D	5 M3	154.3000	1062.0000	962.3000	869.8000	786.5000	710.3000	540.2000 676 1000	0001.070	465.2000	417. 300	374.8000	334.7000	298.2000	264 . 1060	25.0000	172 5000	143 3000	116.3000	95.6700	79.7200	66.8800	56.3600	47.6030	40.3800	34.3300	25.0100	000	18.3200	13.3800	9.8500	יינטלט. א האנה א	1000	3.0750	2.3430	1.8040	1.3920	1.0800	0108.	0.00	6804	3202	2485	. 1923	. 1480	04.	
DEC	SKEM 1	1	3	.03	و0.1	50	23	 	Į.	48.	- 12	02.	.35	04.	75.	90.	5.6		3 1	2.5	5	54	P.30	-, 36	80.	<u>ن</u>	, a		100	<u>\$</u> .	.20	.03 .03	. e	200	06	71.	=:-	.07	: :	9 5	ָ י י י		.38	92	12	10		•
PARAMETERS.	5.0.1	יי איני		S	1.31	<u>.</u>	1.19	1.17	<u> </u>	<u>.</u> .	22.1	88.	8.	1.26	- S	38	¥ i	÷ .	 	i d	9,49	9. IZ	P. 12	1.79	ณ์ เ	± ;	<u>.</u> .	n	(S)	96.1	3.23	3.57	. v.	0 . 73 13 3	5.10	ţ.	t.43	£ .	1 2 2	± ;	? y	. r	6.71	8.02	4.6	9 07		
STICAL PAR	F.N. T	DEG K	20.00	293.43	289.07	284.61	279.27	273.65	267.95	00. 10. 10. 10.	248.63	24. US	233.09	224 85	216.60	208.44	500.50	134.63	130.061	190.001	205.48	209.51	212.74	215.61	218.34	220.72	222.91	275.55	0000 0000 0000 0000	230.18	234.67	239.74	± 5.0	הליני הקיני הקיני	₹.092	265.04	267.24	269.29	365.45	267.73	1000	201.02	1,1,00 1,00 1,00 1,00 1,00 1,00 1,00 1,	25.55	252,55	¥5.95	6	
AMIC STATI	SKEW P	3	5.5		٠. و. ا	60	-,58	-, 12	ស្តី. រ	,	3	6	- 15	07	00.	60.	(	50.0	9 8	8 <del>-</del>	72	.37	±.	54.	85.	.27	9. 08.	9.5		91.	£.	<del>,</del>	ָּהָ הַּ	r d	30	.20	. 20	0.	90.	8		<u>.</u>	? =	- a	. 15	81		
THERMODYN	S.D. P		1,7275	1.5958	1.5130	1.4786	1.4879	1.3506	1.3259	7.0917	2464	2200	1.1713	1.1549	1.1324	1.0818	1.0138	9099.	5,533	120.	7867	44.6	3095	.2722	. 2405	. 2210	. 1975	1562	001	1382	. 1486	. 1273	1108	0880.	.0633	.0548	.0464	. 0399	.0325	.0271	.0227	1910.	90.10	20.00	. 1088	. 3068	) ( ) ( ) (	
11. 12		8 × 600	1009.7000	901.2710	E02.4000	712.9000	631.9800	559.900	493.1400	433.6700	225 2000	289.100	250.8200	216.0100	185.3800	157.9900	133.8200	112.7900	מסכה מר	79.CCBU	56.6730	47.9420	40.8350	34.8820	29.623	25.5800	21.9670	18.8900		12,1050	9.0078	6.7754	5.1241	3.9051	2.3018	1.7824	1.3844	1.0775	.8407	. 6552	.5099	, 5500 t	8/05.	6601	1395	.1053		
TABLE	Z	Σg	200.	. 000	2.000	3.000	4.000	5.000	9.000	7.000	9 6	90.0	11.000	12,000	13.000	14.000	15.000	18.000	17.00g	20.00	2000	20.00	22.000	23.000	24.000	25.000	28.000	20.000	200.00	30.000	32.000	34.000	36.000	38.000	42.000	44.000	46.000	48 000	50.000	52.000	54.000	20.000	28.000	00.00	200.45	56.000		

A CONTRACT OF THE PROPERTY OF

11. 13 THERMOT # 913660 KLA. ME'N P S.C. F	PRICONNAHIC STATISTICAL PARAMETERS KAJA: EIK HISSLE RANGE C. P SKEW P MEAN T S.D.	TICAL PAR/ RANGE MEAN T	WETERS, S.D. T	AN SKEM T	ANNUAL. T MEAN D	S.D. D	SKEM D	A SBON	NOBS 1	NOBS C
£	SEG K		DEG K	!	G/M3	6/13	Ċ	170	ä	ğ
- 19	301.73		& c	8,5	1154,0000	5.5430		5033.	5033.	5033.
9654.1	293.63		8 !	.33	1062.0000	4,0630	98.	5038.	5038.	5038.
1.571345	284.88 284.18		51:1		871.5000	3.3710	. 20	5038.	5038.	5038.
1.2181	279.69		1.29	당	788.4000	3.2370	.63	5036.	5035	5036.
. 33	273.13		1.18	χ. <u>.</u>	641,3000	2.6930	5.7	50%	5024.	5024.
1.0974	19.132		1.16	.08	576.9000	2.4400	75	4538.	4938	4938
1.0831 - 18	25.27		진 전 전	2 6	00000	ากาบาน เกาะ		ב מונים ב מונים ב מונים	0001	2000
11.0862	046.53 200.63		1.31	9 : 0	418,4000	1.9770	2.1-	4683.	4683.	£683.
23.53.03 1.110303 E40.07	232.63		 3		375.4000	1.6150	-1.0.1	4627.	4627.	4627.
1.1215 ~.03	224.29		₹. -	06	335.2000	1.1540	09	4527.	4527.	4527.
1.126501	213.00		양.	37	298.6000	1.1090		4406.	4406.	. 405. 41.
1.0987	207.98			- 6	231 7000	1.000 E	- 0	, do	42.6	
	195.88			5 -	200.4000	2.3200	26	3198.	3198.	3198.
. 7503	193 96		3.35	89.	170.1000	3.3093	60	3.07.	3157.	3157.
.6715	196.76		4.67	ຮຸ:	140.9000	3.3100	35.	3151.	3151.	3151.
.6316	202.40		9.60	<del>.</del> .	115,6000	1.6840	r.	3166.	31.05	30.7
70. E-	210.38		ນ ເຄີ	י לע י	80.1000	5106.	. 00.	2943.	2943.	2943.
2004	213.32		6.29	17	67.3700	.8143	26	2933.	2933.	2933.
95. PES9	215 95		.95	09	26.8600	.6824	± !	2837.	2837.	2837.
.4144	218.50		χ, η η	- i	48.0500	7750.		2806.	2806.	2806.
S 02	223.16		9.19		34.6500	5184.	91.	2689.	2688.	2688.
. 2882.	225.36		. 32 32	±	29.5100	4884°	85.	2385.	2385.	2385.
	227.33		2.3	เก็ก	25.2000	3655	ي بي بر	2358.	, 100 100 100 100 100 100 100 100 100 100	6358.
2031 110	1. C.		, o		18.4700	782.	K	2005.	2005.	200g.
18	8.5		3.78	91.	13,4900	. 2520	<u> </u>	765.	735.	758.
.144003	239.45		4.06	0.1	9.9600	1970	08	762.	798.	758.
<u>4</u>	94.91		. a	6 8	7.3650	1632	2	760.	797.	760.
0865	2. 5. 5. 5. 5. 6. 5. 6. 6. 6. 5. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.			68	4.1040	1001.	- -	757.	795.	.57
.073605	262.94		ф ф	8	3.1050	.0807	.10	755.	789.	755.
80 6:30.	265.28		£.83	₹.	2.3710	.0676	08	755.		755.
.051707	258.80		g;	호 6	1.8250	.0576		.10/	141.	
50 825	270.42		က် ကို (	80.	1.4150	0430	20.	7,40	1,000	25.0
.0351	270.37			50.	1.1050	6140.	5 7 6	, 44.0.		4
20.	258.80 250 35		0 t	)   	0/00:	9260	ָרָי , ניי	7.46	730	736.
. 0236	265.73		о п п	 	9224	1660.	. 20	711.	736.	711.
.0133	260.03			2 0	+81+.	.0177	16	675.	708.	675.
n u	250.03 246.03		7 0	1	3266	3710	08	567.	593.	567.
.0103	2 K		9.34	5	6252.	110	3	431.	449.	431.
5 8	. 5 . 5 . 5 . 5		. 83. 83.	90.	1958	.0085	∾.	355.	365.	355.
. 0054	24.9		10.72	37	. 1509	.0066	3	259.	265.	660
. 005424	246.50		11.50	73	.1156	5500.	37	162.	167.	
n636 .003634 249.60	249.60		9.80	58	.0886	.0031	01	.66	. +01	97.

TABLE STATION	111.1 = 9:3660	MOISTURE KHAJAI	RELATED ST LEIN MISSLE	ATISTICAL RANGE	PAPAMETERS.	. JAI	NUARY				
Z	VAPCR P	S.D. VP	SKEW VP	īv	ΤV	SKEH TV	DEWPT T	C D DD*	C1/C11 000		
	MEAN			MEAN	5.D.	SACH IV	MEAN	5.U. UPI	SKEW DPT	NOBS T+P	NOBS TV
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	28.142	2.143	20	30+.60	1.10	-1.18	295.14	1.27	**		
.002	28.102	2.143	21	304.55	1.12	-1.10	296.12	1.28	38 40	413.	413.
1.000	16.090	2.929	02	294.75	1.06	01	287.02	2.92	_	428.	429,
2.000	9.010	3.652	11	289.95	1.52	34	277.27	7.11	60	427.	429.
3.000	4.655	2.753	.63	285.58	1.32	21	267.25	8.38	-1.12	414.	429.
4.000	2.666	1.779	1.08	280.04	1.38	.20	259 96	8.06	15	379.	429.
5.000	1.526	1.07€	1.59	274.29	1.45	.23	253.42	7.20	.20	361.	428.
6.000	.898	.657	1.90	268.49	1.43	.41	247.43	6.73	.54 .73	348.	428.
7.000	.514	.365	2.45	262.41	1.44	.36	241.79	5.81	. 73	344.	425.
8.000	.278	.190	3.13	255.06	1.41	.11	235.87	4.97	.87	339.	423.
a 000	149	.191	3 47	249 11	1.57	.52	230.23	4.11		<i>32</i> 8.	466
10.000	.072	.040	3.75	241.43	1.59	.43	223.91	3.52	1.16	322.	397.
11.000	.035	.0:8	3.94	233.33	1.65	.63	217.95	2.93	1.42	265.	386.
12.000	.014	.005	2.77	224.93	1.35	27	210.95	2.38	.69	262.	379.
13.000	.005	.002	2.28	216.74	1.35	.00	264.17	2.59	.17	199.	372.
14.000	.002	.001	13	208.61	1.33	11	195.07	2.51	63	116.	367.
15.000	99.999	99.999	999.99	201.01	1.32	!5	999,99	99.99	999.99	25.	364.
16.000	99.999	99.999	<del>9</del> 99.99	194.38	1.41	23	999.99	99.99	999.99	3.	353.
17.000	99.999	99.999	999.99	190.53	1.80	.36	999.99	99.99	999.99	0.	278.
18.600	99.999	99.939	999.99	192.16	3.35	.12	999.99	99.99	999,99	0.	274.
19.000	99.999	99.599	999.99	199.15	2.78	14	999.99	99.99		0.	274.
20.000	99.999	99.999	999.99	204.65	2.30	07	999.99	99.33	999.99	0.	270.
21.000	99.999	93.999	999.99	208.65	5.08	09	999.99	99.99	999.99	0.	267.
22.000	99.999	99.999	999,99	18.115	2.07	05	999.99	99.99	999.99	0.	253.
23.000	99.999	99.999	999.99	214.53	1.96	.44	999 99	99.99	999.99	0.	253.
24.000	99.999	99.939	993.99	217.03	2.39	.45	999.99	99.99	939.99	0.	243.
25.000	99.999	99.999	999.99	218.98	2.57	.17	999.99		999.99	0.	248.
26.000	99.999	99.939	999.99	221.16	2.29	.05	993.99	99.99	999.99	0.	245.
27.000	99.999	99.999	999.99	223.33	2.26	.03	999.99	99.59	999.99	0.	239.
28.000	99.999	99.999	999.99	225.13	2.23	.18	999.99	93.99	999.99	0.	211.
29.000	99.999	99.999	999.99	226.93	2.28	.13	999.99	99.99	999.39	0.	210.
30.000	99.993	99.999	999.99	228.90	2.15	.03		99.99	999.99	o.	187.
				0.50	5.13	.03	939.99	99.99	999.99	0.	186.

TABLE STATION	111. 2 • 913560		PELATED STA		PARAMETERS	, FE	BRUARY				
Z	VAPOR P	S.D. VP	SKEH VP	ΤV	ΤV	SKEW TV	DFWPT T	S.D. DPT	SKEW OPT	NOBS T+P	NOBS IV
	MEAN			MEAN	S.D.		MEAN.				
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	28.078	2.176	59	304.89	1.14	97	296.10	1.32	96	377.	377.
.002	28.016	2.162	53	304.86	1.14	95	296.06	1.31	~.90	392.	392.
1.000	15.862	2.713	09	294.67	1.01	25	286.83	2.73	52	391.	392.
2.000	8.851	3.519	~.16	290.05	1.39	05	276.98	7.20	-1.04	377.	392.
3.000	4.603	2.516	.55	285.52	1.29	06	267.37	7.96	36	344.	392.
4.300	2.605	1.603	1.00	280.03	1.34	.39	259.98	7.55	.09	330.	392.
5.000	1.556	.985	1.31	274.36	1.41	.47	253 E8	6.98	.25	323.	392.
6.000	.5/8	.579	2.00	გიძ.ნმ	1 . sē	. 19	247.03	ບີ.ຂໍນໍ	.53	3.7.	ZO:.
7.000	.458	.265	2.02	262.54	1.33	. 17	241.30	4.93	.64	312.	388.
8.000	.255	.116	2.03	256.15	1.41	.36	235.54	3.91	. 44	306.	380.
9.000	.143	.062	2.18	249.23	1.52	,67	230.19	3.37	.82	302.	367.
10.000	.074	.034	2.48	241.53	1.60	.90	224.31	3.24	.97	256.	352.
11.000	.034	.015	3.20	233.35	1.68	.89	217.87	2.78	1.17	253.	347.
12.000	.014	.005	1.91	224.97	1.35	03	2!1.10	2.35	. 35	197.	342.
13.000	.006	.002	.90	215.77	1.37	.04	204.77	2.26	45	183.	338.
14.000	.002	.001	.42	208.71	1.36	01	195.49	2.53	52	26.	335.
15.000	.001	.000	.69	201.20	1.37	04	189.82	2.66	.23		330.
16.000	<b>99.9</b> 99	98.999	999.99	194.94	1.38	.08	999.99	99.99	999.99	0.	248.
17.000	99.999	99.939	999.99	191.26	1.72	01	999.99	99.59	999.99	0.	248.
18.000	99.999	99.999	993.99	192.88	2.95	04	999.99	99.99	999.99	0.	248
19.000	99.999	99.999	999.99	199.33	2.71	26	939.99	99.99	999.99	0.	247.
20.000	99.999	99.999	999.39	204.59	2.54	27	999.99	99.99	999.99	0.	245.
21.000	99,993	99.999	999.99	208.57	2.41	48	999.99	99.99	999.93	0.	236.
22.000	99.999	99.999	939.99	212.13	2.26	22	999.99	99.99	999.99	0.	236.
23.000	99.939	99.999	999.99	215.01	1.99	.03	999,99	99.99	933.99	0.	227.
24.000	99,999	93.999	999.99	217 75	2.30	.31	999.99	99.99	999.99	0.	225
25.000	99.999	99.999	999.55	219.84	2.51	.07	999 99	99.99	999.99	0.	<i>22</i> 5.
23,000	99.999	99.999	993.99	221.90	2.30	.17	999.99	99.99	299.99	0.	219.
27.000	93 990	03.339	553 53	223.97	2.113	.20		òa aa	qqq qq	0.	204.
29.000	99.999	99.999	9.3.99	225.81	2.58	.23	999.95	99.93	999.39	0.	204.
29.000	99.999	99.993	999.99	227.67	2.72	.16	999.99	99.99	999.99	0.	189.
30.000	99.999	99.999	999.99	229.75	2.62	.01	999.99	99.49	999.99	0.	186.

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	111. 3 • 913660	MOISTURE KHAJAI	RELATED S'	TATISTICAL E RANGE	PARAMETERS	. M	ARCH				•
Z	VAPOR P	S.D. VP	SKEW VP	TV	īv	SKEW TV	DEWPT T	C 0 00=			
	MEAN			MEAN	5.D.	DUCH IA	MEAN	5.U. UPI	SKEW OPT	NOBS T+P	NOBS TV
KM	MB	MB		DES K	DEG K		DEG K	250	•		
.000	28.701	2.034	44	305.19	1.18	-1.36	295.47	DEG K			
.002	28.644	2.029	39	305.17	1.17	+1.32	295.47	1.20	64	405.	405.
1.000	16.303	2.874	.01	295.21	1.00	.17		1.19	59	419.	420.
2.000	9.608	3.466	28	290.01	1.09	12	287.24	2.82	~.50	420.	421.
3.000	5.271	2.706	.24	285.23	1.23	.45	278.46	6.40	-1.18	407.	421.
4.000	3.137	1.831	.53	279.65	1.34		269.25	7.99	51	387.	421.
5.000	1.909	1.310	.90	274.05	1.45	.34	262.16	8.18	29	374.	421.
6.000	1.111	.790	1.20	268.44	1.58	.49 .15	255.62	8.42	.05	368.	421.
7.000	.600	.397	1.54	262.40	1.47	.25	249.46	7.73	.25	357.	421.
8.000	.314	.192	1.85	255.07	1.50		243.27	6.37	.38	353.	417.
9.009	.151	üöi	5 53	2.0.00	1.50	. 12 55.	237.04	3.20	.60	337.	405.
10.000	.076	.035	2.18	241.45	1.69		230.8F	4 31	.83	325.	368.
11.000	.035	.016	2.41	233.28	1.71	.37	224.44	3.47	.54	254.	377.
12.000	.014	.005	2.34	224.87	1.48	.35	218.07	2.97	.84	246.	375.
13.000	.006	.002	1.39	216.69	1.47	17	211.26	2.19	1.04	193.	367.
14.000	.002	.001	1.25	208.63		20	204.75	2.18	.04	113.	350.
15.000	.001	.000	12	201.20	1.40	25	196.75	2.44	.00	21.	354.
16.000	99.939	92.999	999.99	195.04	1.23	.15	189.69	2.59	43	g.	351.
17.000	99.999	99.999	999.99	191.54	1.39	.04	999.99	99.99	<b>999.</b> 99	О.	272.
18.000	99.999	99.999	999.99	193.26	2.05	01	999.99	99.99 '		0.	272.
19.000	99.999	99.999	999.99	199.78	3.47	.04	999.99	99.99	999.99	0.	274.
20.000	99.999	99.939	999.99	205.14	2.83	01	999.99	99.99	99.99	0.	269.
21.000	99.999	99.999	999.99	209.49	2.55	.11	999.99	99.93	993.99	σ.	265.
22.000	99.999	99.999	999.99	213.03	2.31	. 38	999.99	99.99	999.99	0.	251.
23.000	99.993	99.999	999.99	215.85	2.23	-02	999.99	99.99	999.99	0.	250.
24.000	99.939	99.999	999.93	218.33	1.75	11	999. <i>3</i> 9	93.99	999.93	0.	241.
25.000	99.999	99.999	999.99	220.55	2.25	04	999. <b>99</b>	99.99	999.99	0.	245.
26.000	99.999	99.939	999.99		2.17	31	999.99	<del>9</del> 9 99	999.99	0.	243.
27.000	99.999	99.999	999.99	222.75	2.17	65	999.99	33 33	999.99	0.	234.
28.000	99.999	93.999	999,99	28.455	2.09	62	999.99	99.99	999.99	0.	205.
29.000	99.999	99. 399	939,99	226.87	2.13	57	999,99	99.99	999.39	0.	203.
30.000	99.999	99,999	999.99	229.08	2.09	.08	999.99	99.99	999.99	0.	174.
		22,333	333.33	231.22	1.94	.21	999.99	٤ 99	999.99	Ů.	172.

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TABLE	111. 4	MOISTUPE	RELATED S	TATISTICAL	PARAMETERS	. AD	RIL				
	<b>913660</b>	KWAJAI	LEIN MI ISLE	RANGE		7. AF	niL				
Z	VAPOR P MEAN	S.D. VP	SKEW VP	TV MEAN	TV S.D.	SKEW TV	DENPT T MEAN	9.D. DPT	SKEM DAL	N085 T+P	NOBS TV
KM	MB	M8		DEG K	DEG K		DEG K	DEG "			
.000	29.578	1.982	56	305.07	1.44	~1.01	295.98	1.14	0		
.002	29.531	1.993	54	305.05	1.47	-1.09	296.95		84	418.	418.
1.000	17.231	2.792	09	295.70	.91	01	288.13	1.15	18	427.	429.
2.000	10.880	3.049	51	290.36	1.03	.31	290.71	2.63	73	427.	428.
3.000	6.561	2.530	32	285.07	1.00	.10	272.91	4.96	-1.49	419.	428.
4.000	4.201	1.960	10	279.30	.95	.00		6.58	~1.15	409.	4 <i>2</i> 8.
5.000	2.591	1.437	.29	273.61	1.04	.37	266.43	7.58	80	398.	428.
6.000	1.559	.924	.56	coa.05	1.04		259.65	8.02	43	395.	428.
7.000	.869	.541	.74	261.94	1.15	. خ <del>ب</del> عد	255.54	7.90	7.65	వర్తం.	1.00.
8.000	.443	.289	1.03	255.62	1.23	.25	247.02	7.31	10	378.	426.
9.000	.214	.133	1.24	248.72	1.23	.16	239.95	6.62	.18	365.	420.
10.000	.095	.057	1.59	241.02	1.35	.56	233.10	5.56	.33	357.	414.
11.000	.040	.020	1.92	232.86	1.35	. 39	225.94	4.71	.26	261.	398.
12.000	.016	.007	1.65	224.48		. 14	218.82	3.62	.47	260.	398.
13.000	.006	.002	.79	216.16	1.37	.03	211.71	2.99	.26	193.	385.
14.000	.001	.001	.18		1.49	09	204.55	3.08	73	105.	375.
15.000	99.999	99.999	999.99	208.13	1.54	20	194.84	3.23	22	13.	370.
16.000	99.999	99.999	999.99	201.01	1.40	15	993.99	99.93	999.99	ч.	365.
17.000	99.999	99.999		195.53	1.35	09	999.99	99.99	999.99	0.	277.
18.000	99.999	99.993	999.99 999.99	192.50	1.76	02	993.99	99.99	999.99	ð.	263.
19.000	99.999	99.999		154.34	2.58	05	999.99	99.99	999.99	0.	268.
20.000	99.999	99.999	999.99	200.71	2.55	.08	999.93	99.99	999.99	0.	266.
21.000	99.999	99.999	999.99	206.32	2.10	.13	999. <b>9</b> 9	99.99	999.99	0.	260.
22.000	99.999	99.999	999.99	210.60	1.96	.10	999.99	99.99	999.99	θ.	250.
23.000	99.999	99.999	999.99	213.81	2.09	. 33	999.99	99.99	999.99	G.	249.
24.000	99.999	99.999	999.99	216.53	1.86	.13	999.99	99.99	999.99	0.	244.
25.000	99.999		999.99	219.07	2.25	. 34	999.99	99.99	939.99	0.	244.
26.000	99.999	99.999	999.99	221.50	2.17	.12	999.93	99.99	999.99	0.	239.
27.000		99.999	999 99	253.52	1-94	.06	999.53	99.99	999.99	0.	227.
	53.387 00.000	33.333	220.23	220 73	1.01	08	<b>გ</b> ნც <b>ბ</b> მ	ōa aà	999 99	n	193.
28.000 29.000	99.999	99.999	999.99	228.21	1.67	19	939.99	99.99	999.39	0.	190.
	99.999	99.999	993.99	230.11	1.73	.00	999.99	99.99	999.93	o.	163.
30.000	99.999	99.999	993.99	232.16	1.46	30	999.99	99.99	999.99	o.	160.
										• • • • • • • • • • • • • • • • • • • •	

TABLE	111. 5	MOISTURE	RELATED ST	ATISTICAL	PARAMETERS	. ·M/	ΑY				
STATION	= 913660	KHAJA	EIN MISSLE	RANGE							
Z	VAPOR P	S.D. VP	SKEW VP	ΤV	TV	SKEH TV	DEWPT T	S.D. DPT	SKEW OPT	N085 T+P	NOBS TV
	MEAN			MEAN	S.D.		MEAN				
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	30.711	1.658	-,44	305.20	1.37	-1.09	297 51	.92	61	438.	438.
.002	30.702	1.654	44	305.19	1.37	-1.10	297.61	.91	61	440.	440.
1.000	18.102	2.473	.00	296,14	.91	56	288.96	2.17	30	440.	441.
2.000	11.623	2.595	62	290.70	1.05	28	281.93	3.90	-1.77	439.	441.
3.000	7.312	2.066	39	285.24	.96	26	275.04	4.59	-1.35	431.	440.
4.000	4.731	1.544	20	279.29	.98	04	268.89	5.25	-1.33	431.	440.
5.000	2.974	1.259	.10	273.52	.93	36	262.39	6.40	95	429.	440.
6.000	1.724	188.	. 36	267.81	1.05	58	255.38	6.84	58	420.	440.
7.000	.933	.513	.50	261.78	1.12	25	248.17	6.77	30	405.	439.
8.000	.495	.277	.68	255.43	1.15	11	241.44	6.17	11	391.	431.
ნ ინა	ンサビ	177	جه.	Sindisa	1 27	05	234.55	5.45	.03	384.	425.
10.000	.110	.055	1.24	240.73	1.33	.08	227.41	4.27	. 23	283.	414.
11.000	.045	.022	1.80	232.66	1.37	12	219.82	3.51	. 74	270.	411.
12.000	.017	. ა07	1.86	224.34	1.35	16	212.18	2.84	.65	203.	395.
13.000	.005	.002	1.08	216.08	1.37	30	205.06	2.61	.00	97.	389.
14.000	.002	.001	.25	208.10	1.39	41	197.10	2.15	68	30.	376.
15.000	99.999	99.999	999.99	201.05	1.41	.17	999.99	93.99	999.99	3.	370.
16.000	99.999	99.999	999.99	196.07	1.53	.16	999.99	99.99	999.99	0.	281.
17.000	99.993	99.999	999.99	194.12	1.80	04	999.99	99.99	999.99	٥.	277.
18.000	99.999	99.999	999.99	196.62	2.00	18	999.99	99.99	939.99	0.	214.
19.000	99.999	99.999	999.99	202.24	2.06	29	999.99	99.99	999.99	0.	272.
20.000	99.999	99.999	999.99	207.27	1.88	32	999.99	99.99	999.93	0.	269.
21.000	99.999	99.999	999.99	211.13	1.75	07	999.99	99.99	999.99	0.	252.
22.000	99.999	99.929	999.99	214.03.	1.80	.09	999.99	99.99	939.99	0.	252.
23.000	99.999	99.999	999.99	216.67	1.70	.16	999.99	99.99	· 999.99	0.	238.
24.000	99.999	99.999	999.99	219.26	1.99	01	999.99	99.99	999.99	0.	240.
25.000	99.999	99.999	999.99	221.90	1.89	.18	999.99	99.99	999.99	0.	232.
26.000	99.999	99.999	999.99	224.34	1.65	.28	999.99	93.99	999.99	0.	218.
27.000	99.999	99.999	993.99	226.58	1.64	06	999.99	99.99	999.99	0.	195.
28.000	99 999	99.999	999.99	228.68	1.66	.01	999 <b>.9</b> 9	99.99	999.39	0.	191.
29.000	99.999	99.999	999.99	230.69	1.85	04	999.99	99.99	999.99	0.	172.
30.000	99.999	99.999	999.99	232.58	1.73	17	999.99	99.99	999.99	0.	167.

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TABLE STATION	111.6 = 913660		RELATED ST		PARAMETERS	. "Մ	JNE				
Z	VAPOR P	S.D. VP	SKEW VP	τv	TV	SKEW TV	DEWPT Y	S.D. DPT	SKEW DPT	NORS T+P	NOBS TV
	MEAN			MEAN	S.D.		MEAN				
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	30.604	1.557	65	305.27	1.32	-1.24	297.56	.87	80	394.	394.
.002	30.592	1.554	64	305.23	1.35	-1.22	297.55	.86	79	397.	398.
1.000	17.709	2.442	.22	296.16	.78	01	288.61	2.17	16	395.	399.
2.000	11.309	2.561	70	230.51	.91	08	281.51	4.03	-1.90	397.	399.
3.000	6.929	2.165	61	285.01	.97	24	274.06	5.60	-1.65	396.	399.
4.000	4.453	1.540	34	279.11	1.03	.20	267.95	5.69	-1.29	393.	399.
5.000	2.827	1.176	02	273.31	.98	.57	261.79	6.31	<del>-</del> .95	387.	39∌.
6.000	1.619	.776	. 34	267.58	1.03	.51	254.78	6,46	58	3.0.	აყა.
7.000	.881	.467	.63	261.49	1.12	.63	247.71	6.32	27	364.	389.
8.000	.447	.241	.77	255.02	1.22	.76	240.57	5.76	09	360.	387.
9.000	.216	.122	1.00	248.02	1.41	.91	233.34	5.33	.14	343.	377.
10.000	.097	.054	1.19	240.37	1.49	1.35	226.14	4.64	.32	232.	356.
11.000	.038	.020	1.55	232.13	1.38	.14	218.42	3.69	.62	227.	360.
12.000	.014	.007	1.58	223.76	1.35	.18	2::.03	3.07	.45	197.	356.
13.000	.005	.002	1.06	215.45	1.41	.14	203.63	3.14	32	79.	348.
14.000	.002	.001	. 34	207.55	1.47	.22	195.67	3.31	55	26.	341.
15.000	99.999	99.999	999.99	200.BI	1.65	-04	999.99	99.99	999.99	0.	337.
16.000	99.999	99.999	999.99	196.63	1.79	.13	999.99	99.99	999.99		254.
17.000	99.999	99.999	939.99	195.00	2.18	.08	999.99	99.99	993.99		250.
18.000	99.999	99.999	939.99	193.60	2.42	08	999.99	99.99	999.93		249.
19.000	99.999	99.999	999.99	204.14	1.95	23	999.99	99.99	929.99	0.	249.
20.000	99.999	99.999	993.99	208.36	1.70	.01	999.99	99.99	999.99	0.	247.
21.000	99.999	99.999	999.99	211 79	1.67	-,14	999.99	99.99	999.99	0.	236.
22.000	99.999	99.999	999.99	214.27	1.92	-,09	999.99	99.99	999.99	0.	235.
23.000	99.999	99.999	999.99	216.81	1.66	17	999.99	99.99	999.99	0.	229.
24.000	99.999	99.999	999.99	219.42	1.89	.07	999.99	99.99	999.99	0.	228.
25.000	99.999	99.999	999.99	281.82	1.83	.05	999.99	99.99	999.99	0.	228.
26.000	99 999	99.999	999.99	224.13	1.72	23	999,99	99.99	999.99	0.	217.
27.000	99.939	99.999	933.99	226.45	1.67	.02	993.99	99.93	233.22	0.	127
29.000 29.000	99.999 99.999	99.999	999.99	228.48	1.78	29	999.99	99.99	999.39	0.	184.
30.000		99.999	999.99	230.44	2.01	06	999.99	99.99	999.99	0.	164.
30.000	99.999	99.999	999.99	231.89	2.12	15	999.99	99.99	999.99	0.	153.

Z         VAPOR P         S.D. VP         SKEH VP         TV         TV         S.D. HEAN         DEMPT T         S.D. DPT         SKEH DPT         NOBS T+P         NOES L           KM         HB         HB         DEG K	TABLE	111. 7	MOISTURE	RELATED ST	TATISTICAL	PARAMETERS		ULY				
MEAN   MB   MB   MB   DEG   N   DE							<i>f</i> *r					
Math	~		5.U. VP	SKEM VP			skew tv		S.D. DPT	SKEW DPT	NOBS T+P	NOES . '
.000 30.617 1.41227 305.20 1.36 -1.15 297.57 .7843 399. 399002 30.611 1.41127 305.19 1.35 -1.15 297.57 .7843 400. 400. 400. 17.933 2.33604 295.24 .7626 288.82 2.0845 400. 400. 30.001 1.727 2.26549 290.55 .8709 282.18 3.22 -1.37 399. 400. 400. 3.000 7.350 1.90059 285.03 .8822 275.20 4.32 -1.149 398. 400. 400. 4.000 4.732 1.44446 279.10 .90 1.16 268.97 5.00 -i.44 395. 400. 5.000 3.028 1.07504 273.32 .9451 263.02 5.28 -1.02 395. 400. 5.000 1.775 .705 .13 267.62 .9004 255.31 5.4577 386. 400. 7.000 .931 .405 .52 261.56 .97 .04 248.82 5.21 .93 380. 399. 8.000 4.75 .228 .81 255.07 .9901 241.48 5.1630 375. 394. 9.000 231 .119 1.09 247.99 1.0915 234.23 4.89 .01 363.32 5.28 1.000 231 .119 1.09 247.99 1.0915 234.23 4.89 .01 363.32 5.20 1.100 .039 .049 1.18 240.26 1.2113 225.55 4.24 .08 294.51 1.000 .039 .017 1.54 232.15 1.3103 218.89 3.21 .68 249. 358. 12.000 .014 .006 1.92 223.67 1.31 .05 211.01 2.64 .79 216. 332. 13.000 .005 .002 1.70 215.34 1.32 1.6 203.90 2.96 .09 74. 341. 14.000 .005 .002 1.70 215.34 1.32 .16 203.90 2.96 .09 74. 341. 14.000 .000 .99 99.99	VM		MO									
.002 30.611 1.41127 305.19 1.35 -1.15 297.57 .7843 399. 399. 1.000 17.933 2.33604 295.24 .7626 268.82 2.0845 400. 400. 2.000 11.727 2.28549 290.55 .8709 282.18 3.22 -1.37 399. 400. 3.000 7.350 1.90059 285.03 .8822 275.20 4.32 -1.49 398. 400. 4.000 4.732 1.44446 279.10 .90 .16 269.97 5.00 -i.44 395. 400. 5.000 3.028 1.07504 273.32 .9451 263.02 5.28 -1.02 395. 400. 5.000 3.028 1.07504 273.32 .9451 263.02 5.28 -1.02 395. 400. 6.000 1.775 .705 .13 267.62 .9004 255.31 5.4577 386. 402. 7.000 .931 .405 .52 261.56 .97 .04 248.82 5.2139 380. 388. 8.000 .475 .228 .81 255.07 .9901 241.48 5.1630 375. 394. 9.000 .231 .119 1.09 247.99 1.0915 234.23 4.89 .01 363. 382. 10.000 .099 .049 1.18 20.26 1.2113 226.56 4.24 .08 259. 501. 11.000 .039 .017 1.54 232.15 1.3103 218.89 3.21 6.88 248. 358. 12.000 .014 .006 1.97 223.67 1.31 .05 211.01 2.64 .79 216. 352. 13.000 .005 .002 1.70 215.34 1.22 1.16 203.90 2.96 .09 74. 14.000 .099 .999 99.99 99.99 196.84 1.5026 189.06 4.11 36 7.2 33. 335. 15.000 .001 .000 .78 200.54 1.5026 189.06 4.11 36 7. 334. 15.000 .99.999 99.99 99.99 196.84 1.5526 189.06 4.11 36 7. 334. 16.000 99.999 99.999 99.99 196.84 1.5526 189.06 4.11 36 7. 334. 16.000 99.999 99.999 99.99 196.84 1.5526 189.06 4.11 36 7. 334. 16.000 99.999 99.999 99.99 202.28 2.24 4.4 999.99 99.99 99.99 99.99 0. 265. 19.000 99.999 99.999 99.99 202.28 2.24 4.4 999.99 99.99 99.99 99.99 0. 265. 20.000 99.999 99.999 99.99 202.84 2.25 2.4 41 999.99 99.99 99.99 99.99 0. 265. 20.000 99.999 99.999 99.99 206.44 1.81 .08 999.99 99.99 99.99 99.99 0. 265. 20.000 99.999 99.999 99.99 214.69 1.82 .02 999.99 99.99 99.99 99.99 0. 265. 20.000 99.999 99.999 99.99 216.89 1.29 2.02 99.99 99.99 99.99 99.99 99.99 90. 226.00 226.00 99.999 99.99 99.99 226.84 1.81 .09 99.99 99.99 99.99 99.99 90. 226.00 226.00 99.999 99.99 99.99 99.99 90. 226.00 99.99 99.99 99.99 99.99 99.99 99.99 90. 226.00 99.99 99.99 99.99 90. 226.00 99.99 99.99 99.99 99.99 90. 226.00 99.99 99.99 99.99 99.99 90. 226.00 9								DEG K	DEG K			
1.000 17.933 2.336 -0.04 295.24 .76 -2.26 288.82 2.08 -4.5 400. 400. 400. 20. 11.727 2.265 -4.9 200.55 .87 -0.9 282.18 3.22 -1.37 399. 400. 400. 400. 400. 400. 400. 400. 4								297.57	.78	43	399.	399.
2.000				_			-1.15	297.57	.78	43		
3.000       17.26       2.285      49       250.55       .87      09       262.18       3.22       -1.37       399.       400.         4.000       4.732       1.444      46       279.10       .90       .16       268.97       5.00       -1.44       395.       400.         5.000       3.028       1.075      04       273.32       .94      51       263.02       5.28       -1.02       395.       400.         6.000       1.775      705       .13       267.62       .90      04       255.31       5.45      77       386.       400.         7.000       .931       .405       .52       261.56       .97       .04       248.82       5.21      39       380.       389.         8.000       .475       .228       .81       255.07       .99      01       241.48       5.16      30       375.       394.         9.000       .099       .049       1.18       240.26       1.21       -13       225.56       4.24       .08       259.56       1.10       2.02       1.00       200.00       2.00       2.01       1.54       232.15       1.31      03       21							26	268.82	2.08	45		
4.000		_					09	282.18	3.22	-		
5.000						.88	22					
5.000 3.068 1.07504 273.32 .9451 263.02 5.28 -1.02 395. 460. 6.000 1.775 .705 .13 267.62 .9004 255.31 5.4577 386. 460. 7.000 .931 .405 .52 261.56 .97 .04 248.82 5.2139 380. 389. 8.000 .475 .228 .81 255.07 .9901 241.48 5.1630 375. 334. 9.000 .231 .119 1.09 .47.99 1.0915 234.23 4.89 .01 363. 382. 10.000 .099 .049 1.18 240.26 1.2113 225.56 4.24 .08 259. 507. 11.000 .039 .017 1.54 232.15 1.3103 218.89 3.21 .68 248. 358. 12.000 .014 .006 1.9c 223.67 1.31 .05 211.01 2.64 .79 216. 352. 13.000 .005 .002 1.70 215.34 1.32 1.6 203.90 2.96 .09 74. 341. 14.000 .002 .001 2.01 207.32 1.38 .26 195.43 2.94 .72 33. 335. 15.000 .001 .000 .78 200.54 1.5026 189.06 4.11 .36 7. 334. 16.000 99.999 99.999 999.99 196.84 1.7545 999.99 99.99 999.99 .0 .263. 19.000 99.999 99.999 999.99 202.28 2.24 .41 999.99 99.99 999.99 0. 263. 19.000 99.999 99.999 999.99 202.28 2.24 .41 999.99 99.99 999.99 0. 256. 22.000 99.999 99.999 999.99 202.28 2.24 .41 999.99 99.99 999.99 0. 256. 22.000 99.999 99.999 999.99 214.64 1.81 .08 999.99 99.99 999.99 0. 256. 22.000 99.999 99.999 999.99 209.84 1.65 .07 999.99 99.99 999.99 0. 256. 22.000 99.999 99.999 999.99 214.64 1.82 .02 999.99 99.99 999.99 0. 229.26 229.26 2.24 .41 999.99 99.99 99.99 99.99 0. 225. 22.000 99.999 99.999 99.99 221.46 1.82 .02 999.99 99.99 99.99 99.99 0. 226. 22.000 99.999 99.999 99.99 221.46 1.82 .02 999.99 99.99 99.99 99.99 0. 226. 22.000 99.999 99.999 99.99 221.46 1.82 .02 999.99 99.99 99.99 99.99 0. 226. 22.000 99.999 99.999 99.99 221.58 1.94 .01 999.99 99.99 99.99 99.99 0. 226. 22.000 99.999 99.999 99.99 225.76 2.03 .11 990.99 99.99 99.99 99.99 0. 226. 22.000 99.999 99.999 99.99 225.76 2.03 .11 990.99 99.99 99.99 99.99 0. 167. 22.000 99.999 99.999 99.99 225.76 2.00 .11 990.99 99.99 99.99 99.99 0. 167. 22.000 99.999 99.999 99.99 225.76 2.00 .11 990.99 99.99 99.99 99.99 99.99 0. 167. 22.000 99.999 99.999 99.99 225.76 2.00 .11 990.99 99.99 99.99 99.99 0. 167. 22.000 99.999 99.999 99.99 225.76 2.00 .11 990.99 99.99 99.99 99.99 0. 167.						.90	.16	268.97	5.00			
6.000       1.775       .705       .13       267.62       .90      04       255.31       5.45      77       386.       .463.         7.000       .931       .405       .52       261.56       .97       .04       248.82       5.21      33       380.       383.         8.000       .475       .228       .81       255.07       .99      01       241.48       5.16      30       375.       394.         9.000       .231       .119       1.09       247.99       1.09      15       234.23       4.89       .01       363.3       382.         10.000       .099       .049       1.18       240.26       1.21      13       225.56       4.24       .08       259.3       367.         11.000       .039       .017       1.54       232.15       1.31      03       218.89       3.21       .68       249.35       352.         12.000       .014       .006       1.92       223.67       1.31       .05       211.01       2.64       .79       216.352.         13.000       .002       .001       2.01       207.32       1.38       .26       195.43       2.94       .					273.32	.94	51			-		
8.000					267.62	.90	04					
8.000				.52	261.56	.97	.04	248.82				
9.000				.81	255.07	.99	01	241.48				
11.000			.119	1.09	247.99	1.09	15					
11.000		.099	.049	1.18	240.26	1.21	13					
12.000		.039	.017	1.54	232.15	1.31						
13.000       .005       .092       1.70       215.34       1.32       .16       203.90       2.96       .09       74.       341.         14.000       .002       .001       2.01       207.32       1.38       .26       195.43       2.94       .72       33.       335.         15.000       .001       .000       .78       200.54       1.50      26       189.06       4.11       .36       7.       334.         16.000       99.999       99.999       99.99       197.39       2.27      28       999.99       99.99       99.99       0.       263.         17.000       99.999       99.999       99.99       202.28       2.24       .41       999.99       99.99       99.99       0.       263.         18.000       99.999       99.999       999.99       202.28       2.24       .41       999.99       999.99       999.99       0.       263.         19.000       99.999       99.999       999.99       202.28       2.24       .41       999.99       999.99       999.99       0.       256.         20.000       99.999       99.999       999.99       202.64       1.65       .07 <t< td=""><td></td><td></td><td>.005</td><td>1.98</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>			.005	1.98								
14.000		.005	.002	1.70	215.34	1.32				_		
15.000		.002	.001	2.0;	207.32							
16.000 99.993 99.999 999.99 196.89 1.7545 939.99 99.99 999.99 0. 263. 17.000 99.999 99.999 999.99 202.28 2.24 .41 999.99 99.99 999.99 0. 261. 19.000 99.999 99.999 999.99 205.44 1.81 .08 999.99 99.99 999.99 0. 265. 20.000 99.999 99.999 999.99 212.45 1.65 .07 999.99 99.99 999.99 0. 269. 21.000 99.999 99.999 999.99 212.45 1.6206 999.99 99.99 999.99 0. 279. 22.000 99.999 99.999 212.45 1.82 .02 999.99 99.99 993.99 0. 279. 23.000 99.999 99.999 214.64 1.82 .02 999.99 99.99 99.99 0. 279. 23.000 99.999 99.999 999.99 216.89 1.82 .14 999.99 99.99 999.99 0. 226. 24.000 99.999 99.999 999.99 219.19 2.08 .21 999.99 99.99 999.99 0. 224. 25.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 224. 26.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 217. 26.000 99.999 99.999 999.99 225.77 1.8107 999.99 99.99 999.99 0. 202. 27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 99.99 99.99 99.99 99.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 99.99 99.99 99.99 99.99 0. 169. 28.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 99.99 99.99 0. 140.		.001	.000	.78	200.54							
17.000 99.999 99.999 999.99 197.39 2.2728 999.99 99.99 999.99 0. 263. 18.000 99.999 99.999 999.99 202.28 2.24 .41 999.99 99.99 999.99 0. 261. 19.000 99.999 99.999 999.99 205.44 1.81 .08 999.99 99.99 999.99 0. 256. 20.000 99.999 99.999 999.99 212.45 1.65 .07 999.99 99.99 999.99 0. 249. 22.000 99.999 99.999 999.99 212.45 1.6206 999.99 99.99 993.99 0. 233. 23.000 99.999 99.999 999.99 214.64 1.82 .02 999.99 99.99 993.99 0. 233. 23.000 99.999 99.999 999.99 216.69 1.82 .14 999.99 99.99 999.99 0. 226. 24.000 99.999 99.999 999.99 219.19 2.08 .21 999.99 99.99 999.99 0. 224. 25.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 224. 25.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 217. 26.000 99.999 99.999 999.99 225.77 1.8107 999.99 99.99 999.99 0. 202. 27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 99.99 99.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 99.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 99.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 99.99 99.99 0. 169.		<b>99</b> .993	99.999	999.99	196.84					900 00	/.	
18.000 99.999 99.999 999.99 202.28 2.24 .41 999.99 99.99 999.99 0. 251. 19.000 99.999 99.999 999.99 205.44 1.81 .08 999.99 99.99 999.99 0. 255. 20.000 99.999 99.999 999.99 209.84 1.65 .07 999.99 99.99 999.99 0. 249. 21.000 99.999 99.999 999.99 212.45 1.82 -0.6 999.99 99.99 999.99 999.99 0. 239. 22.000 99.999 99.999 999.99 214.64 1.82 .02 999.99 99.99 999.99 0. 239. 23.000 99.999 99.999 999.99 216.69 1.82 .14 999.99 99.99 999.99 0. 225. 24.000 99.999 99.999 999.99 219.19 2.08 .21 999.99 99.99 999.99 0. 224. 25.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 217. 26.000 99.999 99.999 999.99 223.77 1.81 -07 999.99 99.99 999.99 0. 207. 27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 999.99 0. 169. 29.000 99.999 99.999 999.99 229.26 2.33 -16 999.99 99.99 99.99 0. 140.	17.000	99.999	99.999	999.99	197.39					222.22	٥.	
19.000 99.999 99.999 999.99 205.44 1.81 .08 999.99 99.99 999.99 0. 256. 20.000 99.999 99.999 999.99 212.45 1.8206 999.99 99.99 999.99 0. 239. 22.000 99.999 99.999 999.99 214.64 1.82 .02 999.99 99.99 999.99 0. 239. 23.000 99.999 99.999 999.99 216.69 1.82 .14 999.99 99.99 999.99 0. 226. 24.000 99.999 99.999 999.99 216.69 1.82 .14 999.99 99.99 999.99 0. 226. 25.000 99.999 99.999 999.99 219.19 2.08 .21 999.99 99.99 999.99 0. 224. 26.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 217. 26.000 99.999 99.999 999.99 223.77 1.8107 999.99 99.99 999.99 0. 217. 27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 205. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 999.99 0. 167. 29.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 999.99 0. 167. 29.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 999.99 0. 140.		99.999	99.999	999.99	202.28							
20.000       99.999       99.999       999.99       209.84       1.65       .07       999.99       99.99	19.000	99.999	99.999	999.99								
21.000 99.999 99.999 999.99 212.45 1.8206 999.99 99.99 993.99 0. 233. 22.000 99.999 99.999 999.99 214.64 1.82 .02 999.99 99.99 999.99 0. 233. 23.000 99.999 99.999 999.99 216.69 1.82 .14 999.99 99.99 999.99 0. 226. 24.000 99.999 99.999 999.99 219.19 2.08 .21 999.99 99.99 999.99 0. 224. 25.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 217. 26.000 99.999 99.999 999.99 223.77 1.8107 999.99 99.99 999.99 0. 202. 27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 999.99 0. 167. 29.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 999.99 0. 140.	20.000	99.999	99.999									
22.000       99.999       99.999       999.99       214.64       1.82       .02       999.99       99.99       99.99       0.236.         23.000       99.999       99.999       99.99       216.69       1.82       .14       999.99       99.99       99.99       0.236.         24.000       99.999       99.999       99.99       219.19       2.08       .21       999.99       99.99       99.99       0.224.         25.000       99.999       99.999       99.99       221.58       1.94       .01       999.99       99.99       999.99       0.217.         26.000       99.999       99.999       99.99       223.77       1.81      07       999.99       99.99       99.99       0.226.         27.000       99.999       99.999       225.76       2.03       .11       999.99       99.99       99.99       0.167.         28.000       99.999       99.999       227.66       2.10       .06       599.99       99.99       99.99       0.167.         29.000       99.999       99.999       229.26       2.33      16       999.99       99.99       99.99       0.140.	21.000	99.999	99.993	999.99			-					
23.000 99.999 99.999 999.99 216.89 1.82 1.14 999.99 99.99 999.99 0. 225. 24.000 99.999 99.999 999.99 219.19 2.08 21 999.99 99.99 999.99 0. 224. 25.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 217. 26.000 99.999 99.999 999.99 223.77 1.8107 999.99 99.99 999.99 0. 202. 27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 999.99 0. 167. 29.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 999.99 0. 140.	22.000	99.999	99.939									
24.000       99.999       99.999       999.99       219.19       2.08       .21       999.99       99.99       99.99       0.       224.         25.000       99.999       99.999       999.99       221.58       1.94       .01       999.99       99.99       99.99       0.       224.         26.000       99.999       99.999       999.99       223.77       1.81      07       999.99       99.99       99.99       0.       202.         27.000       99.999       99.999       999.99       225.76       2.03       .11       999.99       99.99       999.99       0.       167.         29.000       99.999       99.999       999.99       227.66       2.10       .06       599.99       99.99       99.99       0.       167.         29.000       99.999       99.999       999.99       229.26       2.33      16       999.99       99.99       999.99       0.       140.	23.000	99.999	99.999	999.99								
25.000 99.999 99.999 999.99 221.58 1.94 .01 999.99 99.99 999.99 0. 217. 26.000 99.999 99.999 999.99 223.77 1.8107 999.99 99.99 99.99 0. 202. 27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 999.99 0. 167. 29.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 999.99 0. 140.	24.000	99.999	99.999	999.99								
26.000 99.999 99.999 999.99 223.77 1.8107 999.99 99.99 99.99 0. 207.000 99.999 99.99 999.99 225.76 2.03 .11 999.99 99.99 999.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 99.99 0. 167. 29.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 999.99 0. 140.	25.000	99.999	99.999	999.99							-	
27.000 99.999 99.999 999.99 225.76 2.03 .11 999.99 99.99 99.99 0. 169. 28.000 99.999 99.999 999.99 227.66 2.10 .06 999.99 99.99 99.99 0. 167. 29.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 999.99 0. 140.	26.000	99.999	99.999									
28.000 99.999 99.999 999.99 227.66 2.10 .06 599.99 99.99 99.99 0. 167. 29.000 99.999 99.999 999.99 229.26 2.3316 999.99 93.99 999.99 0. 140.	27.000	99.999										
29.000 99.999 99.999 999.99 229.26 2.3316 999.99 99.99 999.99 0. 140.	28.000	99.999										
70 000 00 000 00 000 000 000 000 000 00	29.000										_	
	30.000	99.999		999.99	230.58	5.22	18	999.99	99.99	979.99	U.	140. 138

TABLE	111. 8		RELATED ST		PAPAMETERS	i, AU	IGUST				
	= 913650		LEIN MISSLE		<b></b> *	545H T1	DENPT T	S.D. CPT	SKEW OPT	NOSS T+P	NOBS TV
Z	VAPOR P	S.D. VP	SKEW YP	TV	ŢV	SKEW TV		5.0. LP1	SKEW UP!	11053 146	14055 14
	MEAN			MEAN	S.D.		MEAN	050 11			
KM	MB	MB		DEG K	DEG K		DEG K	DEG K	00	421	421.
.000	30,476	1.504	.14	305.31	1.40	80	297.49	.83	02	421. 424.	424.
.002	30.466	1.499	.14	305.30	1.39	81	297.48	.82	02	-	425.
1.000	17.717	2.293	.06	236.21	.76	.47	288.63	2.05	27	423.	425.
2.000	11.753	2.110	48	290.43	.88	.55	282.26	2.95	-1.46	422.	
3.000	7.255	1.860	51	284.93	.88	.15	275.03	4.28	-1.57	420.	425.
4,000	4.618	1.455	17	278.99	. 64	.14	258.57	4.65	-1.05	4:8.	n54.
5.000	2,832	1.158	.20	273.13	.82	.30	261.85	6.00	88	419.	424.
6.000	1.345	.799	.69	267.42	. ક્ટ	.60	<b>೭</b> 55.07	6.15	41	410.	4cs.
7.000	.893	.475	1.05	261.39	.98	.47	247.89	5.85	.07	405.	421.
8.000	.459	.258	1.23	254.92	1.07	.60	240.77	5.75	.20	396.	418.
9.000	.218	.126	1.45	247.81	1.20	.55	233.51	5.08	. 36	381.	411.
10.000	,099	.059	1.59	240.06	1.39	1.82	226.21	4.72	.48	266.	408.
11.000	.039	.022	2.10	231.92	1.27	12	219.62	3.80	. 25	c57.	400
12.000	.014	.007	2.77	223.45	1.22	.05	210.90	2.97	1.04	235.	385.
13.000	.006	.003	2.52	215.05	1.17	03	204.13	3.28	.67	72.	375.
14.000	.001	.001	1.64	207.02	1.19	.61	194.83	2.31	.73	55.	359.
15.000	,001	.000	.57	200.50	1.33	.09	190.23	2.59	22	9.	368.
16.000	99.999	99.999	999.99	197.59	1.74	27	999.9 <del>9</del>	99.99	999.99	٥.	568.
17,000	99.999	99.999	999.99	198.44	2.30	~.40	999.99	99.99	999.99	0.	265.
18.000	99.999	99.999	999.99	202.77	2.11	.07	999.99	99.99	999.99	0.	285.
19.000	99,999	99.999	999.99	: 35.61	2.05	05	999.99	99.99	999.99	0.	263.
20.000	99.939	99.999	939.39	209.47	2.11	.04	<b>5</b> 99.99	99.99	999.99	0.	259.
21.000	99.999	99.999	999.99	211.96	2.10	.06	999.99	99.99	939.99	0.	252.
22.000	99.999	99.999	999.99	214.20	2.02	29	999.99	99.99	939.99	0.	25!.
23.000	99,999	99,999	999.99	216.37	1.92	35	999.99	93.99	999.99	0.	243,
24.000	99.999	99.999	923.99	218.54	2.09	55	939.93	99.99	<i>დ</i> )9.93	0.	243.
25.000	99,999	99.999	993.99	220.83	1.99	08	999.99	99.99	999.99	σ.	239,
26.000	99,999	99.999	999.99	212.94	1.97	14	999.99	99.99	999.99	ο.	228.
27.000	99.578	99.335	565.99	245.33	2.16	.::	322.93	30°85	ටි <b>ා</b> ට් පට	Ú	100
28.000	99.999	99.999	993.99	227.00	1.93	.14	999.99	99.99	939.39	0.	192.
29.000	93.999	99.999	999.99	228.73	2.29	.19	999.99	99.39	999.99	0.	156.
30.000	99.999	99.999	999.99	230.00	2.41	02	999.99	99.99	939.99	0.	154.
30.000	22.23	22.223	333.33	250.50							

TABLE	111. 9 = 913650				PARAMETERS	. SE	PTEMBER				
			LEIN MISSLE		•						
Z	VAPOR P	S.D. VP	SKEW VP	TV	TV	SKEH TV	DEWPT T	S.D. DPT	SKEW DPT	NOBS T+P	NOBS TV
	MEAN			MEAN	5.D.		MEAN				
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	30.487	1.590	30	305.40	1.55	68	297.49	.88	45	420.	420.
.002	30.472	1.585	30	305.38	1.56	68	297.49	.88	45	423.	4 <i>2</i> 3.
1.000	17.921	2.638	21	295.37	.79	29	288.77	2.41	84	423.	423.
2.000	11.962	2.353	31	290.51	.93	.01	282.48	3.22	-1.25	420.	423.
3.000	7.604	1.879	38	285.00	.91	.03	275.74	4.G÷	-1.45	420.	423.
4.000	4.839	1.586	37	279.06	.91	.02	269.15	5.45	-1.47	420.	4 <i>2</i> 3.
5.000	3.103	1.207	04	273.28	.90	.13	263.12	5.95	-1.04	420.	423.
6.000	1.802	.819	.25	267.58	.89	-11	256.16	6.31	71	418.	424.
7.000	.985	.484	.51	261.59	.96	.41	248.80	6.28	50	412.	424.
8.000	.516	.27:	.81	255.23	1.09	.67	242.07	5.98	31	359,	423.
0.000	,?5,2	135	.09	2.3.19	1.21	59	234.93	5 28	64	397.	419.
19.000	.113	.063	1.08	240.52	1.28	.79	227.42	4.85	.19	250.	407.
11.000	.045	.024	1.30	232.42	1.36	.98	219.59	4.23	.21	254.	402.
12.000	.016	.008	1.81	223.93	1.24	.52	211.77	3.28	.47	224.	397.
13.000	.005	.003	1.42	215.50	1.23	.49	204.89	2.97	.23	92.	393.
14.000	2002	.001	.27	207.44	1.34	.62	196.80	2.06	41	35.	370.
15.000	.001	.000	.49	500.69	1.40	.48	190.28	2.19	03	8.	359.
16.000	99.993	99.999	<b>99</b> 9.99	197.09	1.68	33	993.99	99.99	999.99	0.	254.
17.000	99.999	99.999	999.99	197.21	2.37	53	999.99	99.99	999.99	0.	250.
18.000	99.999	99.999	999.99	201.41	2.53	.12	999.99	99.99	999.99	0.	248.
19.000	99.993	99.999	999.99	205.57	2.26	.06	999.99	99.99	999.99	0.	244.
20.000	99.993	99.999	999.99	208.75	2.22	.13	999.99	99.99	999.99	0.	241.
21.000	99.999	99.999	999.99	211.33	2.04	.37	999.99	99.99	999.99	0.	233.
22.000	99.999	99.999	999.99	213.41	1.87	.29	999.99	99.99	999.99	0.	233.
23.000	99.999	99.999	993.99	215.95	1.74	.17	999.99	99.99	999.99	0.	229.
24.000	59.999	99.939	999.99	218.57	2.09	.19	993.93	99.99	233.23	0.	230.
25.000	99.939	99.999	999.99	220.78	2.00	14	993.99	99.99	999.99	0.	223.
26.000	99.999	99.999	999.99	222.91	1.94	28	999.99	99.99	99.99	6.	215.
27.000	99.999	99.999	999.99	225.06	2.18	.04	999.99	99.99	9.99	0.	200.
28.000	99.999	99.999	999.99	227.30	1.82	- 08	929.99	99.99	±99.99	٥.	195.
29.000	99.999	99.999	999.99	229.21	2.08	.00	999.99	99.99	999.99	0.	158.
30.000	99.999	99.999	999.99	230.92	1.54	29	999.99	99.99	999.99	0.	159.

المؤسسة والمقامة والمقام والمقام والموقع ومخاوة والمقامة والماها والمعامة والمقامة و

TABLE	111. 10		RELATED ST		PARAMETERS	s. od	TOBER				
	<b>913</b> 660		LE IN MISSLE								
Z	VAPOR P	S.D. VP	SKEH VP	۲V	TV	SKEW TV	DEMPT T	S.D. QPT	SKEH DPT	NOBS T+P	NOBS TV
	MEAN			MEAN	S.D.		MEAN				
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	30.264	1.538	34	305.30	1.46	-1.03	297.37	.96	52	438.	438.
.002	30.249	1.539	34	305.25	1.49	-1.05	297.35	. 35	52	uun.	442.
1.000	18.200	2.568	09	295.31	.84	.35	269.03	228	6:	¥39.	442.
2.000	12.043	2.338	28	290.52	.96	.40	282.59	3.15	-1.14	440.	442.
3.000	7.463	1.999	43	285.05	. <del>9</del> 5	.00	275.38	H.51	-1.69	438.	442.
4.000	4.836	1.567	33	279.13	.92	.18	269.17	5.38	-1.54	<b>437.</b>	442.
5.000	3.078	1.281	.03	273.33	.95	.41	262.85	6.35	95	435.	442.
6.000	1.622	.872	. 39	co7.67	دين . ا	. 23	255.10	0.01	57	420.	~~°€.
7.300	1.002	.547	.68	261.67	1.05	.05	2-9.02	6.68	39	414.	439.
8.000	.540	.306	.72	255.30	1.12	.50	2-2.32	5.29	15	400.	437.
9.000	.261	.152	.88	248.32	1.31	.66	235.05	5.70	.08	392.	435.
10.000	.119	.071	.98	240.60	1.43	.59	227.70	5.27	.:8	297.	426.
11.000	.047	.027	1.37	232.40	1.39	17	219.90	4.35	.40	280.	418.
12.000	.017	.009	1.53	224.00	1.38	41	212.26	3.48	.52	245.	411.
13.000	.006	.903	1.62	215.68	1.34	49	264.87	3.4:	.31	111.	394.
14.000	.002	.001	.88	207.75	1.38	32	196.27	3.04	29	40.	390.
15.000	.00:	.000	19	200.90	1.41	.07	190.95	1.95	48	8.	374.
16.006	<b>99</b> .999	<b>9</b> 9.992	999.99	196.40	1.64	.23	999.99	99.99	999.99	0.	263.
17.000	99.999	99.993	939.99	195.41	2.06	07	933.99	99.99	999.99	0.	262.
18.000	<b>9</b> 9.999	99.993	993.99	198.94	2.76	14	999.99	99.99	999.39	0.	263.
19.000	99.993	99.999	999.99	203.80	2.45	20	999.99	99.99	939.99	0.	253.
20.000	99.999	93.939	999.99	207.62	2.37	.00	999.99	99.99	999.99	0.	259.
21.000	99.999	99.999	999.99	210.66	2.32	Di	999.99	99.99	999.99	0.	243.
22.000	99.999	99.999	999.99	213.17	2.21	09	999.99	99.99	999.99	0.	₽43.
23.000	99.939	99.999	993.99	215.73	2.05	43	999.99	99.99	999.99	0.	237.
24.000	99.999	99.999	999.99	218.37	2.16	32	939.99	99.99	993.99	0.	241.
25.000	99.999	99.999	923.99	220.98	1.92	49	993.99	99.93	999.99	0.	241.
26.000	99.939	99.999	999.99	<i>223.5</i> 6	1.75	06	993.99	99.99	999.99	0.	236.
27.000	90.939	23.302	920.20	275.97	نعن د:	.50	999 99	99.99	999.99	0.	<b>211.</b>
28.000	99.999	99.939	599.99	228.02	1.96	.19	999.99	99.99	999.33	0.	209.
29.000	99.939	99.999	999.99	229.84	2.20	25	999.99	99.99	999.99	0.	182.
30.000	99.999	99.999	999.99	231.81	2.20	!9	999.99	99.99	999.99	0.	179.

Market Indiana Carachara Tanahara Tanahara Carachara Car

TABLE STATION	III. 11 • 913660	MOISTURE	RELATED S	TATISTICAL	PARAMETERS	. N	OVEMBER				
Z	VAPOR P	S.D. VP									
-	MEAN	3.U. YP	SKEH VP	TV	TV	SKEH TV	T TOWED	S.D. DPT	SKEH DPT	N085 T+P	NOSS TV
KM	MB	•••		MEAN	S.D.		HEAN				
.000	_	MB		DEG K	DEG K		DEG K	DEG K			
	29.953	1.707	29	305.19	1.55	84	297.19	.96	54	411.	411.
-002	29.926	1.716	29	395.17	1.55	84	297.18	.97	54	415.	415.
1.000	17.898	2.885	12	296.15	.95	28	288.72	5.62	65	414.	
2.000	11.552	2.805	61	290.57	1.05	19	281.76	4.32	-1.79	412.	416.
3.000	6.998	2.455	34	285.20	1.07	26	274.02	6.:2	-1.37	412. 405.	416.
500	4.327	1.821	.00	279.38	1.14	09	257.20	5.53	87		415.
5.000	2.577	1.356	.30	273.61	1.15	.24	259.95	7.69	54	397.	416.
6.000	1.452	.877	.67	267.82	1.19	16	252.80	7.77		396	∵:ō.
7.000	.810	.518	.89	261.73	1.22	06	2:6.28	7.1	30	386.	416.
8.000	.437	.281	1.07	255.31	1.29	.19	239.89	5.46	.02	377.	415.
9.000	.220	.179	1.17	240.32	1.10.	.19	233.03 233.29	5.40 5.77	.16	<i>5</i> 73.	415.
10.000	.098	.060	1.41	240.67	1.53	.35	226.02		. 30	370.	410.
1:.000	.039	.022	1.93	232.54	1.51	46	218.60	4.87	.57	294.	399.
12.000	.016	.008	1.88	224.25	1.49	99	211.45	3.92	.65	290.	39+.
13.000	.006	.003	1.02	216.04	1.53	-1.16		3.42	.56	259.	365.
14.000	-002	.001	1.83	208.09	1.54	-1.25	204.70	3.43	31	129.	370.
15.000	99.999	90.599	999.99	200.99	1.50		195.35	3.52	.13	32.	363.
16.000	99.999	99.399	999.99	195.48	1.38	92	999.99	99.99	999.99	4.	356.
17.860	99.999	99.999	999.99	192.63		.01	999.99	99.99	999.99	0.	264.
18.000	99.999	99.999	999.99	194.84	1.66	01	999.99	99.99	999.99	0.	262.
19.000	99.999	99.999	939.99		2.52	-09	993.99	99.99	999.99	0.	252.
20.000	99.999	99.999	999.99	201.59	2.54	26	999.99	99.99	999.99	0.	260.
21.000	99.999	99.999		205.49	2.35	33	939.99	99.99	999.93	0.	258.
22.000	99.999	99.999	999.99	10.602	2.22	34	999.99	93.99	999.99	0.	245.
23.000	99.999		999.99	13.515	2.13	!9	999.99	99.99	999.99	€.	243.
24.000	99.999	99.999	999.99	215.46	1.64	.06	999.99	99.99	999.99	0.	237.
25.000		99.999	999.99	218.24	2.05	.17	999.93	99.99	999.99	0.	242.
25.000	99.999	99.939	999.99	221.22	2.10	.23	999.99	99.99	999.99	0.	234.
	99.999	99.999	999.99	223.83	1.86	.33	999.99	99.99	999.99	0.	226.
27.000	99.929	99.999	999.99	226.31	2.16	.17	999.99	39.99	999.99	0.	208.
28.000	99.999	99.999	999.93	228.62	2.22	27	999.99	99.99	999.39	0.	207.
29.000	99.999	99.999	999.99	230.79	2.46	52	999.99	99.99	999.99	0.	163.
30.000	99.999	99.999	299.99	232.51	2.14	43	999.93	99.99	999.99	0. n	163.

TABLE	111. 12	MOISTURE	RELATED ST	ATISTICAL	PARAMETERS	. DE	CEMBER				
	= 913660	KHAJA	LEIN HISSLE	RANGE							
Z	VAPOR P	S.D. VP	SKEW VP	ŤΫ	ΤV	SKEW TV	DEWPT T	S.D. DPT	SKEU OPT	NOBS T+P	NOBS TV
	MEAN			MEAN	5.D.		MEAN	0.0.	DICER DI I	11003 177	14003 14
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	20.987	1.928	53	394.87	1.17	-1.10	296.64	1.13	74	410.	410.
.002	28.931	1.949	50	304.85	1.17	-1.09	296.61	1.14	70	421.	422.
1.000	17.068	3.092	14	295.56	1.15	.10	287.93	2.97	77	420.	422.
2.000	10.135	3.667	30	290.48	1.29	16	279.21	6.51	-1.22	412.	423.
3.000	5.835	2.971	.13	285.54	1.19	42	270.57	8.20	55	392.	423.
4.000	3.500	2.104	.52	279.93	1.21	.09	263.45	8.36	11	369.	423.
5.000	2.150	1.524	.80	274.17	1.26	.16	256.84	8.78	.18	367.	422.
5.00n	1.198	.910	1.12	268.35	1,29	.07	249.99	8.21	.39	363.	4ċ1.
7.000	.658	,493	1.39	262.26	1.30	.35	243.73	7.11	.58	356.	420.
8.000	.364	.260	1.54	255.81	1.28	.25	237.94	6.32	.53	354.	410.
9.000	. 192	.131	1.57	248.84	1.40	.39	231.94	5.65	.55	348.	397.
10.000	.C94	.063	1.73	241.22	1.46	.82	225.50	5.10	.62	303.	389.
11.000	.042	.027	2.12	233.14	1.38	.64	2:3.90	4.22	.78	233.	385.
12.000	.016	.009	2.06	224.85	1.26	.40	211.79	3.44	.89	259.	378.
13.000	.008	.003	1.53	216.60	1.26	.27	204.50	2.75	.41	158.	365.
:4.000	.002	.001	.79	208.44	1.35	.06	196.42	2.22	.00	27.	359.
15.000	99.999	99,999	999.99	200.95	1.32	.04	999.99	99.99	999.99	2.	356.
16.000	99.999	99.999	999.99	194.63	1.34	.00	999.99	93.99	999.99	ō.	270.
17.000	99.999	99.999	999.99	190.82	1.80	53	999.99	99.99	999.99	0.	265.
18.000	99,999	99.999	999.99	192.64	2.71	12	999.99	99.99	999 99	٥.	264.
19.000	99.999	99.999	939.99	199.78	2.64	26	999.99	99.99	999.99	0.	263.
20.000	99.999	99.999	999.98	205.48	2,46	44	999.99	99.99	999.99	0.	260.
21.900	99.999		999.99	209.51	2.12	42	999.99	39.99	999.99	0.	252.
22.000	99.999	99.999	999.99	212.74	2.12	39	999.99	99.99	999.99		250.
23.000	99.999	99.999	999.99	215.61	1.79	36	999.99	99.99	999.99	0.	243.
24.000	99.999	99.999	999.99	218.34	2.24	.08	944.99	<i>9</i> 9.99	999.99	0.	240.
25.000	99.999	99.999	999.99	220.72	2.14	.21	999.99	99.99	999.99	0.	240.
26.000	99.599	99.999	999.99	222.91	1.94	.28	999.99	99.99	999.99		228.
27.000	99.999	99.999	839.99	205.00	خ. بڌ	.öi	339.93	99.99	೮೫೨.೧೨	٤.	506
28.000	99.939	99.999	999.99	226.55	2.03	.24	999.99	99.99	939.39	0.	205.
29.000	99.999	99.999	999.99	228.29	2.08	08	999.99	99.99	999.99	0.	178.
30.000	99.999	99.999	993.99	230.18	1,96	-84	999.99	99.99	999.99	٥.	177.

TABLE	111. 13 = 913660		RELATED ST		PARAMETERS	. ANN	IUAL				
Z	VAPOR P	S.D. VP	SKEH VP	īV	TV	SKEW TV	DEWPT !	S D DPT	SKEW DPT	NORS TAR	NOBS TV
*	MEAN	3.0. 1.	Jilet II	MEAN	s.b.	511211	MEAN	3.0. Di i	SINCH OF I	14000 111	
KM	MB	MB		DEG K	DEG K		DEG K	DEG K			
.000	29.735	2.017	64	305.13	1.37	90	297.06	1.16	90	4944.	4944.
.002	29.693	2.031	63	305.10	1.37	90	297.04	1.17	89	5026.	5033.
1.000	17.345	2.795	-,15	295 79	1.08	40	288.23	2.62	70	5019.	5038.
2.000	10.896	3.123	67	290,39	1.12	26	280.66	5.34	-1.80	4958.	5039.
3.000	6.541	2.51.2	35	285.20	1.09	.09	272.81	6.89	-1.21	48:9.	5038.
4.000	4.110	1.857	07	279.42	1.15	.45	266.24	7.37	87	4723.	5036.
5.000	2.555	1.362	.28	273.66	1.20	.61	259.82	7,77	53	4682.	5035.
5.000	1.480	.871	.61	267.94	1.23	.45	253.11	1.59	~.60	408J.	5021.
7.000	.806	.498	.92	261.90	1.25	.4ê	246.35	6.90	.00	4495.	4998.
8.000	.425	.267	1.16	255.49	1.30	.43	239.74	6.21	.18	4384.	4925.
9.000	.115	.129	1.35	248.49	1.45	.55	233.06	5.38	.38	4274.	4822.
10.000	.095	.057	1.60	240.81	1.52	.69	225.98	4.64	.49	3220.	4693.
11.000	.030	.037	2.05	232.68	1 53	.39	218.80	3.78	.74	3146.	4€27.
12.000	.015	.007	2.11	224.29	1.44	06	211.47	3.02	.70	2621.	4527.
13.000	.015	.003	1.61	216.00	1.48	07	204.54	2.92	01	1269.	4406.
14.000	.002	.001	1.29	207.99	1.49	11	196.18	2.81	20	327.	4316.
15.000	99.999	99.999	999.99	200.91	1.42	08	999.99	99.93	589.59	66.	4246.
16.000	99.939	99.999	999.99	195.88	1.82	.19	999.99	99.99	399.99	C.	3198.
17.000	99.999	99.939	999.99	193.96	3.35	.25	999.99	99.99	993.99	0.	3157.
17.000	99.999	99.999	999.99	195.76	4.67	.00	939.99	99.99	999.99	0.	3151.
19.000	99.999	99.999	999.99	202.40	3.60	14	999.93	99.99	999.99	0.	3122.
20.000	99.999	99.999	999.99	206.98	2.82	22	999.93	99.99	999.99	0.	3079
21.000	99.999	99.999	999.99	210.59	2.41	25	999.99	99.99	999.99	0.	2943.
55,000	99.999	99.939	999.99	213.32	5.22	17	999.99	99.99	993.99	0.	2933.
23.000	99.999	99.599	999.99	215.95	1.25	09	999.99	99.39	999.99	o.	2837.
24.000	99.999	99.999	999.99	218.50	2.25	01	929.99	57.88	999.99	Õ.	2850.
25.000	99.999	99.999	999.99	220.88	2.27	20	999.99	99.99	999.99	Ö.	2806.
26.000	99.999	99.939	993.99	223.16	2.16	25	999.99	99.93	999.99	o.	2683.
27.000	99.599	99.939	535.85 539.95	225.33	2.32	:4	503.53	00.00	000 00	o.	2785
28.000	99.999	99.999	999.39	227.33	2.31	25	999.99	99.99	999.39	õ.	2358.
29.000	99,999	99.999	999.99	229.21	2.49	6.5	999.99	99.99	999.99	0.	2026.
30.000	99.999	99.999	999.99	231.01	2.39	26	999.99	99.99	999.99	õ.	2002.

■ 1000 Part 1

	•••	4800004		ATHOCOL COC	IANUADY
TABLE	IV.1		LEIN MISSL	ATMOSPHERE.	JANUARY
	= 913660	P	D הדינו שו 1920	E RANGE TV	
Z KM	GEO. HT.	MB	G/H3	DEG K	
.000	.000	1010.1000		304.50	
.000	.002	1009.8000		304.55	
1.000	.997		1065.0000	294.75	
2.000	. 1.994	802.3600	964.0000	289.95	
3.000	2.991	712.8200	869.6000	285.58	
4.000	3.987	631.9900	786.2000	280.04	
5.000	4.983	558.9800	709.9000	274.29	
6.000	5.979	493.1300	639.8000	268.49	
7.000	6.974	433.8300	575.9000	262.41	
8.000	7.969	380.5100	517.7000	256.06	
9.000	8.964	332.6100	465.1000	249.11	
13.00C	9.959	289.5900	417.9000	241.43	
11.000	10.953	250.9800	374.7000	233.33	
12.000	11.947	216.4200	335.2000	224.93	
13.000	12.940	185.5900	298.3000	216.74	
14.000	13.933	158.2200	264.2000	208.61	
15.000	14.926	134.0700	232.3000	201.01	
16.000	15.919	112.9400	202.4000	194.38	
17.000	16.911	94.6980	173.1000	190.53	
18.000	17.903	79.3280	143.8000	192.16	
19.000	18.895	66.7150	116.7000	199.15	
20.000	19.886	56.4130	96.0300	204.65	
21.000	20.877	47.8880	79.9500	208.66	
22.000	21.868	40.7670	67.0500	211.81	
23.000	22.858	34.7940	56.4800	214.53	
24.005	23.848	29.7370	47.7300	217.03	
25.000	24.838	25.4650	40.5100	218.98	
26.000	25.827	21.8390	34.4000	221.16	
27.000	25.817	18.7580	29.2600	223.33	
29.000	27.805	16.1350	24.9700	225.13	
29 000	28.794		21.3300	226.93	
30.000	29.792			228.90	
35.000	31.757			es2.37	
34.000	33.732		9.8050	236.97	
36.000	35.705		7.2530	241.77	
38.000	37.676		5.3750	247.76	
40.000	39.647		4.0190	253.26	
42.000	41.616			257.39	
44.000	43.584			262.12	
46.000	45.551	1.3521	1.7550	265.82	
48.000	47.517			270.54	
50.008	49.481	.8223		271.96	
52.000	51.444			271.71	
54.000	53.406			270.23 267.35	
56.000	55.367		.5065 .3976	264.81	
58.000 60.003	57.326 59.284			261.86	
62.000	61.241			258.76	
64.000	63.197			254.75	
66.000	65.158			248.80	
68.000	67.105			245.39	
70.300	69.057			246.83	
	02.007				

The Artist Control of Control o

TABLE	ıv. 2	HYDROST	ATIC MODEL	ATMOSPHERE.	FEBRUARY
	= 913660	KHAJ	ALEIN MISSL	E RANGE	
Z	GEO. HT.	P	D	TV	
KM	KM	MB	G/M3	DEG K	
.000	.000	1010.4000	1154.0000	304.89	
.002	.002	1010.2000	1154.0000	304.86	
1.000	.997		1056.0000	294.67	
2.000	1.994	802.6600	954.0000	290.05	
3.000	2.991	713.1000	870.1000	285.52	
4.000	3.987	632.2200	786.5000	280.03	
5.000	4.983	559.1900	710.0000	274.36	
6.000	5.979	493.3300	639.9000	268.56	
7.000	6.974	434.0300	575.9000	262.5%	
8.000	7.969	380.7100	517.8000	256.15	
9,000	8.964	332.8000	465.2000	249.23	
10.000	9.959	289.7700	417.9000		
11.000	10.953	251.1500	374.9000	241.53	
12.700	11.947			233.35	
13.000	12.940	216.5700	335.4000	224.97	
14.000		185.7200	298.5000	216.77	
15.000	13.933	158.3400	264.3000	208.71	
	14.926	134.1900	232.3000	201.20	
16.000	15.919	113.0700	202.1000	194.94	
17.000	16.911	94.6560	172.8000	191.26	
18.000	17.903	79.5220	143.6000	192.88	
19.000	18.895	66.9050	116.9000	199.33	
20.000	19.885	56.5760	96.3400	204.59	
21.000	20.877	48.0240	80.2100	208.57	
22.000	21.868	40.8860	67.1400	212.13	
23.000	22.858	34.8960	56.5460	215.01	
24.000	23.848	29.8460	47.7500	217.75	
25.000	24.838	25.5720	40.5200	219.84	-
26.000	25.827	21.9430	34.4500	221.90	
27.600	20.817	18.6200	54.5400	223.8 <i>!</i>	
28.000	27.805	16.2260	25.0300	225.81	
29.000	28.794	13.9800	21.3900	227.67	
30.000	29.782	12.0619	18.2900	229.75	
32.000	31.757	9.0206	13.2700	234.70	
34.000	33.732	6.7851	9.7910	239.38	
36.000	35.705	5.1393	7.2276	245.60	
38.000 .	37.676	3.9209	5.3720	252.17	
40.000	39.647	3.0113	4.0290	258.11	
42.000	41.616	2.3262	3.054C	263.63	
44.000	43.58	1.8058	2.3270	268.00	
46.000	45.551	1.4080	1.7870	272.04	
48.000	47.517	1.1012	1.3860	274.44	
50.000	49.481	.8625	1.0830	274.96	
52.000	51.444	.6752	.8543	272.94	
54.000	53.406	.5275	.6753	269.73	
56.000	55.357	-4108	.5328	25.25	
58.000	57.326	.3188	.4203	261.94	
60.000	59.284	-2465	.3302	257.72	
62.000	61.241	. 1900	.2566	255.65	
64.000	63.197	. 1461	.1992	253, 19	
65.000	65.152	.1121	.1538	251 81	
68.000	67.105	.0850	.1183	251.09	
70.000	69.057	.0561	.0893	255.53	

TABLE	IV. 3			ATMOSPHERE,	
	= 913660		ATEIN WISST		
Z	GEO. HT.	P	D	TV	
KM	KM and	MB	G/M3	DEG K	
.000	.000		1154.0000	305.19	
.002	.002		1154.0000	305.17	
1.000	.997		1065.0000	295.21	
2.000	1.994	803.3500	965.0000	290.01	
3.000	2.991	713.6700	871.6000	265.23	
4.000	3.987	632.6400	788.1000	279.65	
5.000	4.983	559.4700	711.2000	274.05	
6.000	5.979	493.5300	640.5000	268.44	
7.000	6.974	434.1800	576.4000	262.40	
8.000	7.969	380.8200	518.1000	256.07	
9.000	3.954	332.8800	465,6000	249.00	
10.000	9.959	289.8200	418.2000	241.45	
11.000	10.953	251.1800	375.1000	233.28	
12.000	11.947	216.5800	335.5000	224.87	
13.000	12.940	185.7200	298.6000	216.69	
14.000	13.933	158.3300	264.4000	208.63	
15.000	14.926	134.1700	232.3000	201.20	
16.000	15.919	113.0700	201.9000	195.04	
17.000	16.911	94.8780	172.6000	191.54	
18.000	17.903	79.5560	143.4000	193.26	
19.000	18.895	66.9590	116.8000	199.78	
20.000	19.886	55.6450	96.2000	205.14	
21.000	20.877	48.1100	80.0000	209.49	
22.000	21.868	40.9880	67.0300	213.03	
23.000	22.858	35.0050	56.5000	215.85	
24.000	23.848	29.9550	47.8000	218.33	
25.000	24.838	25.6770	40.5600	220.55	
26.000	25.827	22.0450	34.4800	222.75	
27.000	26.817	18.9550	29.3700	224.82	
28.000 29.000	27.805	16.3220	25.0600	225.87	
	28.794	14.0750	21.4000	229.08	
30.000 32.000	29.782	12.1551 9.1027	18.3100	231.22	
34.000	31.757 33.732		13.3100	235.41	
36.000	35.73E	6.8559 5.1982	9.8100	240.64	
38.000	37.676	3.9705	7.2660 5.3930	246.35 253.48	
40.000		3.0559			•
42.000	39.647 41.616	2.3674	4.0330 3.0630	260.88	
44.000	43.584	1.8421	2.3500	265.08 269.85	
46.000	45.551	1.4377			
48.000	47.517	1.1245	1.8170	272.43	
50.000				274.18	
52.000	49.481 51.444	.8799 .6875	1.1100	272.89	
			.8742	270.75	
54.000 56.000	53.406	.5361	.6887	267.96	
55.000 59.000	55.367 57.336	.4168	.5422	264.68	
58.000 60.000	57.326	.3232	.4253	261.66	
	59.284	.2500	.3327	258.67	
62.000 64.000	61.241	. 1927	.2601	255.00	
	63.197	. 1480	.2027	251.29	
66.000 68.000	65.152	.1134	. 1554	251.25	
	67.105	.0869	.1.48	249.87	
70.000	69.057	.0655	.0920	248.97	

MARCH

TABLE	IV. 4	HYDROST			
	= 913560	_KHAJ.	alein missl	.E RANGE	
Z	ŒO. HT.	P	D	TV	
KH	KM	MB	G/M3	DEG K	
.000	.000	1010.9000	1154.0000	305.07	
.002	.002	1010.7000	1154.0000	305.05	
1.000	-997	902.5400	1063.0000	295.70	
2.000	1.994	803.5000	954.0000	290.36	
3.000	2.991	713.8300	872.3000	285.07	
4.000	3,937	632.7100	799.2000		
5.000	4 983	559.4400	712.3000	279.30	
6.000	5.579	493.4000		273.61	
7.000	6.974	433.9900	641.3000	268.02	
8.000	7.969		577.2000	261.94	
9.000		380.5500	518.5000	255.62	
_	8.964	332.5700	465.8000	248.72	
10.000	9.959	289.4900	418.4000	241.02	
11.000	10.953	250.8300	375.3000	232.66	
12.000	11.947	216.2200	335.5000	224.48	
13.000	12.940	185.3500	298.7000	216.16	
14.000	13.933	157.9500	264.4000	208.13	
15.000	14.926	133.8200	231.9000	201.01	
16.000	15.919	112.7800	200.9000	195.53	
17.000	16.911	94.7010	171.4000	192.50	
18.000	17.903	79.4810	142.5000	194.34	
19.000	18.895	66.9540	116.2000	200.71	
20.000	19.886	56.6920	95.5900	206.39	
21.000	20.877	48.1940	79.7200		
22.000	21.868	41.0890	66.9500	210.60	
23.000	22.858	35.1100		213.81	
24.000	23.848	30.0600	56.4990	216.53	
25.000	24.838	25.7820	47.8000	219.07	
26.000	25.827		40.5500	221.50	
27.000	20.317	22.1520	34.4600	223.95	
28.000		10.0000	23.3,00	225.33	
29.000	27.805	16.4310	25.0800	558.51	
30.000	28.794	14.1800	21.4700	230.11	
	29.782	12.2534	18.3900	232.16	
32.000	31.757	9.1873	13.3900	236.41	
34.000	33.732	6.9277	9.8820	241.59	
36.000	35.705	5.2603	7.3090	248.01	
38.000	37.676	4.0263	5.4250	255.74	
40.000	39.647	3.1036	4.0830	261.65	
42.000	41.616	2.4054	3.1130	266.25	
44.000	43.584	1.8710	2.3970	268.98	
46.000	45.551	1.4583	1.8570	270.61	
48.000	47.517	1.1383	1.4450	271.54	
50.000	49:481	.8891	1.1300	271.22	
52.000	51.444	-6937	.8874	269.38	
54.000	53.406	.5404	-6963		
55.000	55.367	-4201		267.42	
58.00C	57.326	.3755	.5473	264.49	
60.000	59.284	.2511	.4312	250.12	
000.58	51.241		.3391	2F5.10	
64.000	63.197	. 1922	.2700	245.26	
66.000		- 1'+59	.2096	239.90	
68.000	65.152	.1102	.1611	235.59	
70.000	67.105	.0830	.1214	235.60	
,0.000	69.057	. 3631	.0866	251.16	

APRIL

TABLE IV. 5 STATION = 913660		HYDROST/			
2 GEO. HT.		P	D	tv	
KM	KM	MB	G/H3	DEG K	
.000	.000	1010.6000		305.20	
.002	500.	1010.6000	1154.0000	305.19	
1.000	.997	902.5000	1062.0000	295.14	
2.000	1.994	803.5900	953.0000	290.70	
3.000	2.991	713.9700	872.0000	285.24	
4.000	3.987	632.8700	789.4000	279.29	
5.000	4.983	559.5600	712.7000	273.52	
6.000	5.979	493.4800	641.9000	267.81	
7.000	6.974	434.0000	577.5000	261.78	
8.600	7.959	380.5400	519.0000	255.43	
9.000	A 964	332.5100	466.4000	548 30	
10.000	9.959	289.3900	418.8000	240.73	
11.000	10.953	250.7100	375.4000	232.66	
12.000	11.947	216.0900	335.5000	224.34	
	12.970	185.2200	298.5000	216.08	
13.000	13.933	157.8400			
14.000	14.926	133.7200	264.2000 231.7000	208.10	
15.000 16.000	15.919	112.7300	200.3000	201.06 135.07	
17.000	16.911	94.7500		194.12	
18.000	17.903	79.8610	170.0000 141.1000	196.62	
19.000	18.695	67.2160	115.8000	202.24	
		55.9690	95.7500	207.27	
20.000	19.885				
21.000	20.877	46.+570 41.3250	. 79.9600 67.2600	211.13	
23.000	21.869 22.858	35.3:60	56.7800	214.03 216.67	
	23.848		48.0500	219.26	
24.000 25.000	24.838	30.2400 25.9420	40.7300	221.90	
26.000	25.827	22.2950	34.6200	224.34	
	26.817	19.1920	29.5100	226.58	
27.000 28.000	27.805	16.5450	25.2000	228.58	
29.000	28.794	14.2820	-21.5700	230.68	
30.000		12.3454	18.4900	232.58	
36.000	29.782 31.757	9.2t16	13.55U	ಕೂರ. ಇದ	
34.000	33.732	6.9831		240.95	
36.000		-	10.0300		
38.000	35.705 37.676	5.2939 4.0385	7.4560 5.5530	245.80 251.72	
40.000	39.647	3.1016	4.1540	258.45	
42.000	41.616			262.93	
		2.3961	3.1560		
44.000	43.584	1.8590	2.4110	266.94	
46.000	45.551	1.4463	1.8550	268.46 260.05	
48.000	47.517	1.1254	1.4500	268.95	
50.000	49.481	.8772	1.1340	267.81	
52.000	51.444	.6825	.8858	266.71	
54.000	53.406	.5301	.6958	263.71	
56.000	55.367	.4197	.5439	261.37	
58.000	57.326	.3174	.4255	259.13	
60.000	59.284	.2443	.3343	252.92	
62.000	61.241	. 1871	.2605	248.61	
64.000	63.197	.1427	.2025	243.90	
66.000 69.000	65.152	.1084	.1551	241.90 243.66	
58.000	67.105	.0923	.1174	242.66	
70.000	69.057	.0626	.0887	244.23	

and the contraction of the contr

TABLE	IV. 7 = 913660		TIC MODEL	ATMOSPHERE.	
Z	GEO. HT.	P	ם בכנות וווים	tv	
KM	KM	119 -	G/M3	DEG K	
.000		1010.3000		305.20	
.002		1010.0000		305.19	
	.997		1051.0000	295.24	
1.000 2.000	1.994	803.19 0	953.0000	290.55	
				285.03	
3.000	2.991 3.997	713.5700 632.4500	872.1000 789.4000	279.10	
4.000					
5.000	4.583	559.1500	712.7000	273.32 267.62	
6.000	5.979	493.0700 433.6000	577.5000	261.56	
7.000	6.974		-		
8.000	7.959	380.1300 332.0900	519.2000	255.07 247.99	
9.000	8.964		465.5000	240.26	
10.000	9.959	268.9500 259.2500	419.0000	232.15	
11.000	10.953 11.947	215.6100	375.5000 335.8000	223.67	
12.000 13.000	12.940		296.8000	215.34	
-		184.7200			
14.000	13.933	157.3200		207.32	
15.000	14.925 15.919	112.3100	231.4000 193.8900	200.5+ 195.8+	
16.000					
17.000	16.911	94.5690	166.9000	197.39	
18.000	17.903	79.8180	137.5000	202.23	
19.000	18.895	67.6240	114.1000	205.44	
20.000	19.896	57.4700	95.4100	209.84	
21.000	20.877	48.9550	80.2800	212.45	
22.000	21.858	41.7830	67.8100	214.64	
23.000	22.858	35.7160	57.3700	2:5.89	
24.000	8+9.55	30.5840	48.6:00	219.19	
25.000	24.838	26.2340	41.2400	221.58	
26.500	25.827	22.5390	35.0900	223.77	
27.000	26.817	19.3930	29.9200	225.76	
28.000	27.805	16.7080	25.5700	227.66	
29.000	28.794	14.4120	21.9000	229.26	
39.000	29.782	12.4443	18.8900	230.58	
32.030	31.757	9.3600	13.7760	دعة. أنَّ عمر حج	
34.000	33.732	6.9801	10.1800	235.65	
36.000	35.705	5.2541	7.5340	241.12	
38.000	37.676	3.9972	5.5520	248.00	
40.003	39.647	3.0558	4.1510	253.45	
42.000	41.616		3.1350	258.61	
44.000	43.594	1.8160	2.3810	263.20	
46.000	45.551	1.4080	1.8340	254.97	
48.000	47.517	1.6935	1.4170	265.38	
50.000	49.481	.8503	1.0930	267.60	
52.000	51.444	.6611	.6578	255.94	
54.000	53.406	.5136	.6689	264.91	
56.000	55.357		.5257	261.32	
58.000	57.326		.4120	257.65	
60.000	59.284	.2358	.3222	253.51	
62.000	61.241	. 1914	.2518	248.53	
64.000	63.197			239.98	
66.000	65.152		.1533	234.40	
58.000	67.105			243.91	
70.000	69.057	.9601	.0933	249.16	

JULY

TABLE	IV. 8 = 913660		ATIC HODEL		AUGUST
Z	GEO. HT.	P			
KH	KM	•	0	TV	
		1910 2000	G/M3	DEG K	
.000		1010.7000		305.31	
-002		1010.5000		305.30	
1.000	.997		1051.0000	236.21	
2.000	1.994	803.5000	953.8000	290.43	
3.000	2.991	713.8100	872.8000	294.93	
4.000	3.987	632.6400	793.0000	278.99	
2. CÛÛ	n 001	<b>ਦੰਦਰ 52</b> 00	איניצ בנינה	13. 24خ	
6.000	5.979	493.1300	642-4000	267.42	
7.000	6.974	433.6200	577.9000	261.39	
8-000	7.959	380.1200	519.5000	254.92	
9.000	8.964	332.0500	465.2000	247.81	
10.000	9.959	288.890	419.2000	240.05	
11.000	10.953	250.1600	375.90CD	231.92	
15-000	11.947	215.5000	335.0000	223.45	
13.000	12.940	164.6000	299.0000	215.06	
14.000	13.933	157.1890	264.5000	207.02	
15.000	14.926	133.0900	231.2000	200.50	
16.000	15.919	112.2300	197.9000	197.59	
17.COD	15.911	94.5720	166.0000	193.44	
18.000	17.903	79.8720	137.2000	<b>2</b> 02.77	
19.000	18.835	67-6890	114.1000	205.51	
20_000	19.695	57.5200	95.6500	209.47	
21.030	20.877	49.9620	89.5100	211.96	
22.000	21.858	41.7880	67.9500	214.20	
23.000	22.658	35.7100	57.5000	216.37	
24.000	23.848	30.5650	48.7300	219.54	
25.000	24.838	26.2060	41.3400	220.83	
26.000	25.827	ēē.5030	35.1600	222.94	
27.000	₹b.81 /	19.5510	29.9530	æ5.cs	
28.000	27.805	16.6650	25.5800	227.00	
29.000	28.794	14.3590	21.6500	228.73	
30.000	29.782	12.4028	19.7900	230.00	
32.000	31.757	9.2640	13.6900	232.45	
34.000	33.732	5.9479	10.08CD	235.59	
36.000	35.705	5.2+17	7.4420	241.78	
38.000	37.676	3.9629	5.5000	249.56	
40.000	39.647	3.0-86	4.1010	255.17	
42.000	41.616	2.3494	3.0970	251.27	
44_CCD	43.584	1.6252	2.3520	265.59	
45.000	45.551	1-4153	1.8090	268.51	
48.000	47.517	1-1031	1.4090	275.53	
50_00n	49.481	.6505	1.0950	269. <i>5</i> 7	
52.000	51.444	.6702	.9517	255.94	
54.000	53.405	.5209	.6747	254.98	
56.000	55.357	.4042	.5257	263.42	
58.000	57.326	.3132	.4112	251.41	
60.000	53.264	.3152	.3236	256.60	
62.000	61.241	.1859	.æ∞. €+35.	250.85 250.85	
64.GCD	63.197	. 1422	.1972	247.43	
56.000	EE .:52	.1085	1512	245.15	
68.000	67. 05	.0828	.1143	248.64	
70.000	69.057	.0634	.0959	250.52	

TABLE	IV. 9	HYDROST	ATIC HOOEL	ATMOSPHERE'.	SEPTEMBER
	= 913660		LEIN MISSL		<b>33. 3</b>
Z	Œ0. 4T.	P	D	TV	
KM	KM	119	G/H3	DEG K	
.000		1010.4000		305.40	
-002		1010.2000		305.38	
1.000	.937		1051.0000	295.37	
2.000	1.994	803.3700	953.4000	290.51	
3.000	2.991	713.7200	872.4000	285.00	
4.000	3.997	632.5800	789.7000	279.05	
5.000	4.983	559.2500	712.9000	273.29	
5.000	5.975	493.1400	642.0000	257.58	
7.000	6.974	433.6700	577.5000	261.59	
8.000	7.959	390.2100	518.9000	255.23	
9.000	A.964	332.1900	466.3000	248.1R	
10.000	9.359	289.0700	418.7000	240.52	
11.000	10.953	250.4000	375.3000	232.42	
12.000	11.347	215.7800	335.7000	223.93	
13.000	12.940	184.8900	293.9060	215.50	
14.000	12.933	157.4600	264.5000	207.44	
15.000	14.926	133.3600	231.5000	208.69	
16.000	15 5'9	112.4600	193.9000	197.09	
17.000	16.911	94.6940	157.3900	197.21	
18.C00	17.903	79.8830	139.2000	201.41	
19.000	18.635	67.6360	114.6909	265.57	
20.000	19.825	57.4350	95.6500	208.75	
21.000	20.877	48.6850	<b>60.2800</b>	211.33	
22.000	839.15	41.6930	58.0400	213.41	•
23.000	22.958	35.6350	57.4400	215.95	
24.000	23.849	30.4720	48.5700	218.57	
25.000	24.839	25.1240	41.2200	220.78	
25.000	25.827	22.4320	35.0500	555.81	
27.000	25.8:7	19.2910	29.2530	225.06	
28.000	27.835	16.6140	25.4600	227.30	
29.000	28.794	14.3290	21.7800	229.21	
30.000	29.782	12.3738	18.5700	230.92	
32.000	31.757	9.256	13.5100	255.73	
34.000	33.732	6.9778	9.9340	239.96	
36.000	35.705	5.2869	7.3920	245.83	
38.000	37.676	4.0343	5.4960	252.22	
40.000	39.647	3.0595	4.1170	258.70	
42.000	41.616	2.3959	•	26+.59 ~~	
44.000	43.584	1.8629	2.3810	269.82	•
46.000	45.551	1.4516		270.05	
48.000	47.517	1.1319		269.82	
50.000	49.481	.8928	1.1230	270.07	
52.000	51.444	.6885		259.41	
54.000 56.000	53.405	.5357	.6958 5792	268.92 366 37	
55.000 58.000	55.357 57.326	.4178 .3244		265.27 363.59	
60.000	59.2 <del>8</del> 4	.3244	.4245 .3334	≥62.50 ≥59.61	
62.000	61.241	.1932		252.24	
54.COO	63.197	.1930		245.40	
66.000	65.152			2+2.87	
58.COO	67.105			245.33	
70.000	59.057			247.23	

TABLE STATION	IV. 10 = 913660	HYDROSTATIC HODEL ATMOSPHERE, KHAJALEIN HISSLE RANGE			
Z	ŒO. HT.	P	D	TV	
101	KM	19	G/H3	DEG K	
.000		1010.3000		305.30	
.002		1010 1000			
1.000	.937		1051.0000	305.26	
2.000	1.994	903.2400		296.31	
3.000	2.991		953.2000	290.52	
4.000	3.987	713.6200	872.1000	285.05	
5.000	4.983	532.5000	789.4000	279.13	
6.000	5.979	559.1900	712-7000	273.33	
7.000	6.974	493.1100	641.8300	267.67	
8.000		433.6600	577.3500	261.57	
9.000	7.969	380.2100	518.8000	255.30	
13.000	8.964	332.2:00	465.1000	249.32	
	9.959	289.1100	418.5000	240.60	
11.000	10.953	250.4300	375.4000	232.40	
	11.947	215.8100	335-6000	224.00	
13.000	12.940	184.9400	293.7000	215.68	
14.000	13.933	157.5500	264.2000	207.75	
15.000	14.926	133.4500	23:.4000	200.93	
15.000	15.919	112.5100	199.6000	195.40	
17.000	16.911	94.6330	169.7000	195.41	
18.000	17.903	79.6990	139.5000	198.94	
13.000	18.895	<b>67.3500</b>	115.1000	203.80	
20.000	19.885	57.1270	95.5500	207.52	
21.000	20.877	49.5890	80.3590	210.66	
22.000	21.863	41.4160	57-6900	213.17	
23.600	22.859	35.3710	57.1230	215.73	
24.000	23.648	30.2670	48.2900	219.37	
25.000	24.939	25.9490	40.9100	220. <del>9</del> 9	
25.000	25.827	22.262 <b>3</b>	34.7300	223.56	
27.836	25.d:7	19.1770	೭೪.೮೮೮	ēċs.ši	
28.000	27.805	16.5≥50	25.2500	228.02	
29.000	28.794	14.2590	21.6100	229.84	
30.999	29.782	12.3:93	18.5100	231.81	
32.000	31.757	9.2391	13.5100	237.18	
34.000	33.732	6.9721	9.9660	242.13	
36.000	35.705	5.2965	7.3970	248.29	
38.000	37.576	4.0534	5.5080	255.19	
40.COO	39.547	3.1210	4-1630	259.93	
42.090	41.616	2.4152	3.1620	264.86	
44.000	43.584	1.8758	2.4350	257.14	
45.000	45.551	1.4597	1.6930	268.77	
48.COD	47.517	1.1392	1-4550	271.09	
50.000	49.481	.8891	1.1320	272.34	
52.000	51.444	.6946	.0009	270.94	
54.000	53.435	.5415	-7017	267.58	
56.000	55.357	.4210	.5521	254.35	
58.000	57.326	.3262	.4343	260.40	
60.000	59.234	.2518	-3401	256.74	
62.000	61.241	. 1937	.2557	252.78	
64.000	63.197	. 1484	-2054	243.42	
55,000	85.152	.1135	.1556	\$10.15	
69.000	67.105	.0968	-1205	249.72	
70.000	69.057	.0554	-0927	248.43	

OCTOBER

TABLE	IV. 11	HYDROSTATIC MODEL ATMUSPHERE,					
STATION	= 913660		MEIN ÄISEN				
Z	GEO. HT.	P	D	TV			
KM	KM	MB	G/M3	DEG K			
.000	.000	1010.0000	1153.0000	305.19			
.002	.002	1009.7000	1153.0000	305.17			
1.000	.997	901.7500	1061.0000	295.15			
2.000	1.994	802.9100	962.6000	290.57			
3.000	2.991	713.3500	871.3000	285.20			
4.000	3.987	632.3200	788.5000	279.38			
5.000	4.983	557.1000	711.8000	273.61			
<b>3.000</b>	5.979	493.0800	641.4000	267.82			
7.000	6.974	433.6500	577.2000	261.73			
8.000	7.969	380.2100	518.8000	255.31			
9.000	8.054	332 2100	<u>ዛ</u> ሮድ ነቦበበ	248.32			
10.000	9.959	289.1100	418.5000	240.67			
11.000	10.953	250.4600	375.2000	232.54			
12.000	11.947	215.8600	335.3000	224.25			
13.000	12.940	185.0200	298.3000	216.04			
14.000	13.933	157.6600	263.9000	208.09			
15.000	14.926	133.5700	231.5000	200.99			
16.000	15.919	112.5700	200.6000	195.48			
17.000	16.911	94.5250	170.9000	192.63			
18.000	17.903	79.3560	141.9000	194.84			
13.000	18.895	66.8880	115.6000	201.59			
20.000	19.886	56.6590	95.5900	206.49			
21.000	20.877	48.1550	79.9200	209.91			
22.000	21.858	41.0270	67.2200	212.61			
23.000	22.858	35.0280	56.6300	215.46			
24.000	23.848	29.9590	47.8400	218.24			
25.000	24.838	25.6950	40.4600	221.22			
26.000	25.827	22.0730	34.3500	223.83			
27.000	26.817	18.9960	29.2400	226.31			
28.000	27.805	16.3740	24.9500	228.62			
29.000	28.794	14.1360	21.3400	230.79			
30.000	29 782	12.2194	18.3100	232.51			
32.000	31.757	9.1633	13.4100	236.33			
34.000	33.732	6.9055	9.9240	240.67			
36.000	35.705	5.2366	. 7.3440	246.61			
38.000	37.676	3.9982	5.4760	252.50			
40.000	39.647	3.0686	4.1390	256.39			
42.000	41.616	2.3673	3.1240	262.06			
44.000	43.584	1.8343	2.3930	265.07			
46.000			1.8340	268.96			
	45.551	1.4262					
48.000	47.517	1.1117	1.4220	279.35			
50.000	49.481	.8669	1.1140	269.14			
52.000	51.444	.6750	.8752	255.69			
54.000	53.406	.5243	.6871	263.86			
56.000	55.367	.4061	.5388	260.63			
58.000	57.326	.3136	.4219	257.01			
60.000	59.284	.2413		253.91			
62.000	61.241	. 1850	.2564	249.51			
34.000	63.197	. 1412	.1994	244.93			
66.000	65.152			244.10			
68.000	67.105			247.76			
70.000	69.057	.0627	.6365	250.49			

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69.057

262.99

TABLE	IV. 13		TIC MODEL A		ANNUAL
STATION			TEIN WISST		
	GEO.HT.	P MB	D G/H3	TV DEG K	
KM		1010.4000		305.13	•
.000	200.	1010.7000		305.10	
1.000	.997		1062.0000	295.79	
2.000	1.994	803.1500	963.5000	290.39	
3.000	2.991	713.5400	271.6000	285.20	
4.000	3.907	632.4900	788.6000	279.42	
5.000	4.983	559 2500	711,9000	277 FF	
6.000	5.979	493.2400	641.3000	267.94	
7.000	6.974	433.6200	577.1000	261.90	
8.000	7.969	380.4000	518.7000	255.49	
9.000	9.964	332.4100	466.0000	248.49	
10.000	9.959	289.3100	418.5000	240.81	
11.000	10.953	250.6500	375.3000	232.68	
12.000	11.947	216.0400	335.5000	624.29	
13.000	12.940	185.1700	238.6000	216.00	
14.000	13.933	157.7800	264.3000	207.93	
15.000	14.926	133.6600	231.8000	10.005	
16.000	15.919	112.6600	200.4000	195.88	
17.000	16.911	94.6750	170.0000	193.96	
18.000	17.903	79.E380	140.5000	196.76	
19.000	18.895	E7 1710	115.5030	202.40	
20.000	19.886	56.9230	95.8200	200.98	
21.000	20.877	48.4000	80.1100	210.49	
22.000	2858	41.2530	67.3800	213.32	•
23.000	22.858	35.2420	56.8500	215.95	
24.000	23.848	30.1600	48.0900	218.50	
25.000	24.838	25.8580	40.7800	220.89	
26.000	25.827	22.2060	34.6600	223.16	
27.000	23.817	19.1000	29.5300	225.36	
28.000	27.805	16.4520	25.2100	227.33	
29.000	28.794	14.1890	21.5700	229.21	•
30.000	29.782	12.2532	19.4800	231.01	
32.000	31.757	9,1724	13.4800	234.95	
34.000	33.732	6.9015	9.9560	239.42	
36.000	35.705 37.676	5.2247 3.9830	7.3680 5.4730	244.91 251.32	
Z8.000	39.647	3.0561	4.1050	257.08	
40.000 42.000	41.616			262.24	
44.000	43.584	1.8288		265.28	
46.000	45.551	1.4226		268.80	
48.000	47.517	1.1083		270.42	
50.000	49.481	.8653		270.37	
52.000	51.444			268.80	•
54.000	53.406			<del>2</del> 66.75	
56.000	55.367			264.03	
58.000	57.326			260.81	
50.000	59.284	.2442	.3222	256.90	
62.000	61.241	.1978		252.26	
64.000	63.197			247.58	
CS.000	65 153			241.01	
68.000	67.105			246.50	
70.000	69.057	.0639	.0883	249.60	

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## APPENDIX A

## EXAMPLES OF WIND STATISTICS

Appendix A gives some examples of graphical displays of wind statistics that can be derived from the statistical parameters presented in Table I. These illustrations should aid the user of the RRA in understanding the functional relationships of the probability wind models and, thus, develop an appreciation of the powerful properties of the bivariate normal probability distribution function.

In Figure A-1 the solid straight lines for the univariate normal probability distribution function for the U - and V - wind components are plotted on normal probability graph scales using equation (7). The empirical percentile values for these wind components taken from the previously published RRA for KMR, Document 104-63 (Part I), October 1974, are illustrated by symbols. Considering the differences in the period of record and the statistical methodology, there is good agreement between these wind statistics for this example.

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The conditional probability distribution function (PDF) shown in Figure A-2 is obtained by computing the conditional mean and conditional standard deviation for the V - wind component given that the U - wind component is 10.10 m/s using equations (18) and (19) and the five wind component parameters from Table I.1. The resulting conditional mean and conditional standard deviation is used in equation (7) to make the graph. In this example the conditional PDF is almost identical to the original (unconditional PDF) V - wind component because the correlation coefficient is very nearly zero.

Figures A-3-1 through A-3-6 were obtained by using the five wind component parameters from Tables I.1 and I.6 as input to the rotational equations (44) through (47) and small increments of  $\alpha$  for  $0<\alpha\leq 360$  degrees to compute the component means and standard deviations for each  $\alpha$  were used in equation (8) to obtain the 90th interpercentile range and plotted by an electronic computer. The locus of the component means for each  $\alpha$  giving the circle, was similarly plotted.

Using the five wind component parameters from Tables I.1 and I.6 and p=0.50, p=0.95 and p=0.99 as input values to equation (13), the wind probability ellipses shown in Figures A-4-1 through A-4-12 were obtained by computer graphics. The statistical inferences are, for example, that 50 percent of the wind vectors lie within the smaller ellipse and 99 percent of the wind vectors lie within the outer ellipse. These probability ellipses are illustrated using the standard meteorological coordinate system explained in Chapter I.B.1.

Using the five wind component parameters from Table I.1 in equation (30), the generalized Rayleigh probability distribution shown in Figure A-5 was derived. A comparison is made with the normal probability distribution for wind speed using the mean and standard deviation for wind speed taken from Table I.1. The empirical percentile values (plotted in symbols) for wind speed were taken from the previously published KMR, RRA, October 1974. In this example, there is closer agreement between the empirical percentile values of wind speed and the derived distribution (Rayleigh) for wind speed than with the assumption that wind speed is normally distributed.

The probability distributions of wind speed shown in Figure A-6 were derived using the five wind component parameters from Table I.1 as inputs to the Rayleigh distribution, equation (30).

Figure A-7 was obtained in a similar manner to Figure A-6 using the wind component parameters from Table I.6.

The derived frequencies for wind direction shown in Figures A-8-1 through A-8-12 were obtained using the five wind component parameters from Tables I.1 and I.6 as input values in equation (35). The limits of integration (performed numerically) are over the 22.5-degree interval for each of the 16 compass points. These graphs give the percentage frequency that the wind will blow from the direction intervals.

Figure A-9 (1-8) in cartesian form and figure A-10 (1-12)\* in polar form giving the conditional percentiles of wind speed given the wind direction were derived using the five wind component statistics from Tables I.1 and I.6 as inputs to equation (41), interpolated for percentile values and illustrated by computer graphics. The conditional modes (most frequent) wind speed from the given wind directions were derived using equation (38). The conditional mean wind speeds from the given wind directions were derived using equation (40).

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The locus of the conditional modal wind speed when plotted in polar form versus the given wind directions forms an ellipse. Only in the special case when the coefficient b in equation (41) is zero (i.e., when the component mean values are zero) do the loci of the conditional wind speed for fixed percentile values form a family of ellipses. The irregularities in Figure A-10-3 are caused by the lack of computational precision in evaluating equation (40) and equation (41) when the arguments for the Gaussian probability distribution function have large negative values, i.e., when the coefficients (b/a) become less than negative 4.

This appendix contains only a few of the many options in presenting wind statistics illustrations.

<sup>\*</sup> Although these curves in figure A-10 (1-12) appear to be ellipses, they are not. The only curve in these figures that is an ellipse is the conditional mode.

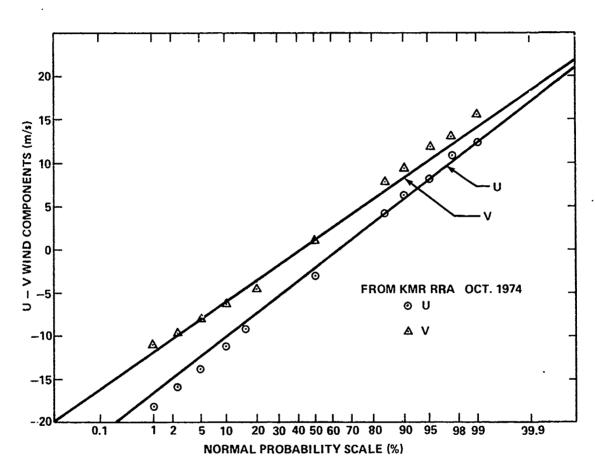


Figure A-1. Normal probability distribution of zonal (U) and meridional (V) wind component KMR, 12 km altitude,
January.

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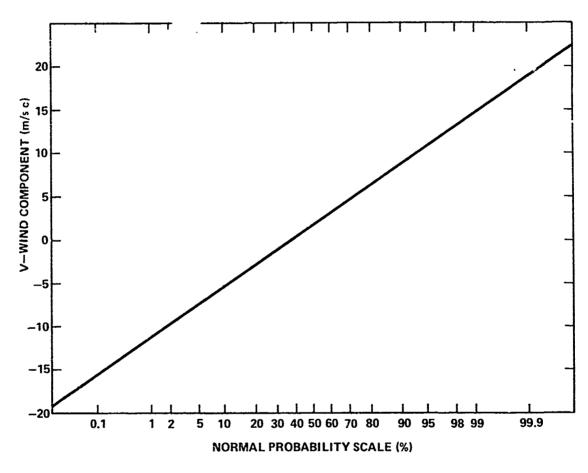


Figure A-2. Conditional distribution of meridional wind component (V) given that the zonal wind component, U = 10.10 m/s KMR, 12 km altitude, January.

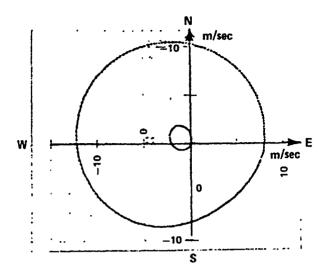


Figure A-3-1. Locus of 90th interpercentile range and locus of mean wind components w.r.t. all azimuths 0-360 degrees KMR, 12 km altitude, January.

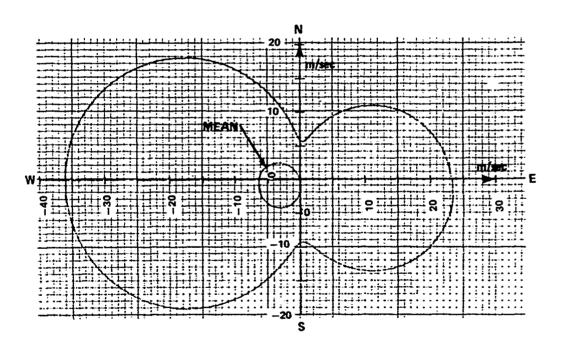


Figure A-3-2. KMR, 36 km altitude, January.

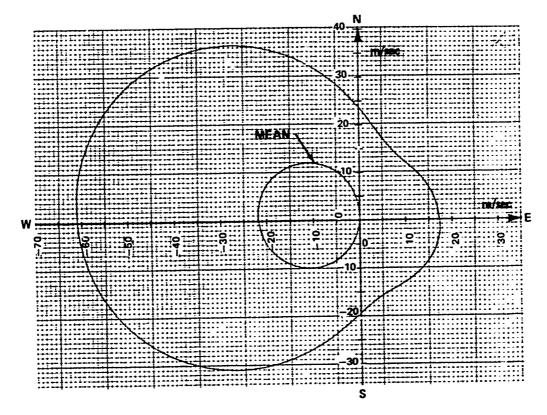


Figure A-3-3. KMR 50 km altitude, January.

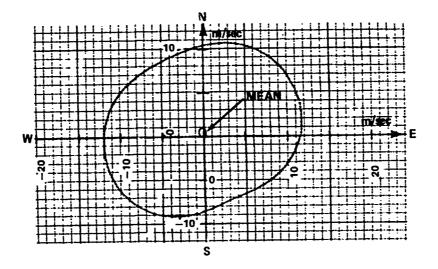


Figure A-3-4. KMR, 12 km altitude, July.

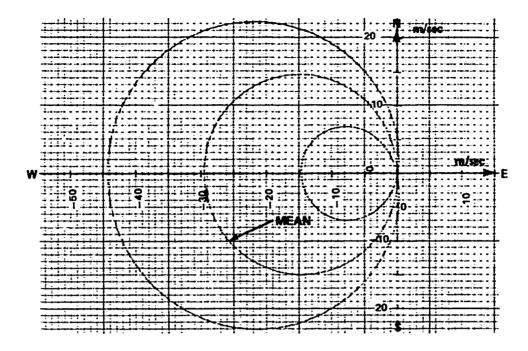


Figure A-3-5. KMR, 36 km altitude, July.

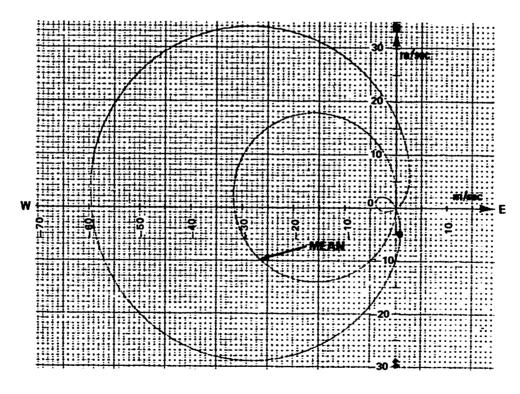


Figure A-3-6. KMR, 50 km altitude, July.

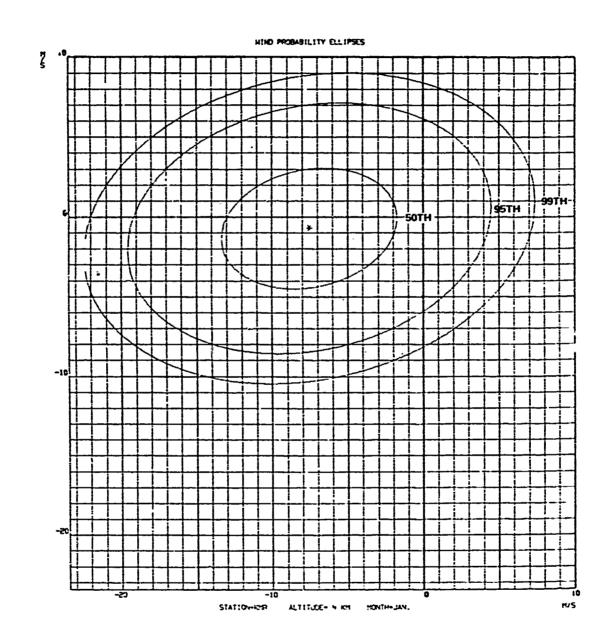


Figure A-4-1. Vector wind ellipses.

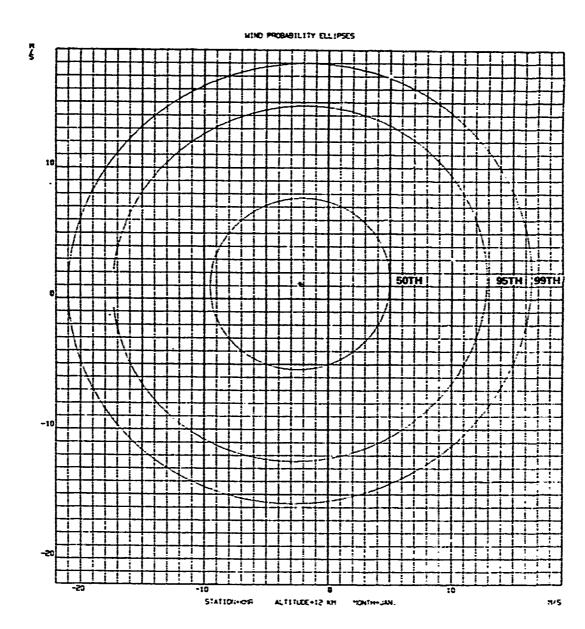
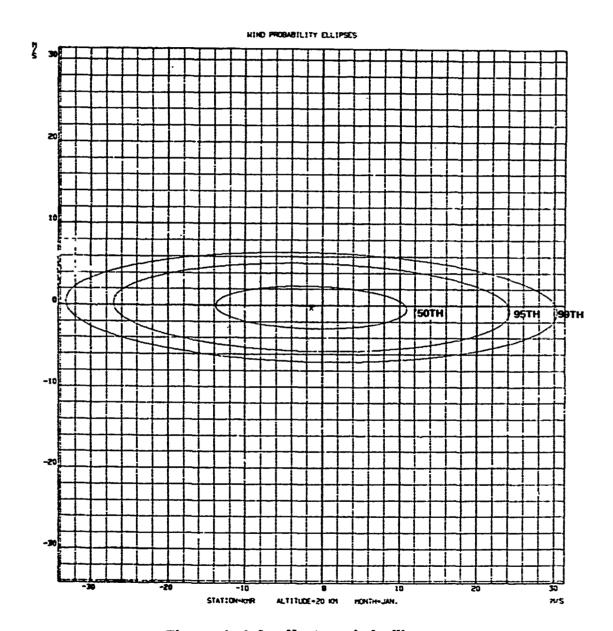


Figure A-4-2. Vector wind ellipses.

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Figure A-4-3. Vector wind ellipses.

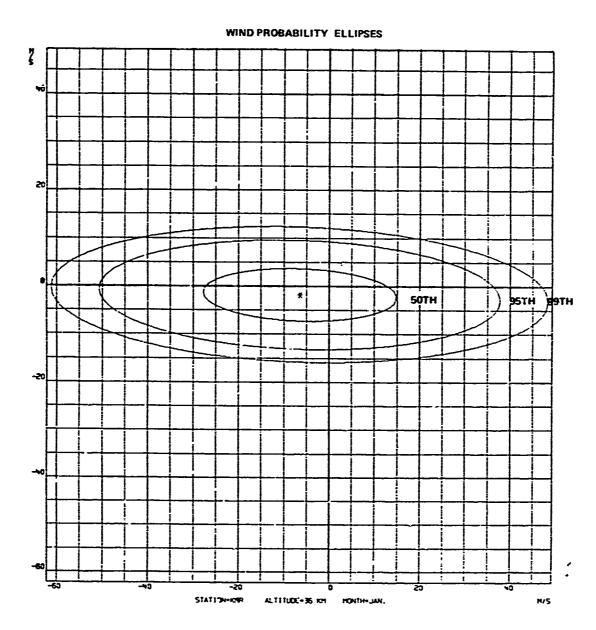


Figure A-4-4. Vector wind ellipses.

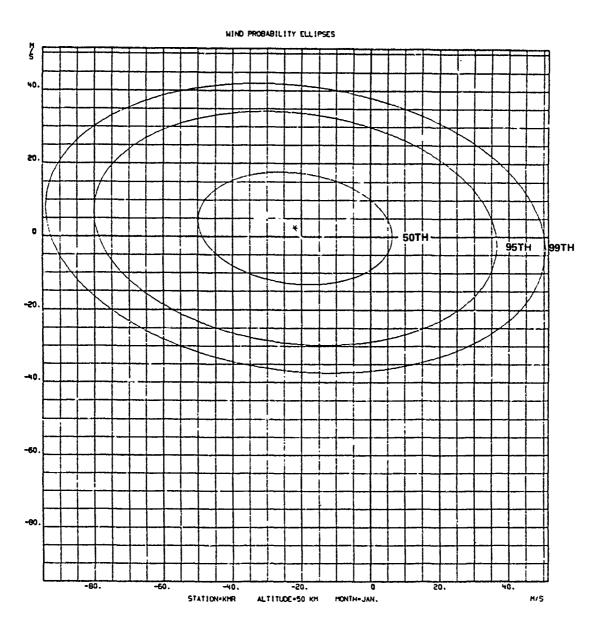


Figure A-4-5. Vector wind ellipses.

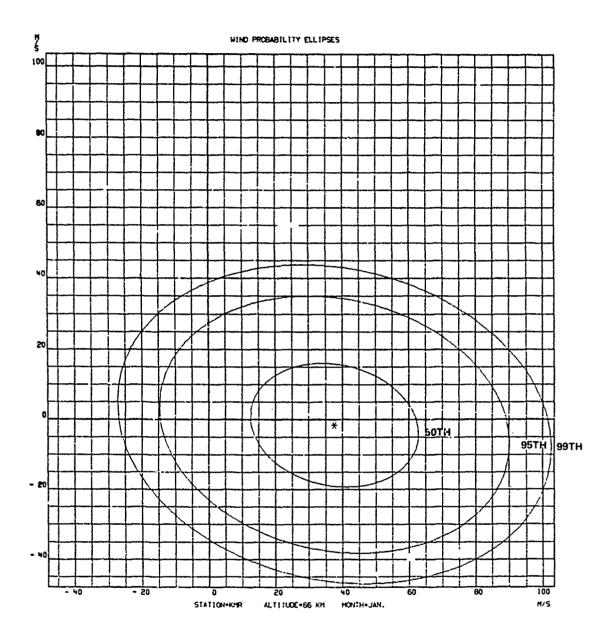


Figure A-4-6. Vector wind ellipses.

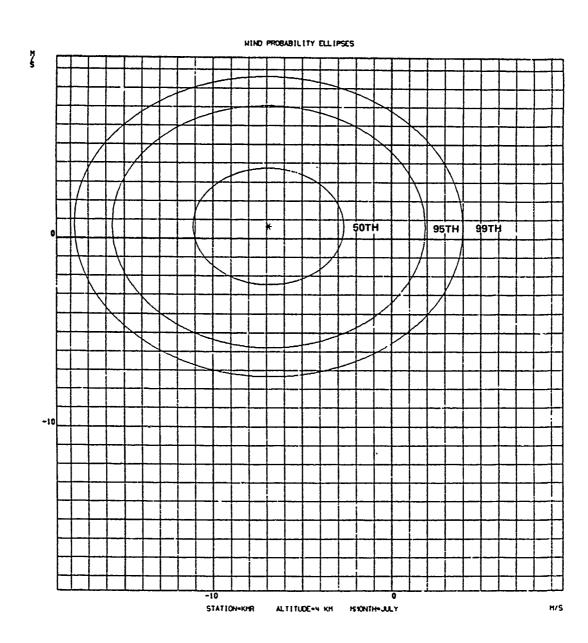


Figure A-4-7. Vector wind ellipses.

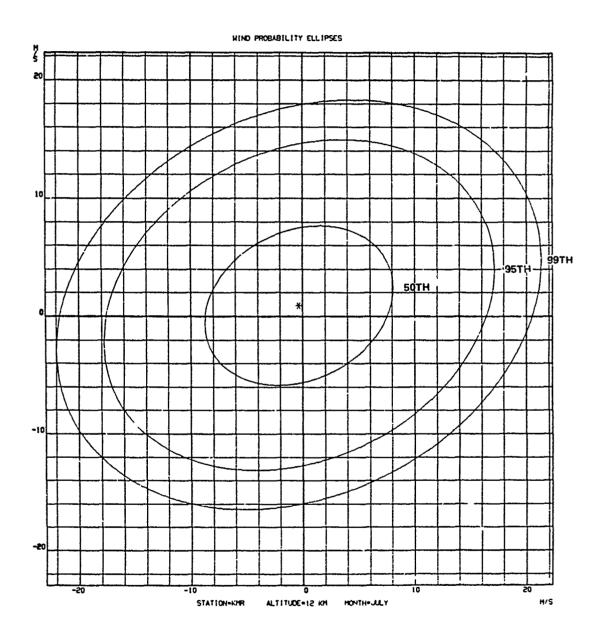


Figure A-4-8. Vector wind ellipses.

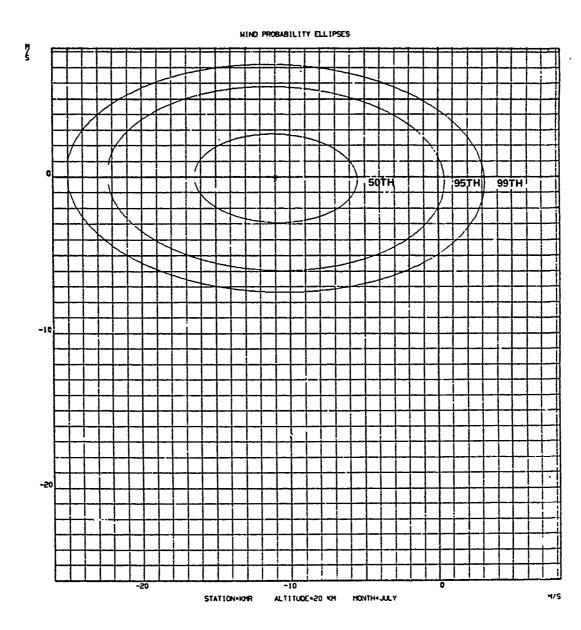


Figure A-4-9. Vector wind ellipses.

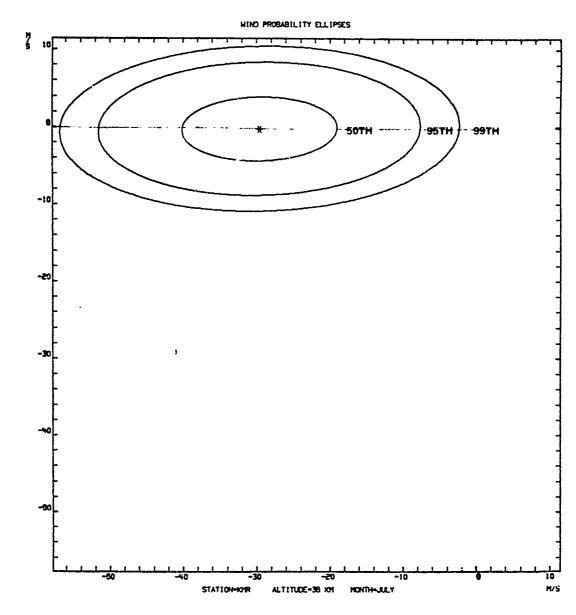
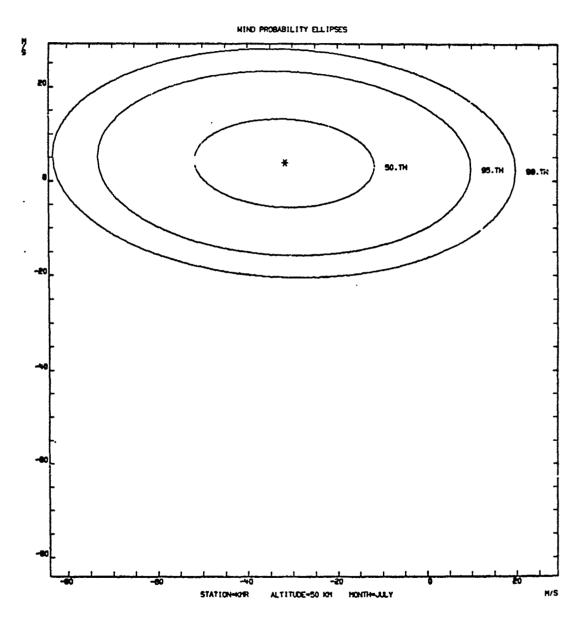


Figure A-4-10. Vector wind ellipses.

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Figure A-4-11. Vector wind ellipses.

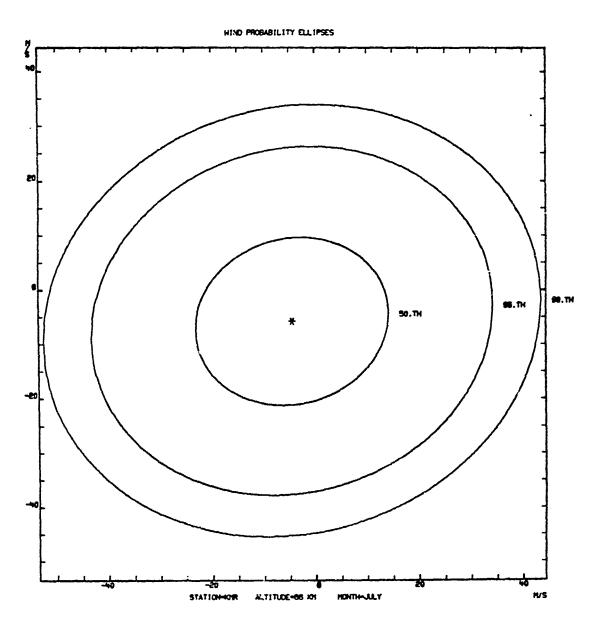


Figure A-4-12. Vector wind ellipses.

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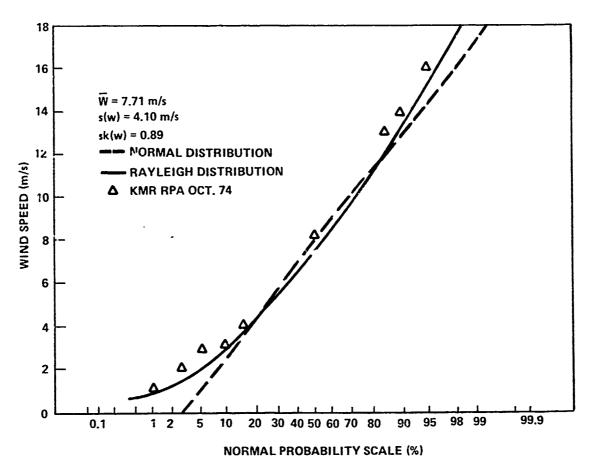


Figure A-5. Wind speed distribution KMR, 12 km altitude, January.

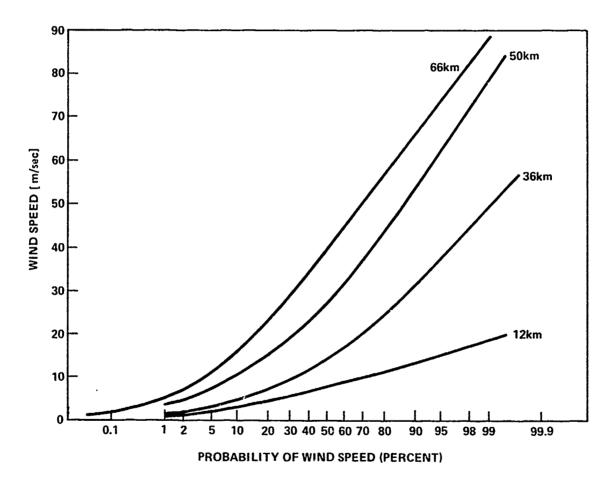


Figure A-6. Derived (Rayleigh) distributions for wind speed at 12, 36, 50 and 66 km altitude, KMR, January.

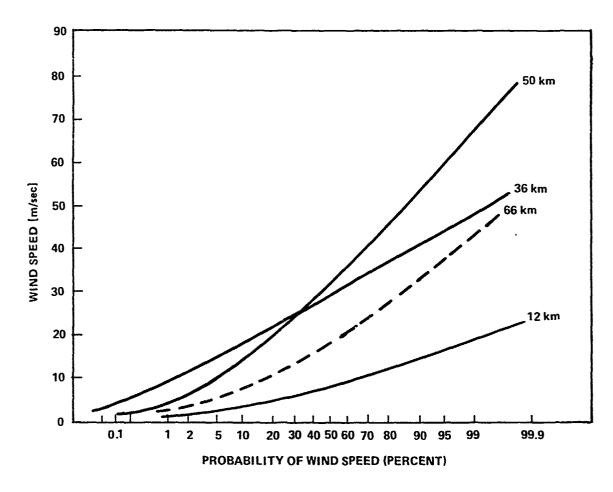


Figure A-7. Derived (Rayleigh) distributions for wind speed at 12, 36, 50, and 66 km altitude, KMR, July.

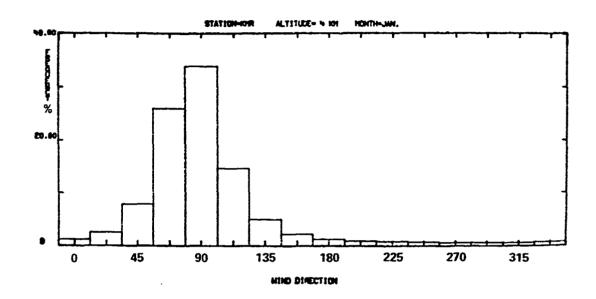


Figure A-8-1. Frequency of wind direction.

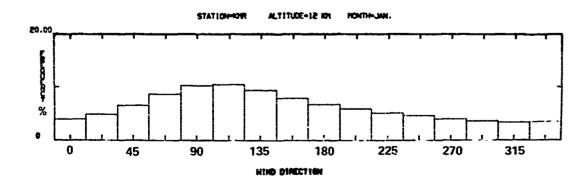


Figure A-8-2. Frequency of wind direction.

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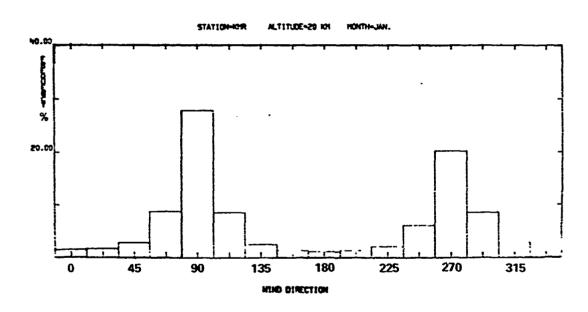


Figure A-8-3. Frequency of wind direction.

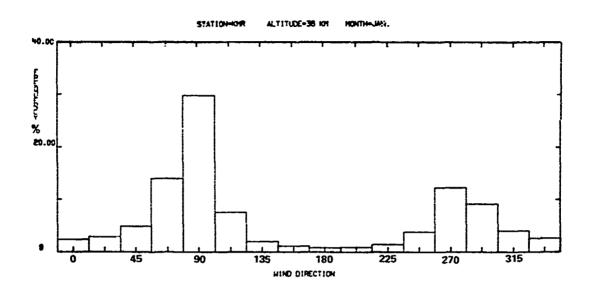


Figure A-8-4. Frequency of wind direction.

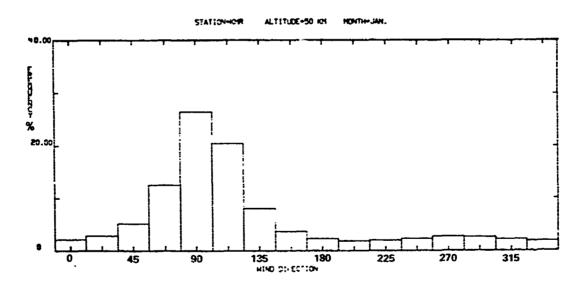


Figure A-8-5. Frequency of wind direction.

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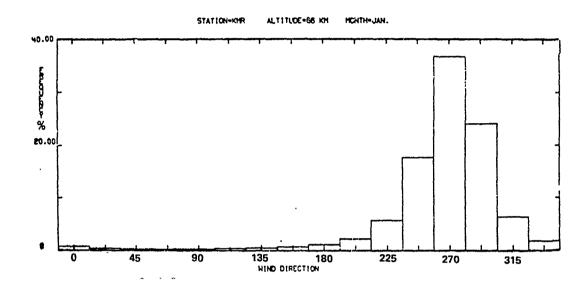


Figure A-8-6. Frequency of wind direction.

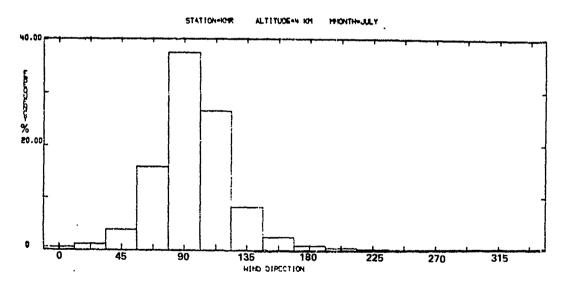


Figure A-8-7. Frequency of wind direction.

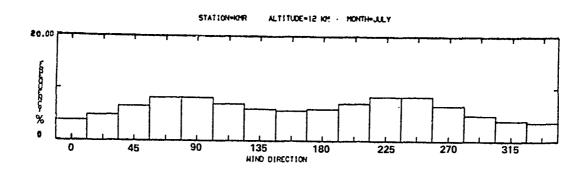


Figure A-8-8. Frequency of wind direction.

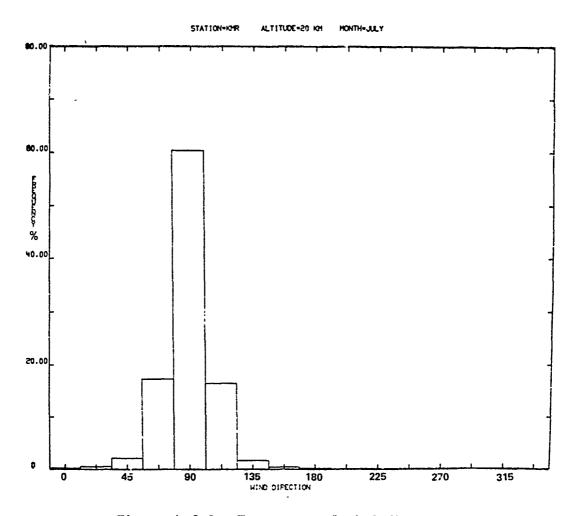


Figure A-8-9. Frequency of wind direction.

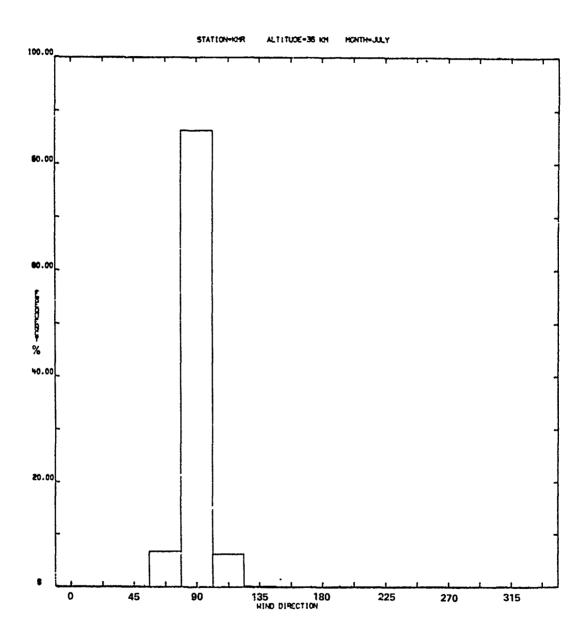


Figure A-8-10. Frequency of wind direction.

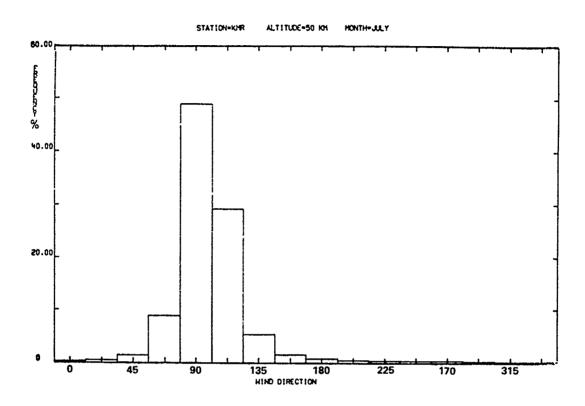


Figure A-8-11. Frequency of wind direction.

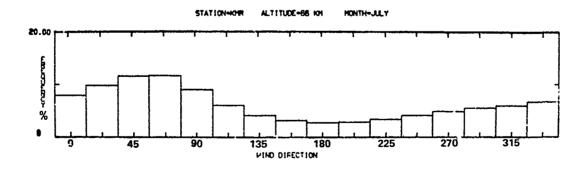


Figure A-8-12. Frequency of wind direction.

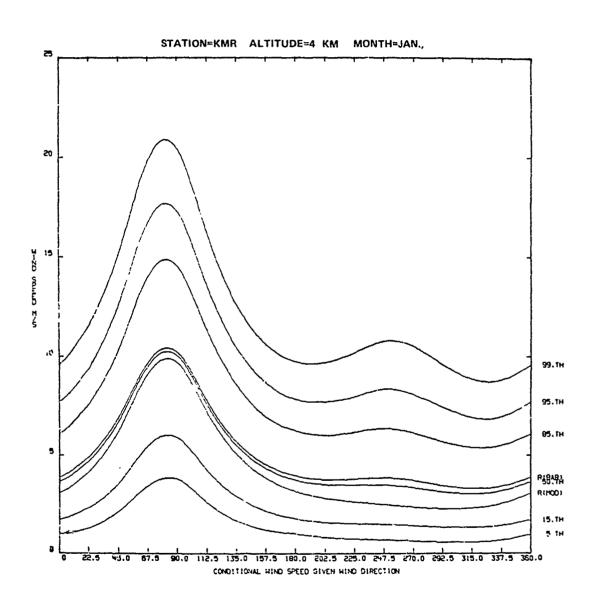


Figure A-9-1. Conditional distribution of wind speeds from the given wind directions cartesian form.

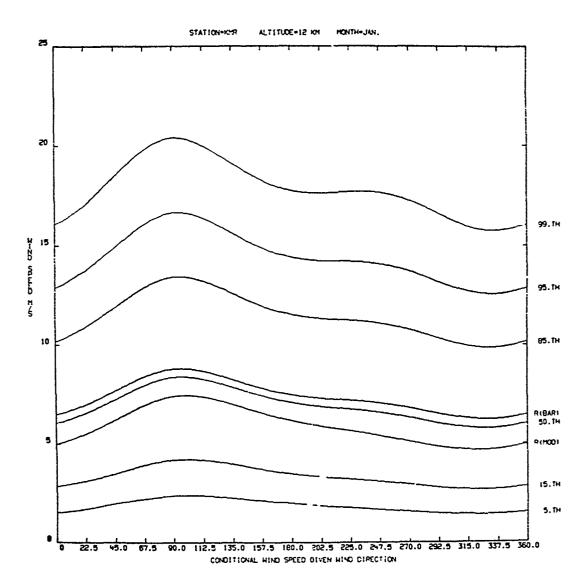


Figure A-9-2. Conditional distribution of wind speeds from the given wind directions cartesian form.

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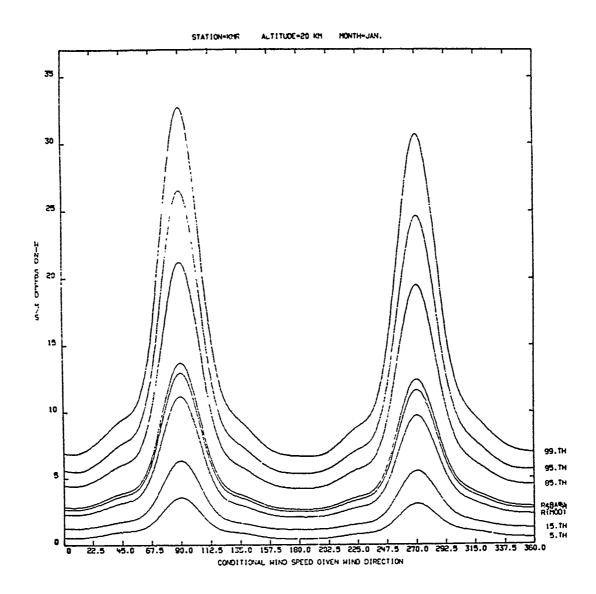


Figure A-9-3. Conditional distribution of wind speeds from the given wind directions cartesian form.

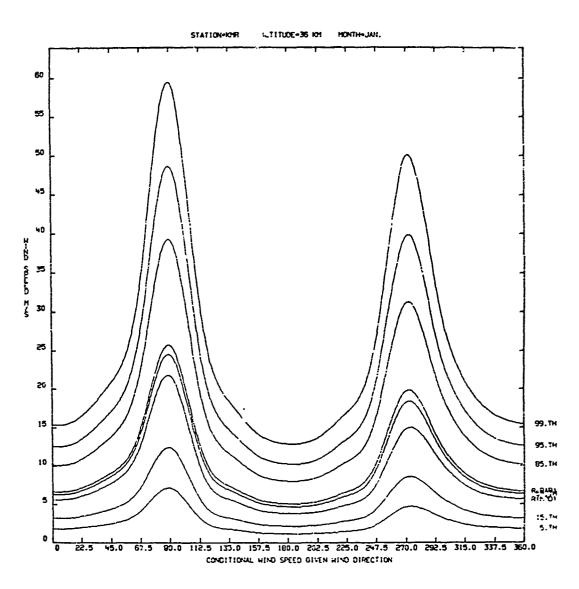


Figure A-9-4. Conditional distribution of wind speeds from the given wind directions cartesian form.

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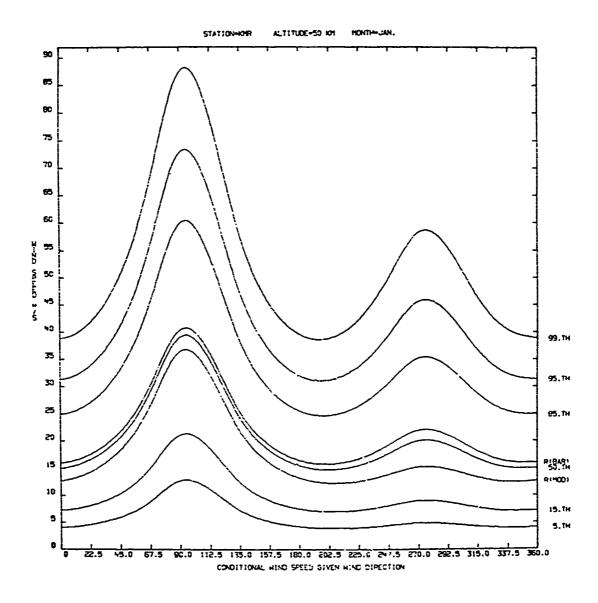


Figure A-9-5. Conditional distribution of wind speeds from the given wind directions cartesian form.

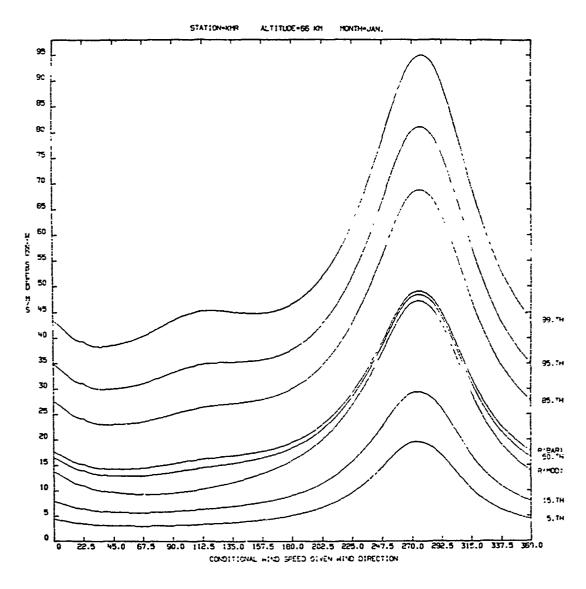
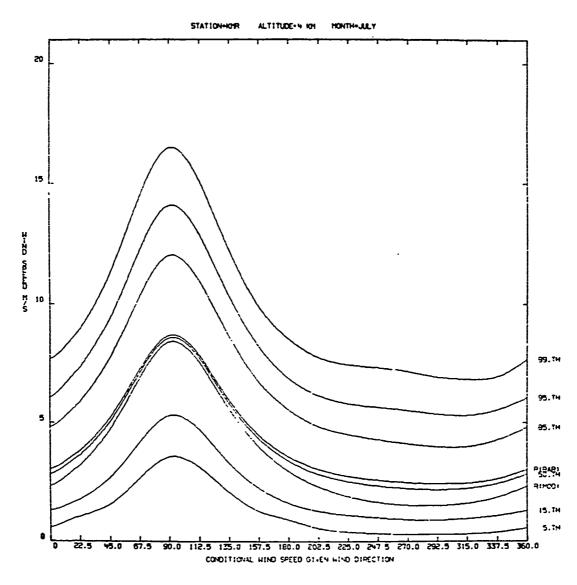


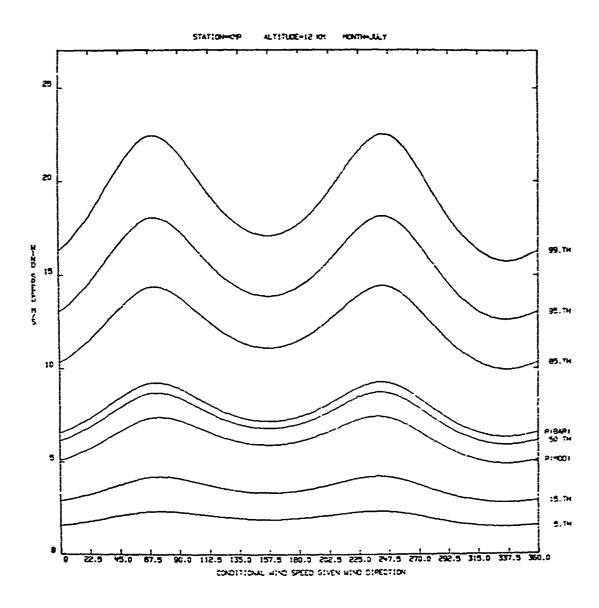
Figure A-9-6. Conditional distribution of wind speeds from the given wind directions cartesian form.

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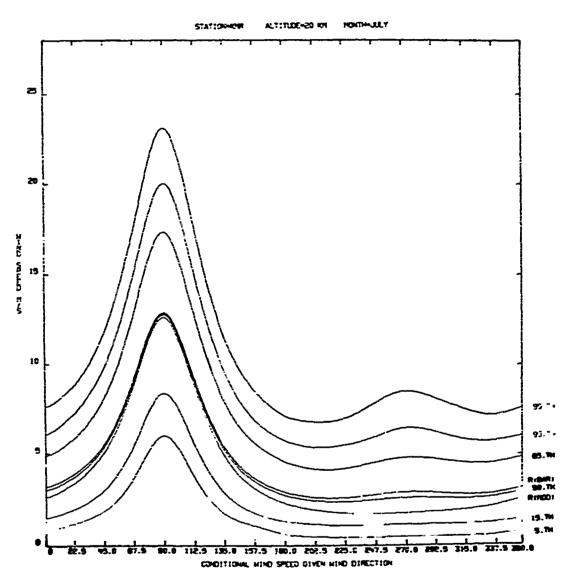
Figure A-9-7. Conditional distribution of wind speeds from the given wind directions cartesian form.



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Figure A-9-8. Conditional distribution of wind speeds from the given wind directions cartesian form.

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Figure A-9-9. Conditional distribution of wind speeds from the given wind directions cartesian form.

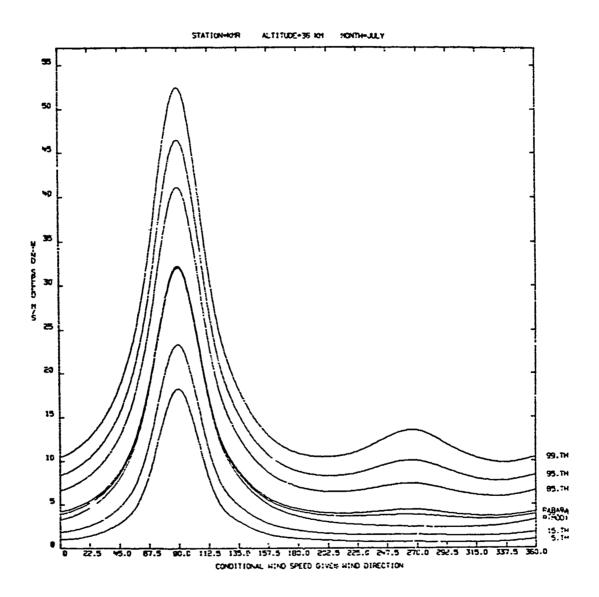


Figure A-9-10. Conditional distribution of wind speeds from the given wind directions cartesian form.

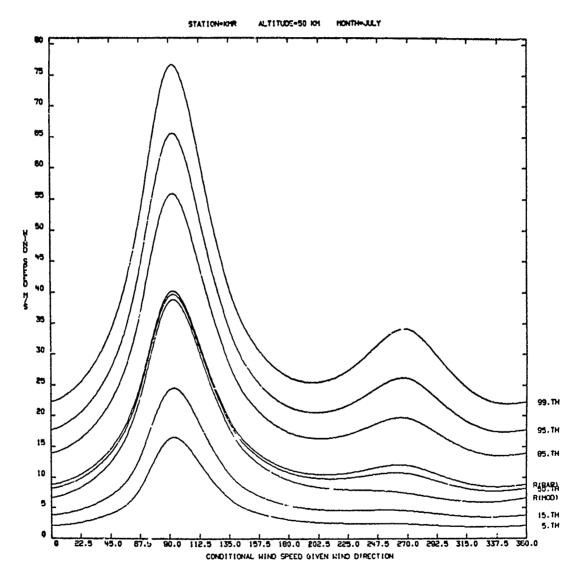


Figure A-9-11. Conditional distribution of wind speeds from the given wind directions cartesian form.

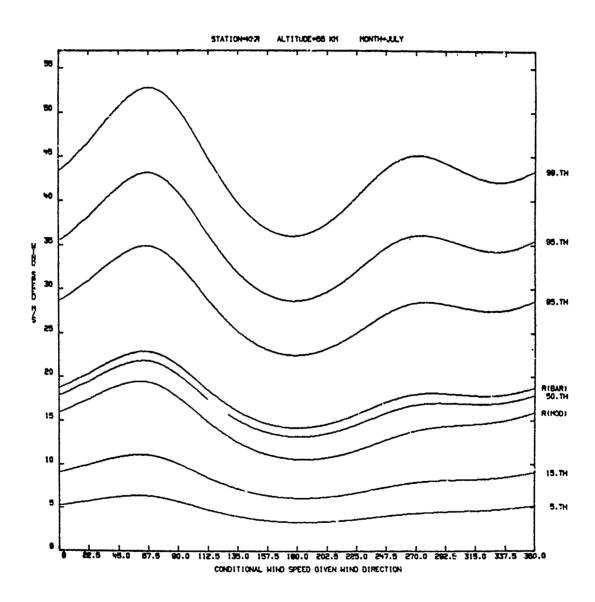


Figure A-9-12. Conditional distribution of wind speeds from the given wind directions cartesian form.

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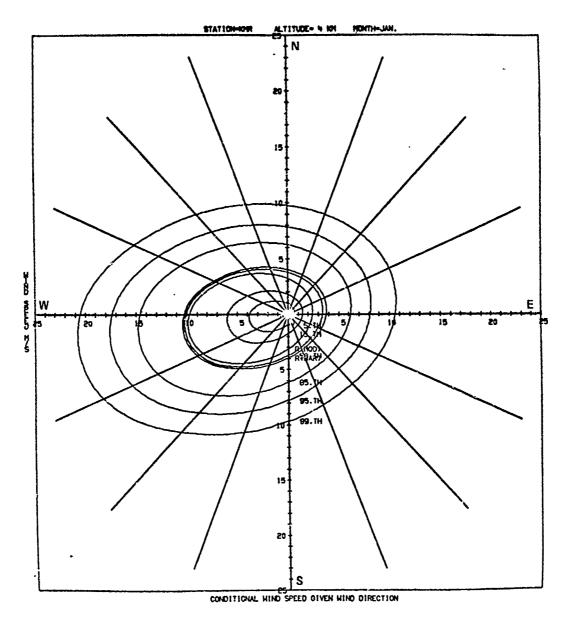


Figure A-10-1. Conditional distribution of wind speeds from the given wind directions polar form.

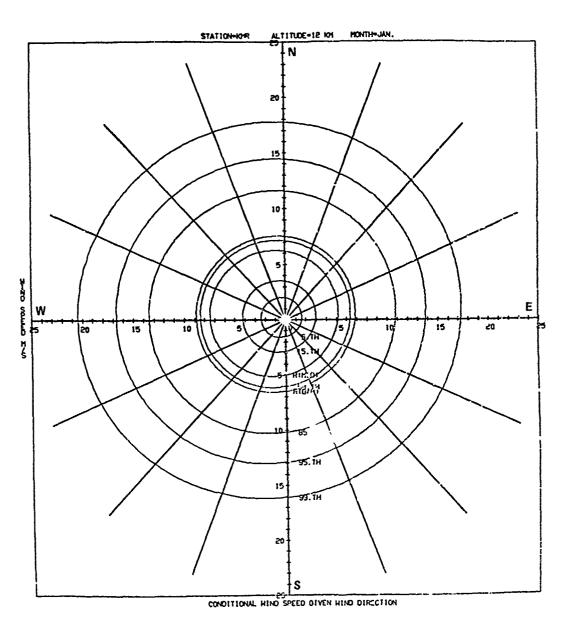


Figure A-10-2. Conditional distribution of wind speeds from the given wind directions polar form.

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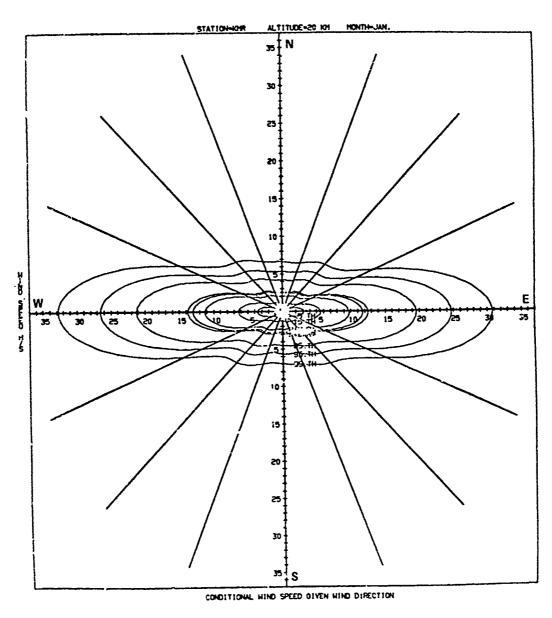


Figure A-10-3. Conditional distribution of wind speeds from the given wind directions polar form.

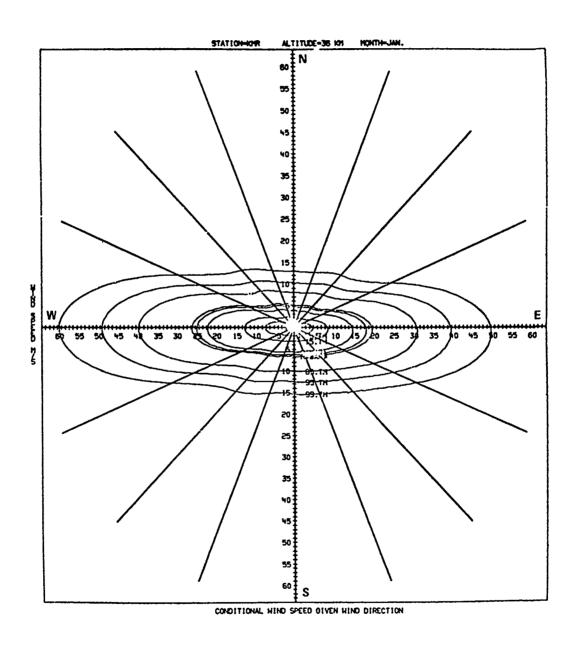


Figure A-10-4. Conditional distribution of wind speeds from the given wind directions polar form.

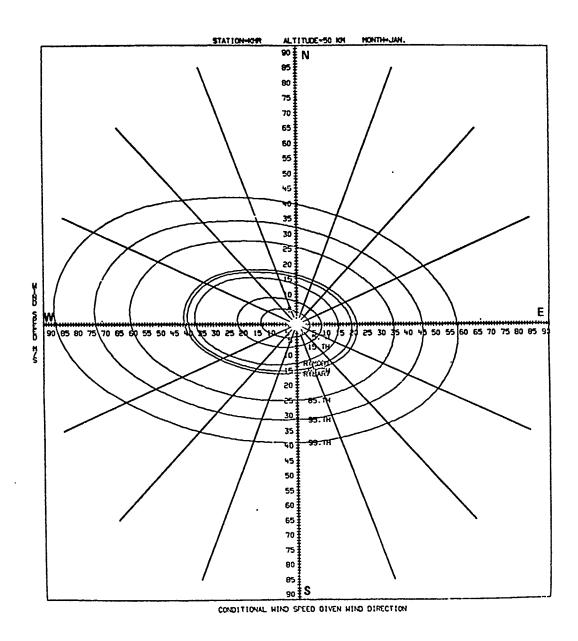


Figure A-10-5. Conditional distribution of wind speeds from the given wind directions polar form.

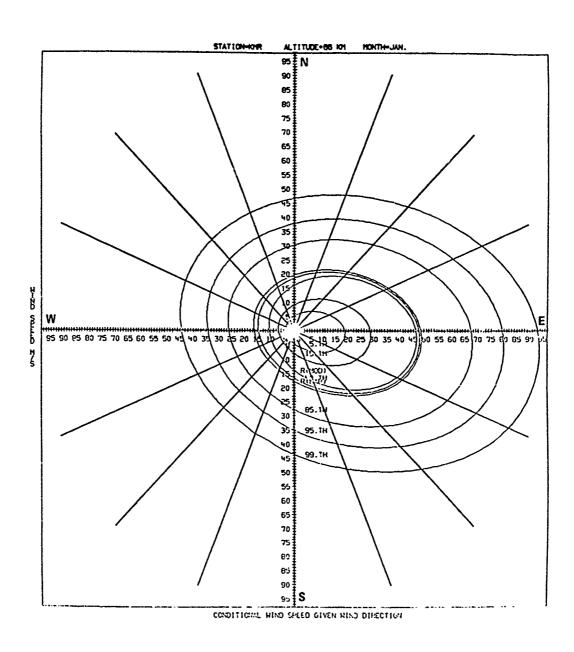


Figure A-10-6. Conditional distribution of wind speeds from the given wind directions polar form.

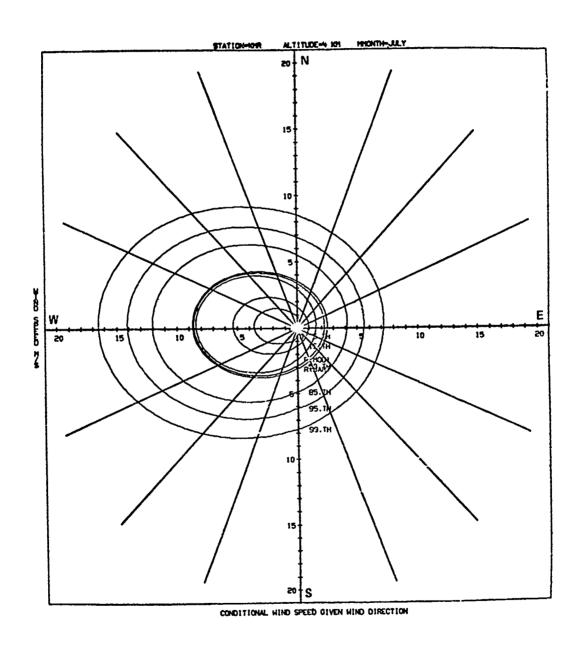


Figure A-10-7. Conditional distribution of wind speeds from the given wind directions polar form.

## STATION=KMR ALTITUDE=12 KM MONTH=JULY

Figure A-10-8. Conditional distribution of wind speeds from the given wind directions polar form.

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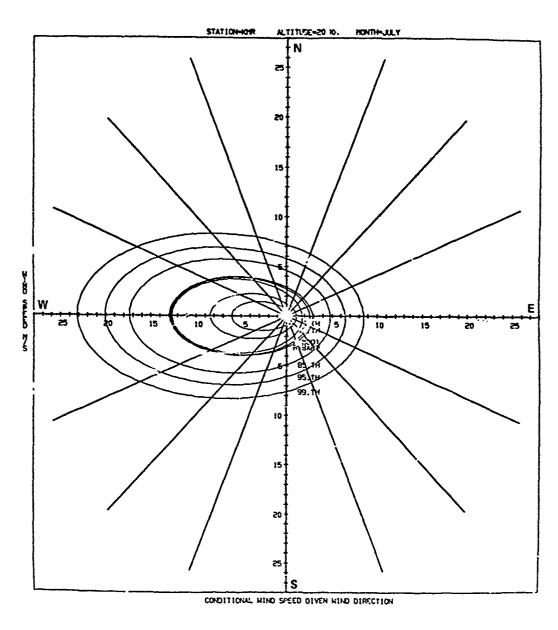


Figure A-10-9. Conditional distribution of wind speeds from the given wind directions polar form.

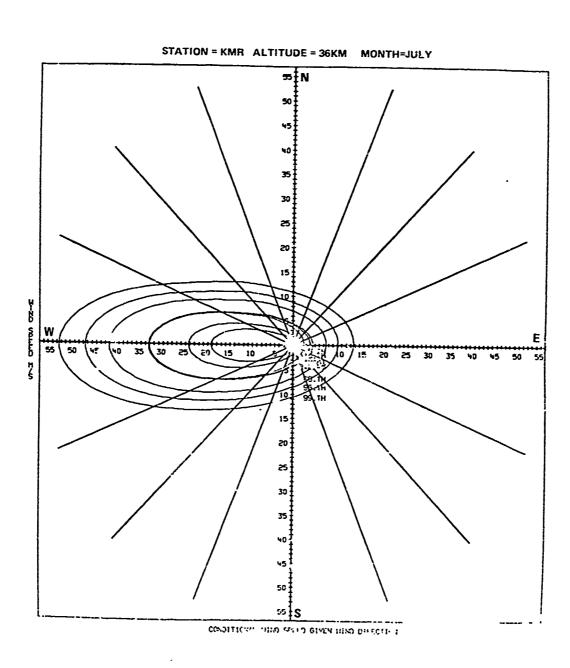


Figure A-10-10. Conditional distribution of wind speeds from the given wind directions polar form.

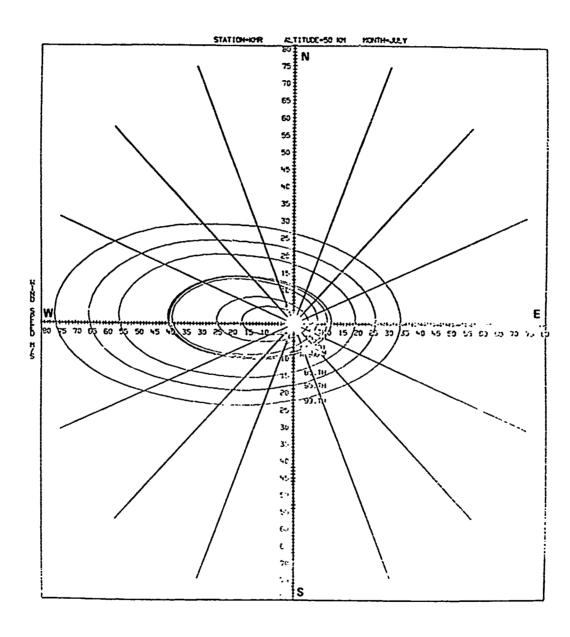


Figure A-10-11. Conditional distribution of wind speeds from the given wind directions polar form.

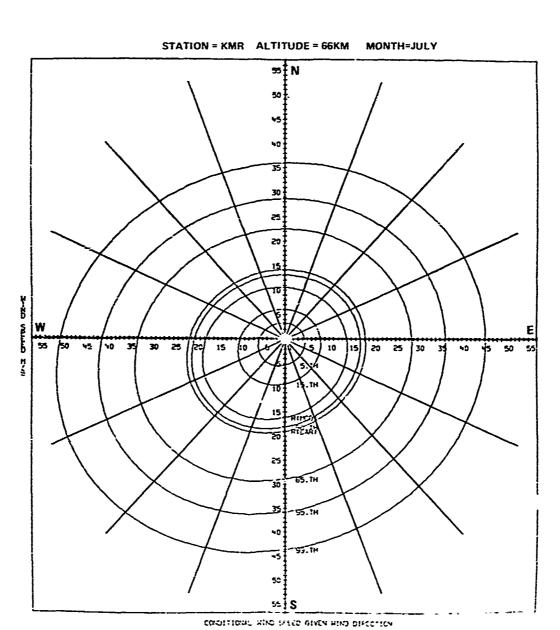


Figure A-10-12. Conditional distribution of wind speeds from the given wind directions polar form.

## APPENDIX B

## RANGE SPECIFIC INFORMATION

Different periods of record were used to generate the lower ( $\leq 30~\rm km$  altitude) and the upper ( $\geq 30~\rm km$  altitude) portion of the Kwajalein RRA. The period of record for the lower portion was from January 1960 to December 1974. The changes in the rawinsonde observation times and the monthly distributions of the number of observations precluded the use of the rawinsonde observations for the lower portion of the KMR RRA for the period after December 1974. The upper portion was generated using the rocketsonde measurements for the period of record January 1969 to December 1976.

The rocketsonde observations used to calculate the upper portion of the KMR RRA were taken primarily from 2200 GMT to 6400 GMT. To ensure consistency, only the upper air observations taken during this "time window" were used for the KMR RRA statistics for both the lower portion and the upper portion.

The "time window" restriction on the KMR data base then implies that the KMR R. is representative of that portion of the diurnal cycle within the time window 2200 GMT to 0400 GMT. Hence, the use of the KMR RRA for time periods outside this time window will be inaccurate depending on the contribution of the interdiurnal variation. In general, the systematic interdiurnal variation of most atmospheric quantities is considered to be small in comparison with the daily random variation above the boundary layer.

Because KMR is in the tropical latitudes, the quasi-biennial oscillation of the wind field and temperature can be detected by a time series analysis of past upper air observation, particularly in the stratosphere. As the term implies, the onset and period of this atmospheric oscillation are not constant. The RRA for KMR has been established for monthly reference periods rather than making an extension to account for past quasi-biennial oscillations because: (a) range program plans are based on a monthly calendar rather than a variable reference period, and (b) there is no universally accepted technique for predicting the phase and duration of future quasi-biennial oscillations.

To prevent further character size reduction for Tables I through IV certain range specific information has been omitted. This important information is given in Table B1 for KMR.

TABLE NUMBER0	TABLE NUMBER 0
DATA SOUPCE (1*DATSAV,2=HDC-A)2	DATA SOURCE (1=DATSAY,2=WDC-A)1
CALL LETTERSPKWA	CALL LETTERSPKWA
HMO NUMBER 91366	WMO NUMSER913660
LATITUDE 8-44'	LATITUDE 8' 44'
DIRECTION (N OR S)N	DIRECTION IN OR S)N
LONGITUDE167°45'	LONGITUDE1, " '45'
DIRECTION (E OF W)E	DIRECTION (E OF W)E
ELEVATION IN METERS 0	ELEVATION IN METERS 2
START PERIOD OF RECORD (MO-YR) 169	START PERIOD OF RECORD (MO-YR) 160
END FERICO OF RECORD (MO-YR-) 12/6	END PERICO OF RECORD (MD-YR-) 1274
NO. OF TIME WINDOWS (0.1 OR 2)	NO. OF TIME WINDOWS (0.1 OR 2)
START TIME WINDOW #1(HR-MNZ) 2200	START TIME W'NDOW \$1(HR-MNZ) 2200
END TIME WINDOWS 81 400	END TIME WINDOWS 81 400
START TIME HINDON 620	START TIME WINDOW #20
END TIME WINDOW #20	END TIME WINDOW #20
DATE OF RRA 1080	DATE OF RRA 980
ALTITUDE RANGE OF RRA LOW LEVEL (KM) 30	ALTITUDE RANGE OF RRA LOW LEVEL (KM) 0
ALTITUDE RANGE OF RRA HIGH LEVEL(KM) 70	ALTITUDE RANGE OF PRA HIGH LEVEL (KM) 30
STANDARD DEVIATION OF THERODYNAMIC LIMITS-6.0	STANDARD DEVIATION OF THERODYNAMIC LIMITS-6.0
WIND LIMITS	WIND LIMITS6.0

Graphical Displays of Thermodynamic Quantities

The differences for the monthly mean values of pressure, density, and temperature for January (Table IV.1) and July (Table IV.7) relative to the annul mean values (Table IV.13) expressed in percent are shown respectively n Figures B1, B2, B3 (for January) and Figures B6, B7, B8 (for July), and for all months in Figures B11, B12, and B13. Further, the differences of the January and July monthly mean temperature from the annual mean temperature expressed as delta degree(s) K are shown in Figures B4 and B9, and for all months in Figure B14. In these figures the altitude regions having the smallest and largest monthly mean differences from the annual mean for these thermodynamic quantities are clearly seen.

The coefficients of variation for pressure,  $C_V^P$ , density,  $C_V^D$ , and temperature,  $C_V^T$ , were computed using the standard deviation values from Table II and the monthly mean values from Table IV. The coefficient of variation is defined by the standard deviation with respect to the monthly mean divided by the monthly mean value.

The coefficients of variations for pressure, density, and temperature are shown in Figure B5 for January and Figure B10 for July. For all months the coefficient of variation for pressure is shown in Figure 15, for density in Figure 16, and for temperature in Figure 17. If the abscissa on the figures is multiplied by 100, then these figures would show the percentage of the random dispersion over the month with respect to the monthly mean for these thermodynamic quantities.

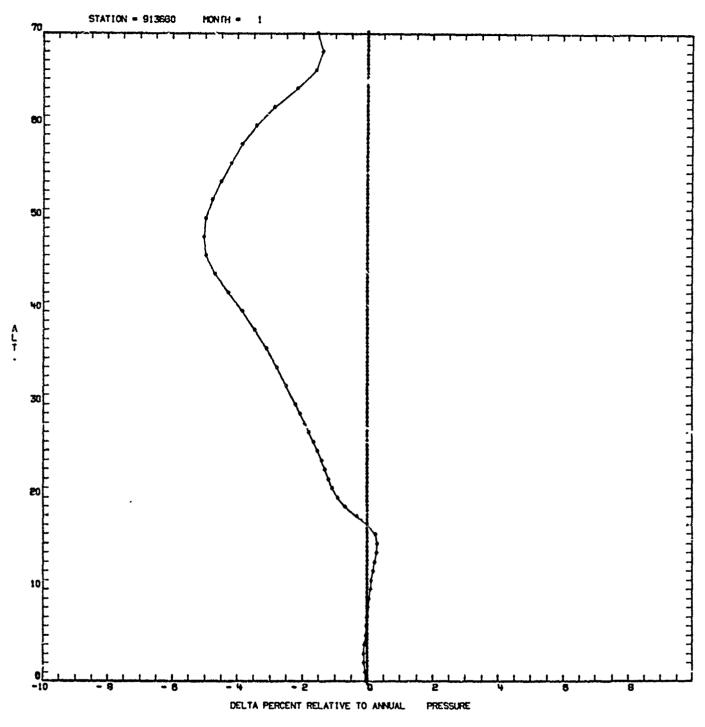


Figure B1.

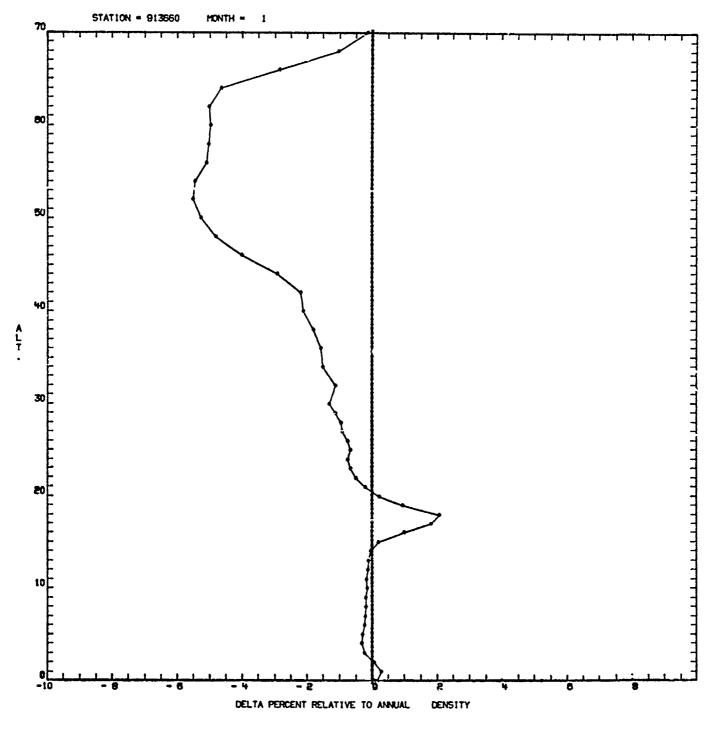


Figure B2.

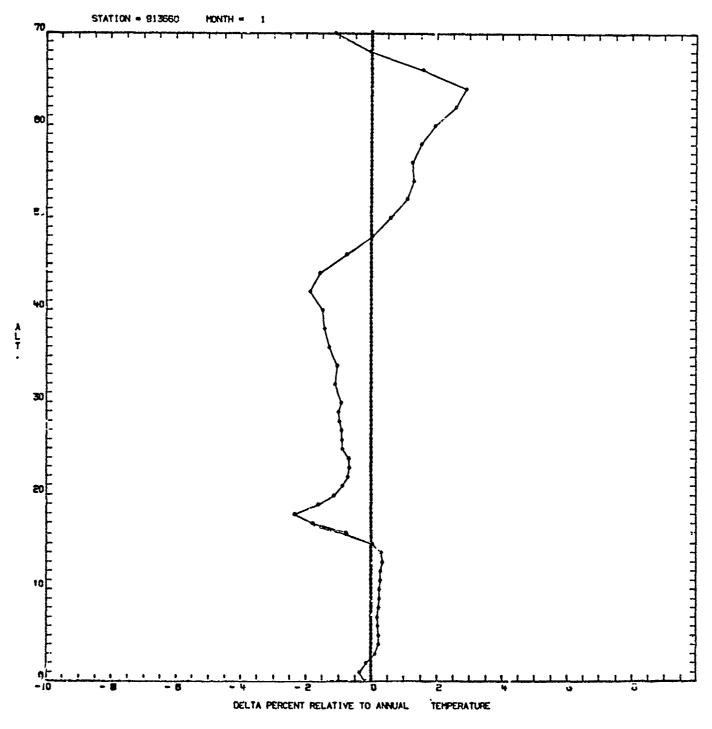


Figure B3.

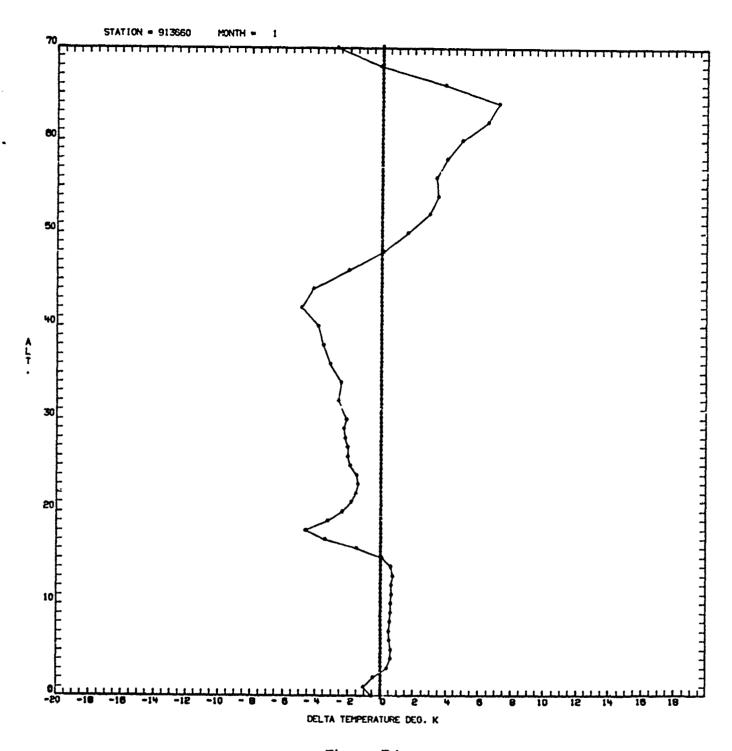


Figure B4.

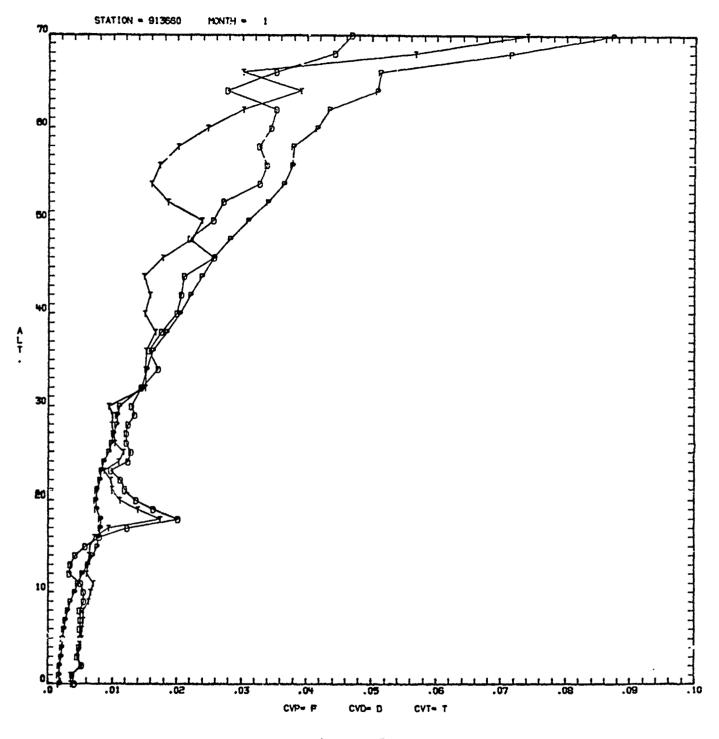


Figure B5.

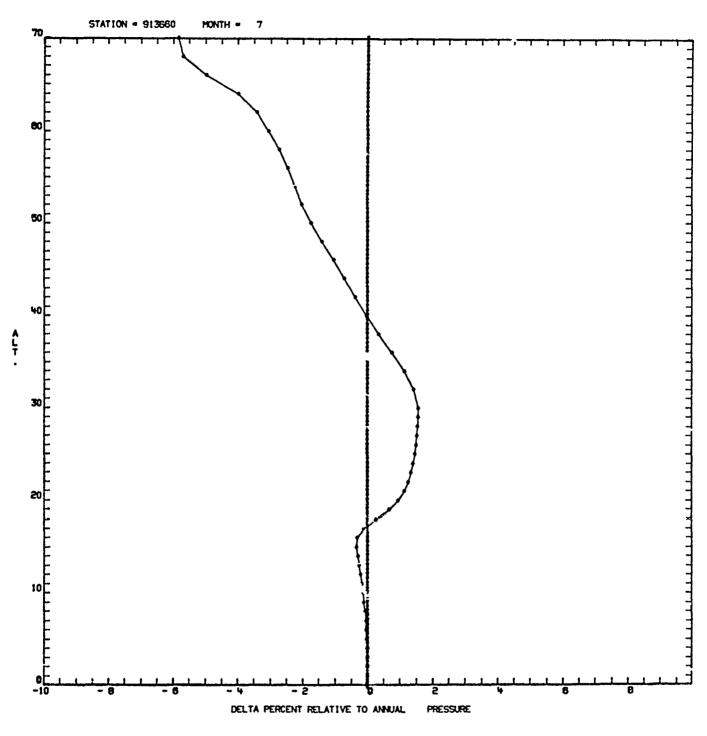


Figure B6.

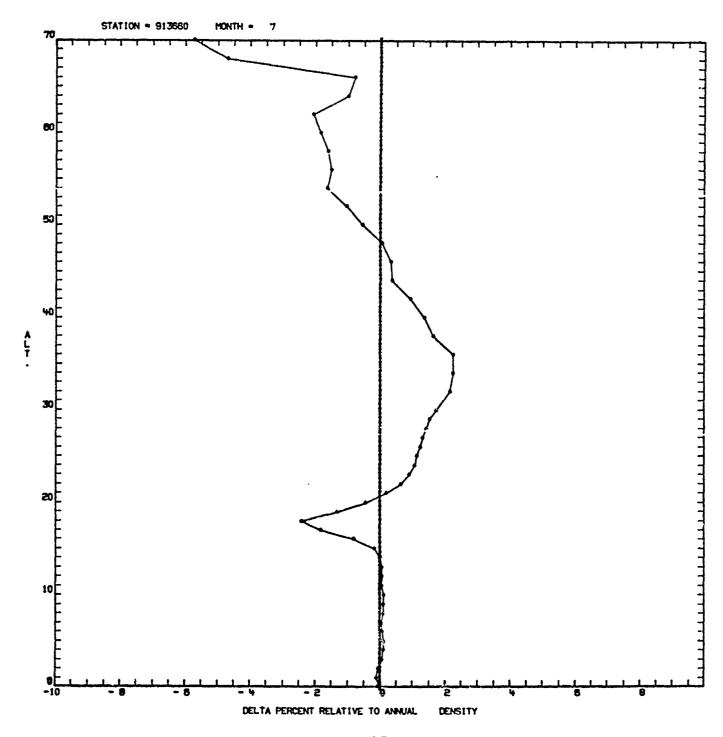


Figure B7.

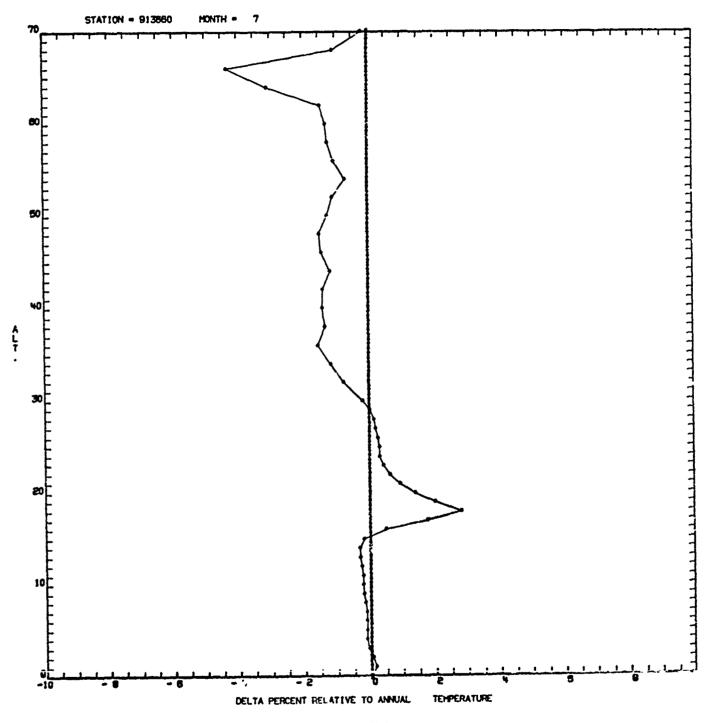


Figure B8.

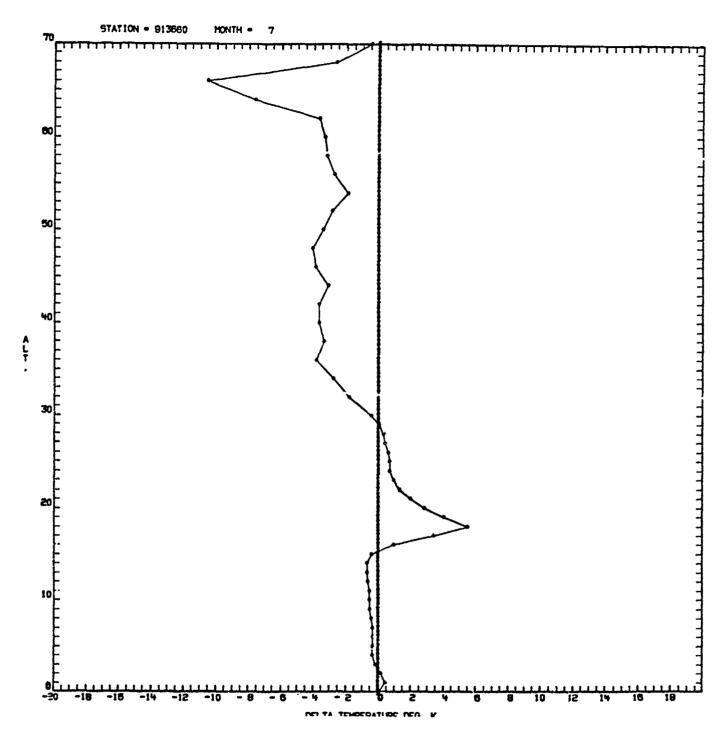


Figure B9.

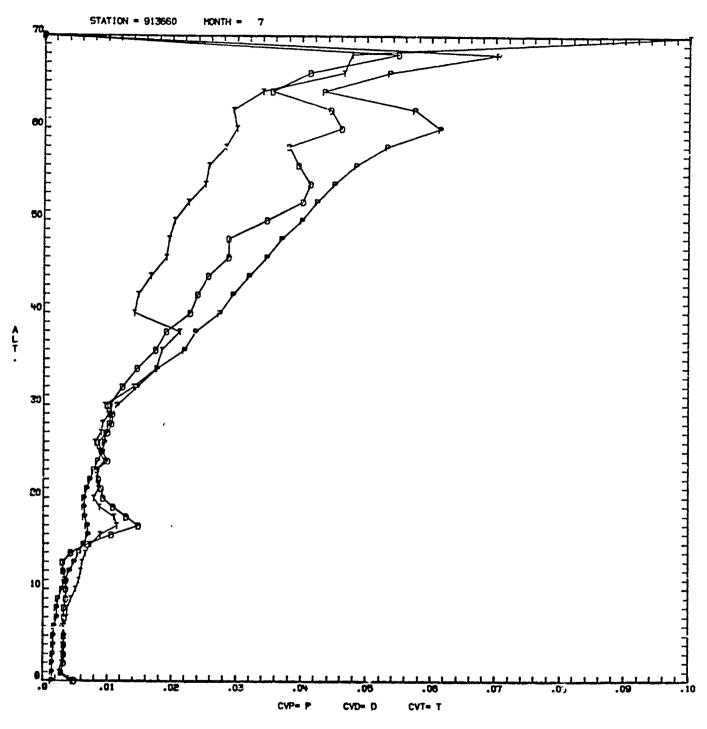


Figure B10.

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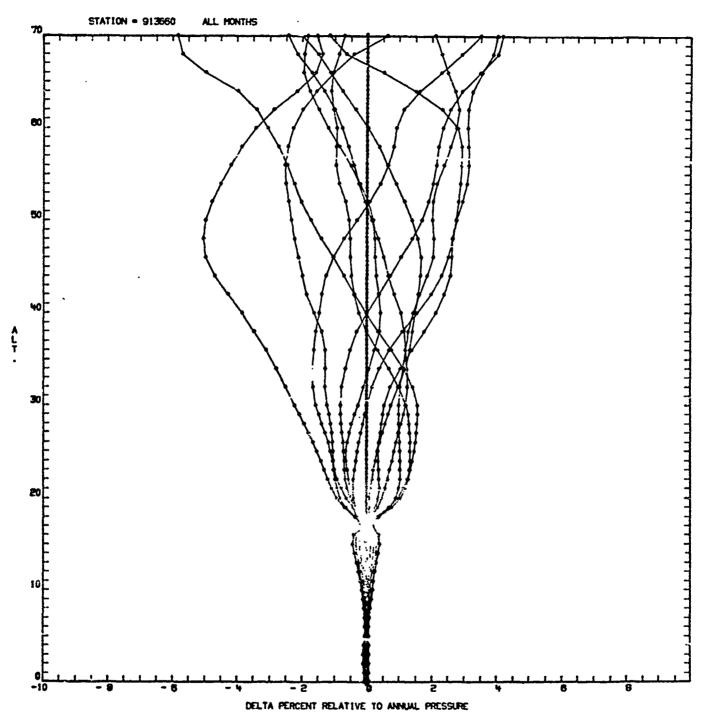


Figure B11.

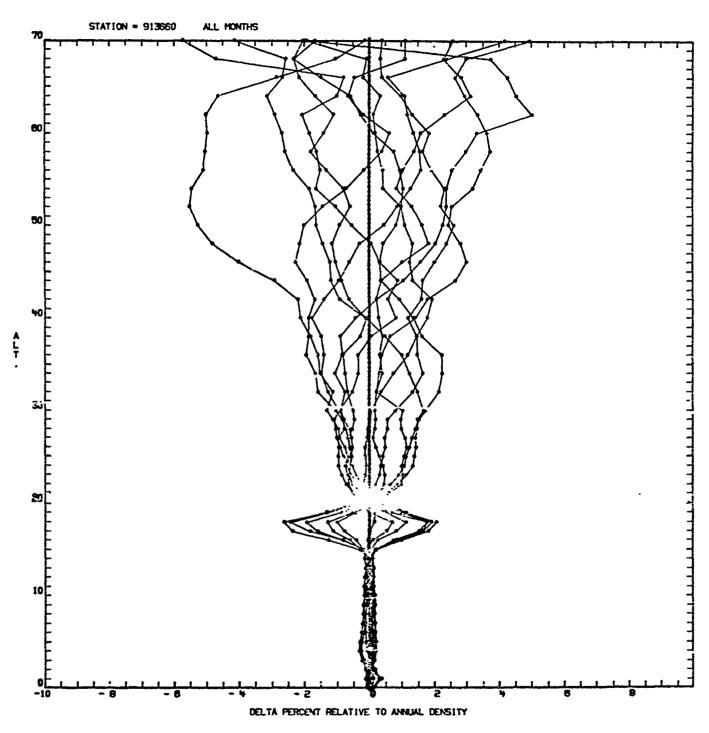


Figure B12.

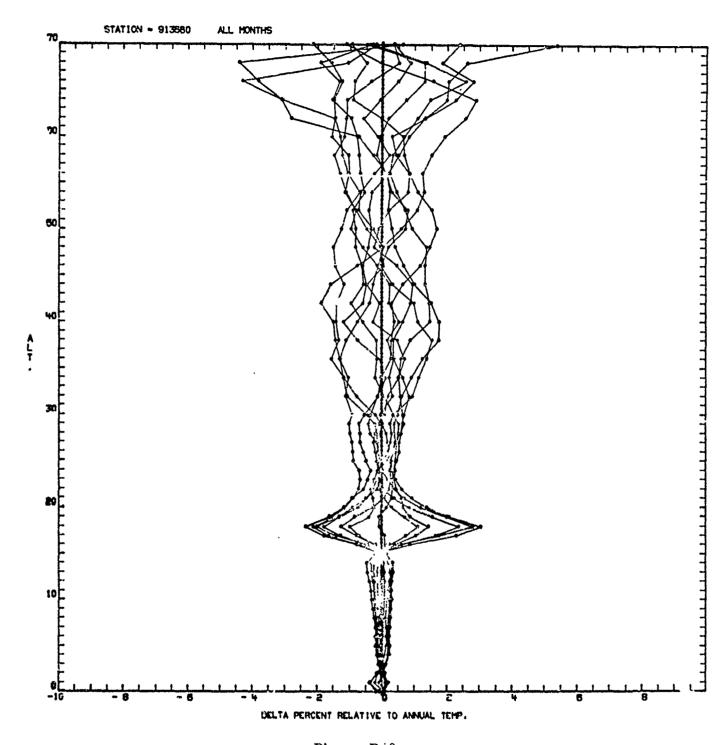


Figure Bi3.

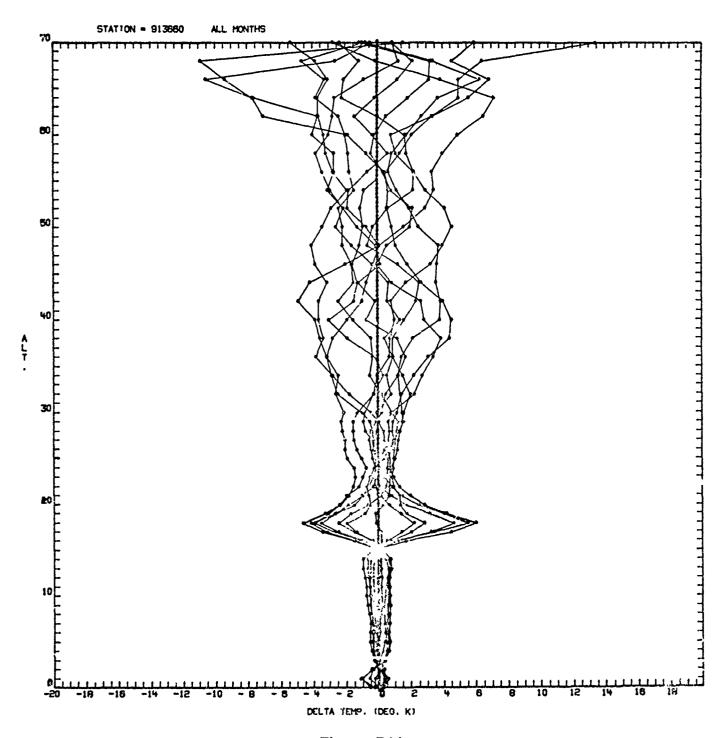


Figure B14.

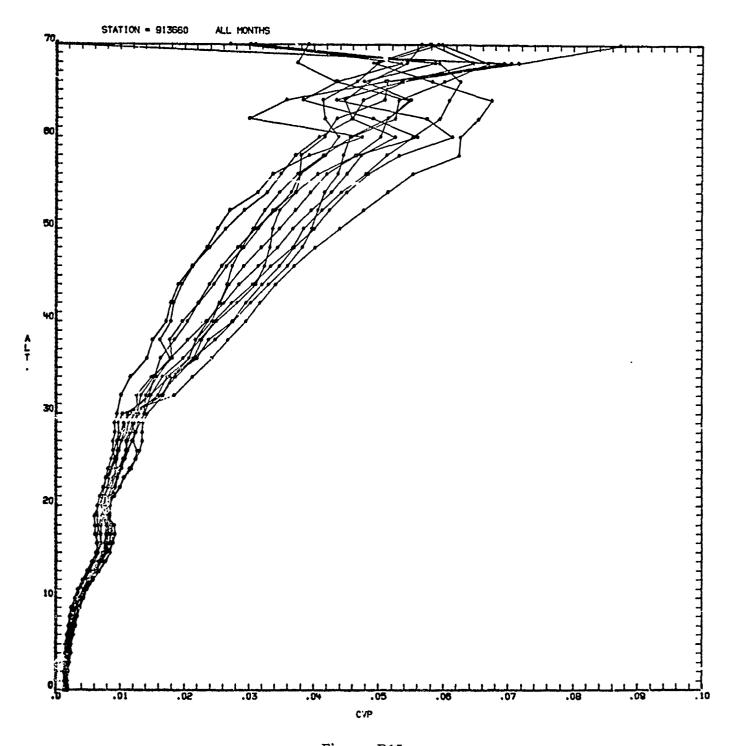


Figure B15.

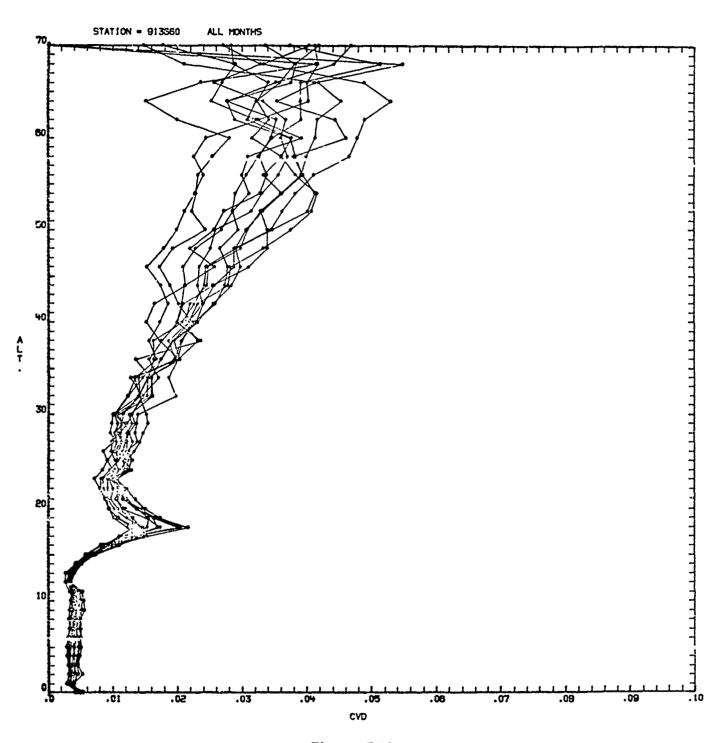
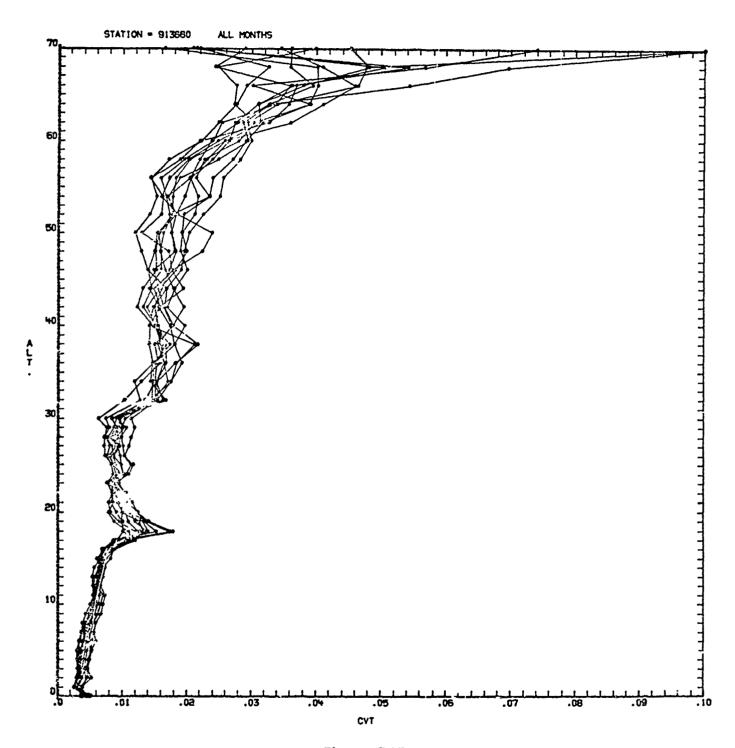


Figure B16.



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Figure B17.